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## Fifty Year Canon of Solar Eclipses: 1986–2035

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Scientific and Technical Information Office

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# FIFTY YEAR CANON OF SOLAR ECLIPSES: 1986 - 2035

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### INTRODUCTION

instance, Meeus et al. give only the center line coordinates of each eclipse locations which are paramount in addressing the scientific goals, the issue Vanderleen, 1966] covers eclipses over a broad 612 year period from 1898 great value to planners. The Fifty Year Canon contains this information available 6 to 12 months before each event and cannot be of assistance opportunities, taking into account the celestial mechanics and geographic through 2510. Because of the sheer number of eclipses covered in this northern and southern limits and detailed maps of each path would be to long range planning. Canon of Solar Eclipses [Meeus, Grosjean and work (1448), the details for any one event must be rather brief. For predictions are regularly issued by the Nautical Almanac Office of the U. S. Naval Observatory. Unfortunately, these circulars only become (Sections 3 & 4), thereby filling a void in the published literature on coordinates over shorter time intervals as well as coordinates for the The primary purpose of the Fifty Year Canon of Solar Eclipses: of funding and the logistical problems of organizing an expedition to Center line 1986 - 2035 is to provide a reference of moderately detailed eclipse Special circulars containing detailed eclipse work should be useful in identifying the most favorable eclipse predictions and maps for use by the astronomical community. using a fairly coarse time interval of every 12 minutes. remote destinations.

information in print about the visiblity of future eclipses and what appears laymen. The solar eclipse is unquestionably the most spectacular celestial Furthermore, most references are obscure, not easily accessible and/or out time and maximum magnitude of partial phases or totality/annularity can questions arise as to where a particular eclipse will be visible from, and The orthographic maps in the Fifty Year Canon show regions The secondary purpose is to provide a general reference on future be estimated for any locale. Furthermore, the 200 year eclipse catalog Section 1) and world maps of every umbral eclipse during this period of visibility for both umbral and penumbral eclipses. From these, the deal of interest among the general public and news media. Naturally, in the popular literature is often short on accuracy or even incorrect. As such, eclipses generate a eclipses for teachers, students, amateur astronomers and interested when the next eclipse occurs. Unfortunately, there is very little Section 2) provide a convenient and useful reference. phenomenon visible to the naked eye.

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### ORGANIZATION OF THE CANON

The Fifty Year Canon of Solar Eclipses: 1986 - 2035 is composed of projection maps which show the regions of visibility of both partial and lists the general characteristics of every solar eclipse from 1901 through Section 1 is a catalog which Section 2 presents a detailed set of cylindrical projection world Finally, section 4 consists of a series of orthographic maps which show the umbral paths of every solar eclipse from 1901 circumstances on the center line for every central eclipse from 1986 through 2100. Section 3 gives geodetic path coordinates and local central phases for every solar eclipse from 1986 through 2035. four major sections and two appendices. through 2035.

used to predict the occurrence and general characteristics of solar eclipses. It makes use of many approximations while maintaining a reasonable level by Meeus [1982] and the ample comments should make the program self-Appendix A provides some general background on solar eclipses and of accuracy and reliability. The program is based on algorithms devised covers eclipse geometry, eclipse frequency and recurrence, modern eclipse Appendix B is a listing of a very simple Fortran program which can be prediction, geometry of the umbral shadow and time determination. explanatory.

A detailed description of each section of the Fifty Year Canon Solar Eclipses: 1986 - 2035 follows.

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## SECTION 1 - SOLAR ECLIPSE CATALOG: 1901

remaining 2 (5.1%) are annular/total. Since the Saros cycle is not static, umbral. However, to appreciate a realistic frequency and type distribution umbral. Of these, 12 (30.8%) are annular, 12 (30.8%) are total and the The period from 1986 to 2003 contains Section 1 consists of a catalog of the general characteristics at the of present eclipses, it's necessary to sample a period commensurate with instant of greatest eclipse for every solar eclipse during the two hundred these figures will change. For example, eclipses in Saros series 124 will The second century contains 224 eclipses of which 77 are penumbral and 147 are 39 eclipses of which 13 (33.3%) are penumbral and 26 (66.6%) are year interval 1901 to 2100. During the first century, there are 228 eclipses of which 78 are penumbral and 150 are umbral. change from annular/total to partial in 2004. the 18 year 11 day Saros cycle.

while column 2 gives the Julian Date. The Julian Date is the number of value for delta T (in seconds) which was used in the calculations. Delta Moon's shadow passes closest to the Earth's center. Column 4 lists the determined from observations. Beyond 1985, the values for delta T were eclipse. Greatest eclipse is defined as the instant when the axis of the rotation rate are unpredictable (See: Appendix A - Time Determination). Column 3 gives the Universal Time (hours:minutes:seconds) of greatest extrapolated and are only approximate since fluctuations in the Earth's Column 1 of the catalog lists the Gregorian Date of each eclipse T is the difference between Terrestrial Dynamical Time and Universal days elapsed since Greenwich Mean Noon on 1 January 4713 BC. Time. For the period 1901 - 1985, the values for delta T were Column 5 characterizes the nature of the eclipse as follows:

T = Total Eclipse.
A = Annular Eclipse.
A/T = Annular/Total Eclipse.
P = Partial Eclipse.

Additional information about the eclipse is defined as follows:

Begin (i.e. - the first eclipse of a new Saros series). - the last eclipse of an old Saros series). = Central Eclipse with no Northern Limit. = End (i.e.

- Central Eclipse with no Southern Limit.

\* = Non-Central Umbral Eclipse

(i.e. - edge of umbral cone grazes Earth but shadow axis misses).

take place at the descending node (Gamma increases with each succeeding replaced with the topocentric ratio of the apparent diameters of the Moon and Sun. The apparent diameter ratio is always greater than or equal to Eclipses belonging to an odd numbered Saros take place at the ascending node of the Moon's orbit (Gamma decreases minimum distance of the shadow cone axis from the center of the Earth The Saros series numbers are consistent with those introduced with each succeeding eclipse), while eclipses of an even numbered Saros eclipses, the magnitude is always less than 1.000. For annular eclipses, surface at the instant of greatest eclipse. Eclipse magnitude is defined The magnitude for total eclipse. The sign of Gamma indicates whether the shadow cone axis passes north (+) or south (-) of the Earth's center. Column 8 gives eclipse). Column 7 lists the value of Gamma, which is defined as the in units of equatorial radii. This corresponds to the instant of greatest the fraction of the Sun's diameter obscured by the Moon. For partial the maximum magnitude of the eclipse from any point on the Earth's the magnitude is also less than 1.000 and is equal to the topocentric eclipses is always equal to 1.000. Therefore, the magnitude has been The next column gives the Saros series to which the eclipse ratio of the diameters of the Moon and Sun. by van den Bergh [1955]. 1.000 for total eclipses.

greatest eclipse are listed in the columns 'LATITUDE' and 'LONGITUDE'. central phase (total or annular) at the instant of greatest eclipse is given longitudes are East of the Greenwich Meridian. Although greatest eclipse The geodetic coordinates of the shadow cone axis at the instant of in the horizon. The next two columns, 'SUN ALT' and 'SUN AZ', give the Sun's altitude and azimuth as seen from the previous coordinates at annularity at that time follows (kilometers). Finally, the duration of the These coordinates are given in degrees and minutes to the nearest tenth of greatest eclipse lies on the day/night terminator and the Sun appears eclipses, the shadow axis misses the Earth entirely. Therefore, the point of a minute. Negative latitudes are South of the Equator and negative reaches its greatest obscuration from any location on Earth. For partial duration (for total eclipses), the differences are usually negligible. For the instant of greatest eclipse. The width of the path of totality or central eclipses, these coordinates represent the point where the Sun differs slightly from the instants of greatest magnitude and greatest in minutes and seconds.

# SECTION 2 - WORLD MAPS OF ECLIPSE PATHS: 1901

Each map is centered on the equator and covers 160° in latitude (80° North to 80° South) and 130° in longitude. The first map of each  $40^\circ$  West to  $90^\circ$  East and the third map encompasses  $80^\circ$  East to  $150^\circ$ trio runs from longitude 160° West to 30° West, the second map covers Section 2 presents maps of the path of every umbral eclipse during the two hundred year period 1901 through 2100 (as tabulated in Section polar regions) is covered with a 10° of longitude overlap between each West (= 210° East). Thus, the entire planet (excluding the extreme decade is plotted on a set of three cylindrical projection maps of the 1). The eclipses are broken up into twenty year intervals and every

can be established by noting that it usually lies midway between the ends e-lipse appears directly above the point of greatest eclipse ('\*'). In cases greatest eclipse is indicated with an '\*', usually near the center of each re the '\*' appears within two overlapping eclipse paths, its identity The date of each shadow at every half hour Universal Time. Furthermore, the point of twenty year interval are plotted, along with the outline of the umbral path. Total eclipses are readily distinguished from annular eclipses The northern and southern limits of each eclipse path during because their paths are plotted with a heavier pen.

interval of Section 2. They occur in 1928, 1950, 1957 (two), 1967, 2014 greatest eclipse lies on the terminator edge of the path. In addition, the eclipse of Feb 2044 has no southern limit. These two events are also There are eight non-central eclipses during the two hundred year recognized by annular eclipse of May 2003 has no northern limit, while the annular their distictive 'D' shaped paths and from the fact that the point of These non-central eclipses are easily bounded by the terminator along their missing edges. and 2043 (two).

# SECTION 3 - CENTRAL PATH CATALOG: 1986

109 solar eclipses occur; 37 are penumbral or partial while the remaining 72 are umbral. Appearing at the top of each table is the type of eclipse (annular, total or annular/total) and date, followed by the Saros series and the extrapolated value of delta T which was used in the calculations. point are given in degrees and minutes to the nearest tenth of a minute. Negative latitudes are South of the Equator and negative longitudes are coordinates of the path of totality or annularity for every central eclipse over the fifty year interval 1986 to 2035. During this period, a total of data are listed at one, two, four or six minute intervals. The next six The first column of each table gives the Universal Time (UT) for the data which follows. Depending on the duration of the central eclipse, columns define the geodetic coordinates of the northern and southern The latitude and longitude of each Section 3 consists of a series of tables which list the geodetic limits as well as the center line. East of the Greenwich Meridian.

minutes and seconds. For annular/total eclipses, the sections of the path kilometers. Finally, the duration of the total or annular phase is given in fraction of the Sun's diameter obscured by the Moon. The next two columns, 'SUN ALT' and 'SUN AZ', give the Sun's altitude and azimuth eclipses, the ratio is always greater than or equal to 1.000. For annular The column identified as 'DIAMETER RATIO', is the ratio of the at maximum eclipse as seen by an observer on the center line. The eleventh column lists the width of the path of totality or annularity in magnitude at maximum eclipse. Eclipse magnitude is defined as the which are total in nature are identified by a 'T' after the duration. eclipses, the ratio is less than 1.000 and is identical to the eclipse topocentric apparent diameters of the Moon and the Sun.

in longitude. Fortunately, corrections to the tabulated longitudes are quite All path characteristics are calculated for sea level and the effects of extrapolated ones because of the unpredictable fluctuations in the Earth's divergence will be to induce a shift in the path coordinates east or west rotation (See: Appendix A - Time Determination). The result of this century, the actual value for delta T will inevitably diverge from the As we progress into the twenty-first straight forward, using the following equation: refraction have been ignored.

Shift (in degrees) = 
$$0.00417807 * (\Delta T1 - \Delta T2)$$

iere:  $\Delta T1$  = table value of delta T (in seconds)  $\Delta T2$  = true or observed delta T (in seconds)

correct longitudes of the umbral path. Changes in delta T have no effect This shift is added to the tabulated path longitudes to calculate the on the tabulated latitudes.

It should be pointed out that the path of the annular eclipse of 29 April 2014 is not included in this section because it has no central line. 2003 has no northern limit since the northern edge of the shadow cone The shadow axis misses the Earth while the edge of the shadow cone misses the Earth. In this case, the northern boundary of the path is barely grazes the planet. Furthermore, the annular eclipse of 31 May defined by the Earth's day/night terminator.

during the fifty year interval 1986 to 2035. Each map is an orthographic eclipses are oriented with their origins (i.e. - disk center) at the sub-solar Section 4 consists of a series 109 maps, one for every solar eclipse North is to the top in all cases and the daylight terminator is the Sun's declination plus or minus  $45^\circ$  (depending on the hemisphere). ongitude at the instant of greatest eclipse and the latitude is equal to plotted for the instant of greatest eclipse. The sub-solar point on the The maps for total or annular eclipses are oriented with the point of The maps for partial projection of the Earth which shows the path of partial and central Earth is indicated by a star shaped character. greatest eclipse at the origin.

If the penumbra has both a northern and southern limit, the The limits of the Moon's penumbral shadow delineate the region of visibility of the partial solar eclipse. This irregular or saddle shaped at sunrise (western loop) and sunset (eastern loop). The points 'P1' and begins/ends at sunrise and sunset' loops is the curve of maximum eclipse (partial eclipse begins) and last contacts (partial eclipse ends) the Earth's coordinates where the penumbral shadow cone becomes internally tangent Great loops at the western and eastern extremes of the penumbra's path surface. If the penumbral path has both a northern and southern limit, shadow axis falls no closer than about 0.45 radii of the Earth's center. Earth and consists of several distinct zones or limits. At the northern eclipses have only one of these limits, as do central eclipses when the dentify the areas where the eclipse begins/ends at sunrise and sunset, curves are connected in a distorted figure eight. Bisecting the 'eclipse rising and setting curves form two separate, closed loops. Otherwise, 'P4' mark the coordinates where the penumbral shadow first contacts then points 'P2' and 'P3' are also plotted. These correspond to the region often covers more than half of the daylight hemisphere of the and/or southern boundaries lie the limits of the penumbra's path. to the Earth's disk. respectively.

Curves of maximum eclipse are northern to the southern penumbral limits, or from the maximum eclipse plotted at each half hour Universal Time. They generally run from the outlines of the umbral shadow, from which the Universal Time of each A curve of maximum eclipse is the locus of all points where the If the eclipse is central, the curves of maximum eclipse run through the half-hourly The curves of constant eclipse magnitude at sunrise and sunset curves to one of the limits. eclipse is at maximum at a given time. curve can be identified.

delineate the locus of all points where the magnitude at maximum eclipse southern limits of the umbra which define the path of totality are curves maximum eclipse at sunrise and sunset. Furthermore, they're parallel to eclipses. In fact the northern and southern limits of the penumbra can the northern/southern penumbral limits and the umbral paths of central curves are for magnitudes of 0.2, 0.4, 0.6 and 0.8. The northern and be thought of as curves of constant magnitude of 0.0. The adjacent s constant. These curves run exclusively between the curves of of constant magnitude of 1.0.

the day/night terminator and the sun appears in the horizon. For central The point on the Earth's surface which is at or is nearest to the axis at eclipse at sunrise and sunset. The outline of the Moon's umbral shadow misses the Earth entirely. Therefore, the point of greatest eclipse lies on greatest duration (for total eclipses), the differences are usually negligible. eclipses, the umbral path begins and ends along the curves of maximum Moon's shadow passes closest to the Earth's center. Although greatest is plotted at every half hour Universal Time along the central path. In addition, the umbra's position is labeled at each integral hour Universal this time is marked by an '\*'. For partial eclipses, the shadow axis Greatest eclipse is defined as the instant when the axis of the eclipse differs slightly from the instants of greatest magnitude and

shadow with the Earth. P1 and P4 are the first and last contacts of the The first number identifies the sequence order of the eclipse in the series, while the second number is the total number of eclipses in Moon's shadow axis from the Earth's center in Earth radii (Gamma) and the series. The Julian Date (JD) at greatest eclipse is given, followed by the extrapolated value of delta T ( $\Delta$ T) used in the calculations (delta left corner are the Universal Times of greatest eclipse and conjunction of the geocentric ratio of diameters of the Moon and the Sun. For partial Data pertinent to the eclipse appear with each map. In the upper U1 and U4 are the first and last contacts of the umbra; they denote the start geocentric coordinates of the Sun and Moon at the instant of greatest apparent semi-diameter (SD) and horizontal parallax (HP). The Saros eclipse. They consist of the right ascension (RA), declination (DEC), eclipses, the geocentric ratio is replaced by the magnitude at greatest To the upper right are exterior contact times of the Moon's the Moon and Sun in right ascension, the minimum distance of the and end of the total or annular eclipse. Below each map are the series for the eclipse is listed, followed by a pair of numbers in penumbra; they mark the start and end of the partial eclipse. parentheses.

are given, as well as the local circumstances there. In particular, the Sun's altitude (ALT) and azimuth (AZ) are listed along with the duration of totality or annularity (minutes:seconds) and the width of the path Time). Finally, the geodetic coordinates of the point of greatest eclipse T is the difference between Terrestrial Dynamical Time and Universal (kilometers).

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### ACCURACY OF THE EPHEMERIDES

0.01 arc-seconds. The lunar ephemeris was developed primarily from the off for planetary perturbations is 0.025 and 0.01 in longitude and latitude Clark [1954]. All solar perturbation terms in longitude and latitude with The solar ephemeris which was used for these predictions is based perturbation terms in longitude and latitude with arguments greater than coefficients greater than 0.025 arc-seconds have been included. The cutthe work of Brown [1919] with improvements from Eckert, Jones and Moon's fundamental arguments with coefficients greater than 0.025 greater than 0.0010. Finally, all terms additive to the respectively. Perturbations in lunar parallax include all terms with on the classic work of Newcomb [1895]. It includes all planetary seconds have been retained. coefficients

deviations of the solar and lunar ephemerides with the JPL DE-200 are as In order to determine the accuracy of these ephemerides, they have been compared against the Jet Propulsion Laboratory's Developmental Ephemeris 200 (or JPL DE-200) for 260 new moon dates over the The mean differences and standard interval 1980 through 2000.

# Comparison of Solar/Lunar Ephemerides with JPL DE-200

Dec S. Dev. (arc-sec)	0.173	0.386
Dec Mean (arc-sec)	-0.030	-0,008
RA S. Dev. (sec)	0.044	0.031
RA Mean (sec)	+0.036	-0.002
	Sun	Moon

velocity in right ascension of the Moon with respect to the Sun is 0.0343 deviations in right ascension correspond to an uncertainty in the umbra's seconds per second. Thus, the combined uncertainties in right ascension position of 2102 meters in the east/west direction. The mean angular north/south direction in the Earth's fundamental plane. Similarly, the The solar and lunar deviations in declination correspond to an uncertainty in the umbral shadow's position of 1044 meters in the can also be thought of as an uncertainty of 2.2 seconds in time.

Such information coordinates and local circumstances for long range planning. In fact, the shifts of this magnitude are not visible. Thus, the uncertainties are well Almanac Office, U. S. Naval Observatory, Washington, D.C. 20392-5100, These circulars are available 6 to 12 months before each major eclipse. For eclipses of low solar altitude, the observer must also make within the acceptable range for the purposes of predicting eclipse path On the scale of the maps presented in Sections 2 and 4, path account a detailed analysis of the Moon's limb profile. Such inforn is available through special eclipse circulars published by: Nautical predictions using higher accuracy ephemerides which also take into predictions presented here should be adaquate for most center line experiments. However, observers near the path limits will require corrections for the effects of atmospheric refraction.

-1.34 seconds has been applied to the lunar ephemeris to reconcile it with Canon, the author has applied a -0.6 arc-second correction to the Moon's Moon's center of mass and center of figure. In addition, a correction of In the generation of eclipse predictions presented in the Fifty Year ecliptic latitude. This takes into account the difference between the the FK4 equinox.

predictions. The larger value (k=0.2724880) was used for annular eclipses and exterior contacts while a smaller value (k=0.272281) was reserved for for 'k' is commendable because it should eliminate confusion arising from This is significant because a solar eclipse cannot be regarded as total as adopt a value for the mean lunar radius of k=0.2725076, in units of the peaks and low valleys along the Moon's rugged limb. Previously, the Nautical Almanac Office used two separate values for 'k' in their eclipse present since two different values of 'K' were used for total and annular Supplement, 1974]. In principle, the IAU's adoption of one single value In August 1982, the IAU General Assembly passed a resolution to represents the lunar valley bottoms and hence the minimum solid disk. as any photospheric rays reach the observer through valleys along Nevertheless, a smaller value of 'k' is still necessary since it 1983] and is believed to be the best mean radius, averaging mountain Nautical Almanac Office for solar eclipse predictions [Fiala and Lukac, the use of two different values. It also eliminates the discontinuity second and third contact calculations of total eclipses [Explanatory Earth's equatorial radius. This is the value currently used by the the lunar limb [Meeus, Grosjean and Vanderleen, 1966]. long

eclipse begins and ends (second and third contacts, respectively) and the Of primary interest to most observers are the times when central duration of the central phase. When the IAU's mean value for 'k' is

The calculation of these corrections is not trivial but must be performed, For observers near the center line of a total eclipse, the limb corrections used to calculate these times, they must be corrected to accommodate low valleys (total) or high mountains (annular) along the Moon's limb. especially if one plans to observe near the path limits [Herald, 1983]. can be closely approximated by using a smaller value of 'k' which accounts for the valleys along the profile.

larger IAU value for 'k'. Furthermore, the smaller 'k' will produce longer For this reason, the author has chosen to adopt the smaller value compared with the Nautical Almanac Office's calculations which use the slightly shorter durations and narrower paths for total eclipses when for 'k' (k=0.272281). As a consequence, the current work predicts durations and wider paths for annular eclipses.

the smaller 'k' are in better agreement with actual observations made near path width of 2.3 km (k=0.272281). However, the Astronomical Almanac Moon for several seconds during maximum eclipse. The symmetry of the beading phenomena in photographs proves that the observers were near for 1986 predicts a duration of 3.3 seconds and a path width of 31.1 km using different values of k in eclipse calculations. For example, the Fifty Year Canon predicts a maximum duration of totality of 0.2 seconds and The total solar eclipse of 3 October 1986 illustrates the effects of the center line and not the edge of the path. Thus, predictions using eclipse was never quite total. Instead, Baily's Beads surrounded the (k=0.2725076). Experienced observers in the path reported that the the center line.

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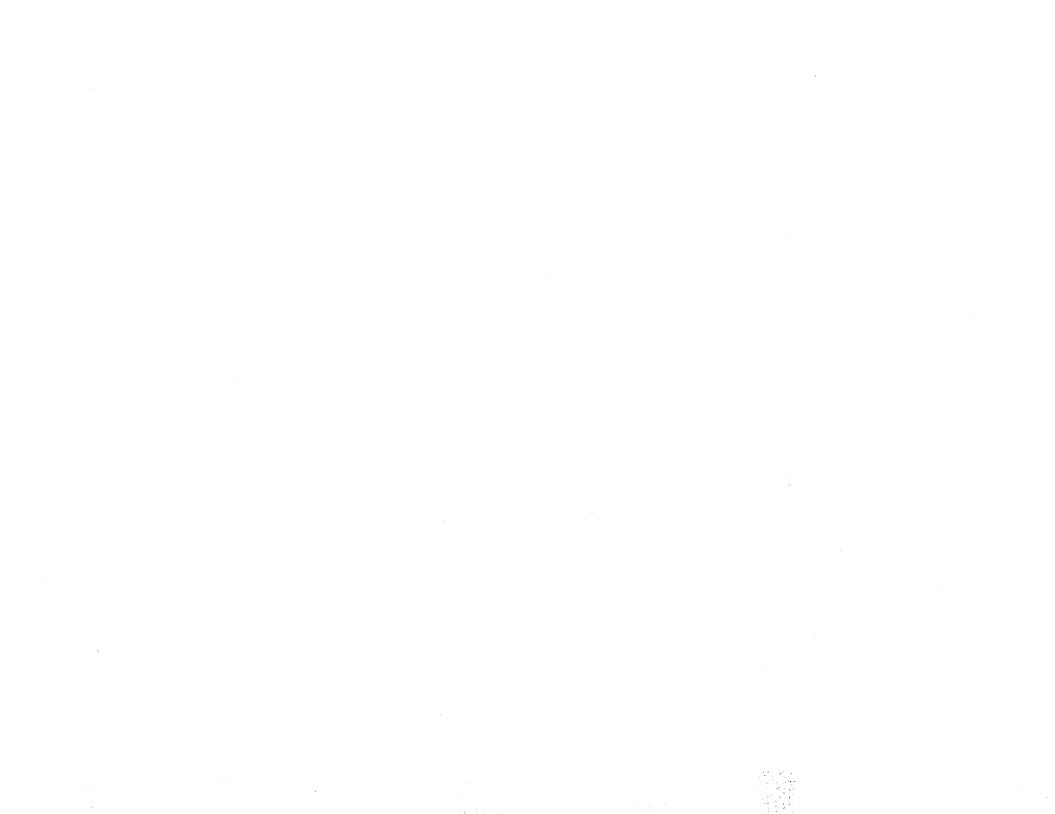
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SECTION 1 - SOLAR ECLIPSE CATALOG: 1901 - 2100



### Table 1

TOCAL CIRCUMSTANCES AT GREATEST ECLIPSE CANON OF SOLAR ECLIPSES

POOR QUALITY LEBRARA SET SERVE SET SET SERVE SET SET SERVE SET SET SERVE SET SET SET SERVE SET	9.048 9.691 6.63 1.23 1.801 8.818	286.6 226.6 333.2 264.7 158.5 21.8	2.91 8.98 2.88 5.88 1.08 4.98	4.01 EII 2.27 - 3.3 2.24-021- 2.25-32- 3.6	26. 26.1 54. 27.1 -243.3 16. 26.8 11. 6.9 -293.4 -65. 42.6 66. 10.3 -63. 40.3	8426.0 8280.1 8286.0 8386.0 820.1 8420.0 1110.0 12574.0 8387.0	0.9418 6.837.0 6.837.0 6.808.0 7.17.0 7.828.1 7.838.1	124 111 1134 123 123 123 123 113 113	A T A A T A B B B	8.31 8.31 2.31 7.71 7.71 8.91 9.91 7.81	0:12:58 12:34:23 4:33:15 22:52:28 16: 0:19 26: 46:17 7:28:28 13:16:18 13:16:18	24201428.61 2420366.02 2420369.05 2420364.17 2421222.37 2421426.69 2420364.17 2421428.61 2421428.61	19 JUL 1917 19 JUL 1916 24 DEC 1916 36 JUL 1916 36 JUL 1916 36 JUL 1916 37 JUL 1916 38 JUL 1916 38 JUL 1916 38 JUL 1916
1.31:4 6.73:4 7.74:8 6.1:0 7.33:1	4.363 7.261 7.261 6.48	9.728 9.386 9.881 9.18 9.18	9.81 7.37 2.17 8.83 4.38	7.1-88- 0.81-321- 0.86-481 0.86-481- 0.8	1.2- 38- 1.3- 18- 1.3- 18- 1.3- 18- 1.5- 18- 1.1- 1	2.42.0 00.00 00.00 1.00.00 00	8342.1- 1449.0- 5030.1 7922.0- 7723.0 6225.0 7723.0 8416.1 8416.1 7001.1-	152 127 127 137 147 147 147 147	P + P + A + P P P P	8.9 6.01 6.01 7.51 7.41 7.41 5.31	24:44:43 6:42:9 6:42:35 6:42:45:19 73:36:9 13:36:3 13:36:3 13:36:3 13:36:3 13:36:4 13:36:4 13:36:4	2418663.32 2418800.74 2419166.44 2419166.46 2419686.07 2419686.07 2419686.07 2419686.07 2420040.70	12 DEC 1989 2 MAY 1918 22 MCT 1912 17 APR 1912 17 APR 1913 18 MCT 1912 17 APR 1913 20 MCT 1913 21 AUG 1913 21 AUG 1913 22 MCT 1913 23 MCT 1913 24 MCT 1913 25 MCT 1913 26 MCT 1913 27 MCT 1913 28 MCT 1913 29 MCT 1913 20 MCT 1913 21 MCT 1913 22 MCT 1913 23 MCT 1913 24 MCT 1913 25 MCT 1913 26 MCT 1913 27 MCT 1913 27 MCT 1913 28 MCT 1913 28 MCT 1913 29 MCT 1913 20 MCT
1.84:E 7.42:2 6.52:7 8.51:4 8.11:0 8.53:0	4.291 1.981 8.832 1.881 8.841 8.92 1.13	8.102 8.371 8.1 8.081 7.771 7.71 8.011	56.08 30.2 50.8 78.8 81.7 81.7 8.63 8.63	3.81 4 8.31 071 8.31 65 8.31 62.9 9.22 83 1.42-83-1 1.23-63-1	42 27.8 42 26.5 43 66.3 46.8 46.	7740.1 6753.0 1355.0 1355.0 130581 6396.0 1306.1 6306.1	8073.0 9842.1- 9842.1- 9238.0 9276.1 9238.0 9288.0 7861.0 7861.0 7861.0	146 136 136 158 158 118 148 148	Т Р Р Р Р Т Р Р Р Т Р Р Р Т Р Р Р Г Р Р Р Р	8.88.98.88.98.89.88.99.98.77.88.99.98.99.98.99.99.99.99.99.99.99.99.	7.43:15 7.43:15 7.43:15 7.12:45 7.12:45 7.12:45 7.14:24 7.15:24:28 7.16:24:28 7.16:24	2417088.06 2417264.82 241713.05 2417142.55 241765.14 241767.14 2418121.19 2418121.19 7418121.19	23 PEC 1908 24 ALC 1908 25 ALC 1908 26 ALC 1908 27 ALC 1908 28 ALC 1908 28 ALC 1908 29 ALC 1908 20 ALC 1908 20 ALC 1908 21 ALC 1908 22 ALC 1908 23 ALC 1908 24 ALC 1908 25 ALC 1908 26 ALC 1908 27 ALC 1908 28 ALC 1908
8.82:8 2.1 :11 7.23:1 9.11:5 2.7 :8 8.61:8 8.73:7	7.782 8.888 8.887 1.782 1.782 1.783 1.488 1.488	7.238 8.061 2.061 1.38 1.71 4.231 6.888	6.18 6.18 6.32 6.32 8.08 6.43	4.82-86- 1.83-88- 1.83-88- 1.72-241 1.83-281- 1.84-81-81-81-81-81-81-81-81-81-81-81-81-81-	7.14-1- 4.84 01 8.73-68- 1.14 17 8.73-68- 2.81 03 6.63-73- 4.88 3 6.18-68-	0890.1 08120.0 08120.0 8838.0 1960.0 1960.0 1960.0 1960.0 1960.0	7295.0- 3374.0 4285.1- 4283	138 153 153 118 121 140 141 141	Т <b>А</b> РР <b>В</b> А Т А Т А Т А Т А Т А Т А Т А Т А Т А	8.2 2.0 1.0 1.0 2.0 1.0 0.0 0.0 0.0 0.0	97:82:2 91:92:1 1:92:4 1:92	2416522.73 2416648.09 2416663.83 2416663.83 2416666.74 2416666.74 2416678.09 2416678.09 2416910.72	18 MAY 1901 11 NOV 1901 2 MARY 1902 31 OCT 1902 21 SEP 1903 17 MAR 1904 17 MAR 1904
CENTRAL DURATION	HTA9 HTGIW	Z¥ NNS	NUS TJA	LONGITUDE	E LATITUDE	MAGNITUDE	CAMMA	SVECS	<b>3</b> 4YT	DELTA T	GREATEST ECLIPSE	STAG MAIJUL	DATE

### Table 2

COCAL CIRCUMSTANCES AT GREATEST ECLIPSE CANON OF SOLAR ECLIPSES

0.123 1.33.5 1.33.5 2.53.4 5.53.5 5.53.5	2.8801 8.431 6.07 8.221 8.082 8.082	284.5 231.6 206.9 206.1 206.1 204.5	0.41 3.55 3.57 2.49 8.03 4.34	2.03-83- 0.55 4231 0.55 421 0.15 -451- 0.34-181- 0	4.92 I8 4.92 I8 4.92 I8 5.92 I8 6.03 I8 7.94 I8 7.9	6603.0 1340.0 7868.0 77729.0 7320.1 1989.0 1250.1 8649.0	1492.1 8303.1 6030.1- 8030.1- 4058.0 2012.0- 8384.0 8384.0 8883.1-	111 124 129 129 134 139 144 111	PP	\$2.52 \$3	28:34:0 76:33:21 76:33:21 76:36:30 76:36:30 76:36:30 76:36:30 76:36:30	242696.78 2426596.78 2426596.36 2426596.34 2427128.03 2427265.38 242782.53 242782.53 242782.53 242782.53	18 APR 1935 12 SEP 1935 14 FEB 1935 24 FEB 1935 26 1935 27 FEB 1935 27 FEB 1935 27 FEB 1935 28 FEB 1935 29 FEB 1935 20 FEB 1935 20 FEB 1935 20 FEB 1935 21 FEB 1935 21 FEB 1935 22 FEB 1935 23 FEB 1935 24 FEB 1935 25 FEB 1935 26 FEB 1935 27 FEB 193
8.03:0 6.03:0 7.8:3 9.1:0 7.33:1	7.87 7.87 1.591 1.1 4.481	8: 791 9: 731 9: 888 9: 841 8: 98	6.48 6.48 2.87 6.18 6.18	24 45.6 24 45.6 25 45.6 25 45.6 26.9 27 24.9 27 24.	6.64-53- 6.64.1 6.64.1 6.66.4 6.66.3 6.66	8210.1 8210.1 8210.1 82630.1 8660.0 8630.1 8600.1 88300.1	3364.0- 1618.0 1618.1- 1600	146 146 127 127 127 158 158 146 146 146	* 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	6.22 8.22 8.22 8.23 8.23 0.52 0.52 0.52 5.52	\$25.502 \$25.502 \$2.502	2424884.35 242688.07 2426238.67 2426386.06 2426416.35 242662.91 2426962.99 2426917.08 2426962.29	3 1AN 1927 29 JUN 1928 3 ANY 1928 17 JUN 1928 17 JUN 1928 18 ANY 1928 19 MAY 1928 17 JUN 1928 18 ANY 1928
8.88:8 8.36:5 8.36:5 8.4:9 8.4:7 8.61:4 8.61:4	2.852 8.831 8.831 7.841 7.841 7.841	8.858 1.102 1.102 1.071 7.3 8.871	7.77 6.93 6.83 86.3 78.6 86.3	166 4.31 166 4.3 166 2.9 166 2.9 176 2.9 176 2.9 176 2.9 176 2.9 176 4.3 176 4.3 17	20.24-01- 20.4-45 3	8730.1 8150.0 80540.1 1183.0 1183.0 10050.1 10050.1 10050.1	1812.0- 8413.0- 8413.0 1218.1 1844.1- 4823.1- 8617.0- 8630.0	136 136 126 128 118 143 143 143 133	<b>↑</b> ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑	8.12 2.22 4.22 5.22 5.22 7.22 6.22 9.22 7.22	4.46.28 12.44.16 14.53.59 14.5	69.8168242 60.8678242 60.8678242 60.867863 60.867863 60.86863	14 JAN 1926 14 JAN 1926 20 JUL 1926 31 JUL 1926 31 JUL 1926 31 JUL 1926 31 JUL 1926 31 JUL 1926 32 JUL 1926 31 JUL 1926 32 JUL 1926 31 JUL 1926 31 JUL 1926
1:16.6 5:22.2 5:82.9 7:86.8 1:56.1 4:62.1 4:62.1 5:63.2 6:22.3 6:22.3 7:68.3	9.881 1.211 2.64.4 2.65.9 2.85.9 2.85.2 2.85.2	7.86.5 4.26.1 5.65.1 1.38.8 8.85.1 7.231 7.231	2.52 0.23 8.37 6.23 1.72 1.08 7.91	8.61-321- 8.11 231 8.12 23 8.14 53 1.13 84 1.13 84 1.13 84 1.14 10 1.14 10 1.15 10 1.16 10	2.2-88- 2.31-21 2.31-21 2.31-21 2.31-21 2.31-21 2.31-21 2.31-21 2.31-21 2.31-21 2.31-21 2.31-21 2.31-21 2.31-21 2.31-21 2.31-21 2.31-31 2.3	1676.0 2620.1 2856.0 20170.1 2019.0 1576.0 1247.0 1620.0 1859.0	8916.0- 8988.0 898.0- 8982.0- 8982.0- 8982.0- 8982.0- 8982.0- 8982.0- 8982.0- 8982.0- 8982.0- 8982.0- 8984.00- 8985.00- 8986.00- 8	121 126 141 141 146 178 178 178 178	A T A P P A T A T A	4.93 8.91 8.91 8.03 8.13 8.13	9:27:77 15:21:58 16:21:58 16:21:58 16:11:58 16:11:58 17:38:58 17:38:58 17:38:58	2421576.89 2421763.42 2421931.14 2421931.14 2422242 2422242.89 2422242.80 24223142.85	14 DEC 1917 8 JUN 1918 2 DEC 1919 12 MAY 1920 18 MAY 1920 18 MAY 1920 18 MAY 1920 19 MAY 1920
CENTRAL DURATION	HTA9 HTGIW	Z¥ NNS	SUN TJA	LONGITUDE	<b>JOUTITAJ</b>	MAGNITUDE	GEMMA	SOAAS	<b>BAYT</b>	ATJ30 T	GREATEST ECLIPSE	STAG NAIJUL	BTAQ

Table 3

### TOCAL CIRCUMSTANCES AT GREATEST ECLIPSE CANON OF SOLAR ECLIPSES

5.63:5 7.33:1 6.63:0 8.51:1 1.63:0 7.36:2 7.36:2	1.351 8.58 8.58 5.451 6.75 8.751	8.002 1.531 9.72 7.352 8.928 8.938 4.331	8.83 2.69 2.69 8.82 8.82 8.18 6.29	2.62 TII 8.61-161- 6.61-37- 6.74 dd 6.74 dd 7.62-701- 8.1- 14- 8.92 821 8.82 821	2 66.6 23 -6.9 23 -6.9 24 -6.1 24 -6.1 25.9 26.5	1396.0 1520.1 9803.0 2529.0 2810.1 4629.0 3880.0 7479.0 3680.1	2478.0 1814.0 6138.0- 8803.1 8089.0 17243.0 4331.0 4834.0	137 147 147 147 147 147 147 147 147	A 1.82 A 4.82 T 8.82 G 8.62 G 8.62 A 8.62 A 8.62 A 1.08 A 1.08 A 1.08 A 1.08	3:11:38 17:21:48 2:38:44 2:38:44 2:48:21 0:12:0 12:48:21 2:58:44 2:48:21 2:48:21 2:58:3 2:58:3	243266.34 2432866.76 2432866.76 243389.11 243359.16 243359.16 243359.16 2433891.84 2433891.84	12 NOV 1947 9 MAY 1948 12 SEP 1960 12 SEP 1960 14 MAR 1949 16 NOV 1949 17 SEP 1961 18 MAR 1949 18 MAR 1949 1940 1940 1940 1940 1940 1940 1940
8.58.8 4.8.9 6.15.6 6.13.6 7.51.5	8.788 8.341 7.701 8.19 8.391	10.6 172.7 2.4 3.63.6 184.3 3.22.6	8.35 8.78 8.37 6.34	4.88-891- 6.98-39- 6.98-39- 6.98-39- 7.12 12- 6.98-47- 6.98-	1.78-46- 6.00 e1 1.78-7- 6.00 e1 7.83 e9 6.00 e1 7.83 e9 7.12 e9 6.01 0	6046.0 8240.1 8240.0 0076.0 810.1 8368.0 8481.0 8481.0 8477.0	5408.0- 5202.0 8160.0- 8160.0- 8264.0- 84662.1- 84170.1- 8652.1- 8636.0-	136 146 146 146 146 146 136 136 138	A 6.32 A 6.32 A 6.32 A 6.32 A 6.32 G 9.72 G 9.72 G 9.72 G 9.72	11:81:4 64:35:12 64:35:12 64:44 7:81:41 7:81:41 7:12:61 14:75:71 84:74:61	89.789957.68 243125.14 2431291.74 2431291.74 243124.01 243125.23 2432326.07 2432326.07	1 AUG 1943 26 JAN 1946 29 JUL 1946 3 JUL 1946
2.94.1 6.36:1 6.36:3 6.04:7 8.12:6 2.39.2	284.2 4.81.4 2.9.3 2.71.9 2.6.9 143.0 4.923	118.6 74.4 163.1 17.9 2.00 2.00 164.8	8.91 8.77 8.77 8.37 5.58 5.58	2.0 est 5.0- aat 5.0- aat 5.15 est 5.0- aat 5.16 est 6.13-69- 6.13-69- 6.3- at 7.5- 03- 6.3- at 7.5- 03- 7.5- 03-	7.7 87 7.74-27- 7.74-27- 9.12 91 9.12-12-13-13-13-13-13-13-13-13-13-13-13-13-13-	1579.0 6350.1 4659.0 6469.0 6759.0 6759.0 6359.0 6359.0 6353.0	8859.0 8879.0 8812.0 8812.0 7303.0 7403.0 6434.1 7423.1 7423.1 7423.1 8578.0	123 148 143 133 133 133 133	8.83 8.83	23:38: 8 16:39:20 23:31: 4 20: 8: 2 20: 8: 2 20: 8: 2 20: 8: 2 20: 4 20: 8 20: 8 20: 8 20: 8 20: 8 20: 8 20: 8 20: 8 20: 8 20: 8	02.5750542 2429542.36 2429542.36 2429904.03 2430568.69 2430653.61 2430653.61 2430653.61	19 APR 1939 12 OCT 1939 12 APR 1940 27 MAR 1941 27 MAR 1941 27 MAR 1941 37 16 MAR 1942 37 16 MAR 1942 37 16 MAR 1942 38 1948
6.08:1 4.316:2 5.15:5 6.4 :7 7.00 :21	4.482 1.381 7.563 8.482 4.483 2.318	8.732 1.781 3.59.9 3.59.9 3.4.8	1.22 1.73 1.73 7.37 9.97 8.48	2.62 311 0.11-62- 1.63 3 0.26-9- 1.63 6.3 2.64 731 0.05 051 0.05 051	2. 72.28 2. 62.28-28-28-28-28-28-48-48-48-48-88-88-88-88-88-88-88-88-88	2867.0 8766.0 4062.0 6260.1 6469.1 6469.1 4816.0 2330.1 6817.0	1.1438 1.365.1 10.244.1 10.245.0 10.255	140 141 130 130 131 131 431	9 9 . 8 2 3 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	19:59:44 19:59:49 19:59:49 19:59:49 19:59:49 19:59:49 19:59:19 19:59:19 19:59:19	2427837.18 2427984.33 2428162.25 2428162.25 2428616.48 2428616.48 2428616.48 2428616.48	\$\text{\$1\$ NOA 1838}\$ \$2 DEC 1834\$ \$3 DEC 1834\$ \$3 DEC 1839\$ \$3 ONG 1839\$ \$3 EEB 1839\$
CENTRAL DURATION	HTA9 HTGIW	Z¥ N∩S	SUN TJA	LONGITUDE	E LATITUDE	MAGNITUDE	CAMMA	E SAROS	ATJEQ GYT TYP	GREATEST ECLIPSE	JULIAN DATE	DATE

T.73:1 8.32:0 8.11:6 8.72:6	0.48 7.601 6.61 6.531	24.6 24.6 329.6 210.3 150.4	3.07 7.81 5.47 2.77 4.53	8.82-82- 8.82-82- 8.81 831 4.8 82 6.81-811- 2.73-63- 7.7 411 7.7 411	6.8 81 1.36 81 4.74-41- 4.9 88 1.63-03-03- 1.63-03- 1.63-03- 1.63-03- 1.63-03- 1.63-03- 1.63-03- 1.63-03- 1.63-03- 1.63-03- 1.63-03- 1.63-03- 1.63-03- 1.63-03- 1.63-	5520.0 5520.1 5617.0 2650.1 4768.0 6600.1 4366.0 4140.1	2055.0- 2055.0- 3051.1- 3041.1- 8040.1- 8449.0 2012.0- 1744.0	130 147 129 129 139 139 139 139	+ 4 4 4 4 1 4 1 4	5.75 8.75 8.85 8.85 8.95 8.95 8.05 8.05 8.05 8.05 8.05	1:68:6 19:68:6 19:68:68 19:68:68 19:68:68 19:68:68 19:68:68 19:68:68	2439265, 243926212 243936212 2439396, 74 2439396, 74 2439396, 74 24408653, 24	26 MAY 1966 2 MAY 1967 2 MOV 1967 2 MOV 1967 2 MAR 1968 18 MAR 1969 11 SEP 1969 11 SEP 1969 11 SEP 1969 11 SEP 1969
8.2 :4 8.4 :8	1.481	9.891	0.78	7.03-611-	4.S4 I	9996.0	3065.0	132	·	8.88	87:71:7	89.7808542	38 MAY 1965
9:31:9	7.791	8.846	0.38	7.7- 84- 13-38-1- 13-38-8 173 16.2 13-38-3	7.81-88- 8.83-48- 6.38.78 8.81-48-8	8833.0 6.37.0 8.322.0 8137.0 4430.1	8382.1- 821.1- 8282.1 8211.1 8224.0-	122 122 127 127	P. P. P.	4.38 9.38 7.38 9.38	28:38: 13:12:63 13:18:1 13:18:1 13:18:1	2438469.35 243866.69 2438686.97 2438586.97 2438911.39	4 DEC 18e4 5 10F 18e4 10 10N 18e4 14 1VN 18e4 50 10F 18e3
8:35:8 8:35:8 8:35:8 8:65:1	8.994 7.841 8.201 8.91 4.101	9.91 8.7 8.84 8.191.3	4.72 8.77 4.88 4.08 8.84	3.2- 4- 8.4- 871- 1.5 4 3 1.1 31 5.59 813	8.03-54- 0.63 II 6.41-6- 8.03-64- 1.14 I3	3789.0 08.40.1 3179.0 1399.0 1230.1	1888.0- 3012.0 1511.0- 0004.0- 0733.0	140 130 130 130 150	¥	34.1 34.3 34.8 34.8 36.1	44:84:01 0:12:35:35 0:75:51 0:76:61 11:86:02	28.7527.95 28.7787.02 28.7787.02 28.5855.07 28.58531.38	11 AUG 1962 11 AUG 1963 11 AUG 1963
2:45.2	8.732	<b>≯.</b> 631	8.72	5.0- 281- 2.2 47 7.1- 04-	2.8-27- 7.4.1 4.12.74	8407.0 813.0 1360.1	1.164Ø 1.2056 9.8828	150 163 148	9 T	8.88 8.88 9.88	7:26:63 8:19:44	2437020.81 2437020.81 2437345.85	16 FEB 1960 27 MAR 1960 27 WAR 1960
8.8 :T 7.01:3 7.32:7 7.1 :E	8.722 8.802 8.745 4.021	1.481 3.71 3.42.5 8.99.0	9.87 7.27 6.29 1.39	6.45-48- 6.45-48- 6.55-521- 7.52-251- 7.52-751- 8.35-751- 8.35-751-	67 62.0 7.82 87.7 7.12.15.3 8.82.1 1.0- 42-1 1.0- 42-1 24.9	8,848.0 1,868.6 1,8688 1,8688 1,8688 1,8358	2260.1 8069.0 \$200.1- 8472.0 \$262.0- \$434.0- 7024.0	143 133 158 153 153 118	++ 4 ++ ↑ + ↑ ↑	6.18 6.18 6.28 8.28 8.28 8.28	8: 0:32 9: 52: 0 9: 52: 0 9: 52: 0 9: 52: 0 7: 52: 0 7: 52: 0	2436899.83 243698.60 243698.64 2436312.64 2436818.68 2436844.02	2 OCT 1966 30 APR 1967 12 OCT 1968 23 OCT 1968 24 APR 1969 25 OCT 1968 26 OCT 1969 27 OCT 1969
8.24:1 1.38:2 0.98:7 7.7:7 7.9:3 7.44:4	278.3 152.7 262.0 7.532 7.53.9 8.345.9	8.632 2.7e1 4.136 8.6 8.871 8.0	1.12 61.9 74.8 1.18 64.8 26.5	8.84-401- 1.88 17 4.24 411 4.26 021 4.04.9 6.41-83- 1.0-711- 1.0-711- 8.44.041	1.23 18 6.20 48 6.20 48 6.50 - 23 6.50 - 23 6.50 - 23 7.34 41 7.34 45 7.34 41 7.34 41 7.34 41	8347.0 8102.0 7175.0 8359.1 8279.0 8710.1 8710.1 830.1	221.1 221.1 221.1 221.2 2445.1 2613.0 26	146 136 138 131 121 121 124 146 146	<b>↑</b> ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑	7.08 0.18 0.18 0.18 1.18 5.18 6.18 6.18 7.18	100 100 100 100 100 100 100 100 100 100	243425.54 243425.64 24369.16 24369.16 24369.16 243469.16 243469.16 243469.16 243469.16 243663.39	\$ 100 1828 14 DEC 1828 50 100 1824 20 100 1824 20 100 1824 20 100 1824 11 100 1823 14 EEB 1823 14 EEB 1823 14 EEB 1823 14 EEB 1823 14 EEB 1823 14 EEB 1823
CENTRAL DURATION 6:40.0	HTA9 HTGIW 4.48	NUS SA ⊗.72	SUN FLT	LONGITUDE 8.8 3.3	LATITUDE	MAGNITUDE Ø.942Ø	GAMMAD GAIØ5	SORAS	•	DELTA	GREATEST ECLIPSE	JULIAN DATE	BATE

CONON OF SOLAR ECLIPSES CANON OF SOLAR ECLIPSES

Table 4

Table 5

### TOCAL CIRCUMSTANCES AT GREATEST ECLIPSE CANON OF SOLAR ECLIPSES

6.63:1 6.63:1 6.63:1 7.7:0 6.83:1 7.7:0 8.84:5	1.121 8.7 8.48 1.568 1.2 1.5 3.751	192.9 164.1 2.02 2.02 2.02 3.012 9.912 9.913	66.38 7.57 3.17 7.01 6.2 7.27 7.38	9.54 4 4.44 4 4.45 57 4.65 57 4.85 18- 5.71 2 5.71 2 5.71 2 8.12-851- 8.13-951-	0.62 78 0.62 78 7.74-78- 8.16-88- 7.21-18- 8.02-21- 2.43 63 0.02 41	886.0 7520.1 4048.0 7520.1 1000.1 11000.1 11000.1 11000.1 11000.1	EIQA. Q 4372. Q 4216. Q 8170. I 7679. Q 8280. I 8299. Q 4872. Q 7814. Q	182 187 119 119 124 119 129 134 139	A T A T A T A T A T A T A T A T A T A T	7.83 8.43 8.43 8.43 8.43 8.63 8.63 8.63 8.63 8.63 8.63	12:31:12 16:45:41 22:54:16 21:29:36 14:11:26 6:12 19:6:13 12:45 12:45 1:58:55	2445673.02 2445851.28 2445051.46 244628.09 244659.76 244659.76 244659.63 2446884.03 2446884.03	4 DEC 1988 38 MAY 1984 12 MOV 1986 3 OCT 1986 3 OCT 1986 23 SEP 1987 23 SEP 1987 24 SEP 1987 25 MAR 1988
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CONON OF SOLAR ECLIPSES CORNSTANCES AT GREATEST ECLIPSE

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5.402

332.4

248.6

9.782

S. QE

160.3

8.802

3.588

9.411

176.8

184.3

3.838

ZΥ

NNS

**⊅**.06

8.8

1.8

8.7I

1:49:2

4. TA: Q

7.73:2

9'6 : 7

I.78:2

Z.22:0

4.8 :I

5:25.6

3.54:5

6:02:9

7.6 :3

7.22:8

6.09:T

**₽.8I:**2

7:61:2

2.32:7

I.82:4

5:11:3

£.81:1

1:64.3

3:61.3

7:6:2

£.8E:@

8.68:8

7.28:4

DURATION

CENTRAL

18:27.2

2.911

I.S&I

2.691

T. TTT

2.44

4.88

125.3

£.69I

8.642

2.082

1.62E

7.732

8.182

7.582

2.818

8.882

9'16T

4.78I

1.914

9.929

8.06

2.12

T. TII

9.002

**MIDTH** 

HTA9

I.64

4'IE

131 18.6

Z:8- 89I-

164 62.3

4.28 2T

0.81-22-

121 13.1

126 35.9

2.83 8

1.88 TEL

I.84-I7-

9.81-17-

9.8- 08-

8. 34.9

8.3 88

Q'II PII

7.84-821-

61 28.6

£. 23.3

2.31 32

1.63-88-

Z.8 TT

8.82 AII

1.3 401

8.2 £8

9.03-321-

8.82-77-

8.12 IT

8.71 94

8.88 88

4.43 78

Z. 54-67-

4.81-201-

**TONGILODE** 

Ø: 73 8@I

1.62-231-

7.41-EE-

-136-43.4

Z. 44-281- 7.32 @T

E. IE 88

Z.T IT

0.53-89-

9.8E-17-

8.8 62

8.6- 62-

7. PI-8I-

1.2 2.7

Z.SI-SY-

8.71 17

6'81-19-

6.86-64-

Z. ØE 99

8. QE-78-

8.31-48-

6.34 88

I.S4 E8

Ø'98-91-

7.73 2

Ø. 62 32

E.81-18-

4.21 3a

Q. 54-48-

I.43-09-

0.8 IS

52 IG'8

2.12 11

Ø.88-6-

6.8E I3

@. Y- 28-

8.34-87-

I.12-01-1

3.52-71-

6.84 Q8

9. IE @E

7.63 8

1.83-12-

I.86-0

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### CANON OF SOLAR ECLIPSES

Table 8

MAGNITUDE LATITUDE	CAMMA	SORAS	39YT
AT GREATEST ECLIPSE	UMSTANCES	SEID .	Γ0C¥Γ

### COCAL CIRCUMSTANCES AT GREATEST ECLIPSE CANON OF SOLAR ECLIPSES

Table 9

2.8 :4 8.03:2 8.99:8 1.4 :8	7.531 1.15 3.311	8.281 8.81 8.888 8.88 1.882	0.17 8.33 8.17	0.h1-28- 1.3h-711- 8.32 201 8.2- 201 8.2- 88- 0.8h-1h- 8.8- 89- 7.71 121 8.81 28	22 21.9	9340,1 67979,0 9199.0 9280,1 9383,0	7810.1 7810.1 7810.0 7810.0 7810.1 7810.1 7810.1 7810.1 7810.1 7810.1	155 166 166 166 166 166 166 176 176 176 176	₽₽₩₩₩₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽	0.311 6.311 7.311 7.311 4.711 8.811 6.811 7.611	2:10:37 12:2:12 13:31:62 23:39:8 7:8:18 1:8:3:6 1:9:32 1:9:32 1:9:32 1:9:32	2470272.59 2470449.38 2470627.27 2470803.49 2471336.02 2471336.02 2471483.25 2471612.55 2471600.25	11 APR 2061 4 OCT 2061 30 WAR 2062 22 SEP 2063 12 SEP 2064 3 AUG 2064 3 AUG 2064 2 SEP 2064 2 SEP 2064
4:83:4 6:72:6 7:34:4 8:75:0 8:12:0	4.172 4.172 6.481 6.481 7.82	184.7 8.3 363.9 186.5 361.5	4.9.4 6.33 1.88 3.93 8.93	8.84-111- 8.83 771 8.92 8. 8.31-081- 8.92 11 8.92-39- 8.34 92 8.92-39- 8.92-39- 8.92-39- 8.92-39- 9.92-31-	62.83 63.93 63.93 63.93 63.93 63.93 63.73 69.93 69.93 69.93 69.93 69.93 69.93	1440.0 0440.1 1530.0 7300.1	2976.1 2976.1 1846.1- 1890.1- 1890.0 5766.0- 5762.0 6491.0- 7440.1	163 143 143 153 153 153 153 153 153 153 153 153 15	P P P P T A T A P P P P A A P P	100.9 110.6 110.6 111.5 112.7 112.7 113.3 113.3 114.5	1:33:16 13:30:50 13:50:57 13:50:57 13:50:57 13:30:50 13:30:50 13:30:50 13:30:50	246864.95 246864.95 246961.49 246961.49 246961.65 246961.75 246961	28 JAN 2047 29 JUN 2048 31 MAY 2048 31 JUN 2048 32 JUL 2047 22 JUL 2047 32 JUN 2048 31 MAY 2048
2.12:4 2.44:7 2.72:2 2.72:2 3.6:6 6.8 6.8 6.8 7.42:4 7.13:4	273.4 273.4 278.3 461.1 261.2 261.2 261.6 318.1	28.8 269.6 264.2 329.8 264.2 329.8 264.2 329.8 264.2	2.27 2.27 3.8 3.81 3.17 3.17 8.73	8.22-781- 8.22-781- 7.83-181- 7.21-38- 8.25-38 1.80-31- 8.80-38- 1.71 171 7.71 171	26 56.5 23-45.7 61 27.6 64 19.7 26 19.7 26 19.7 26 19.7 26 19.7 26 19.7 26 19.7 27.45.1	41.0614 0.950 0.950 0.960 0.966 0.966 0.9266 0.9261 1.0631	\$362.0 \$362.0 \$360.1 \$360.1 \$316.0 \$316.0 \$316.0 \$355.0 \$363.0	146 121 121 121 124 146 146 146	++	4.401 9.301 1.001 1.001 1.001 1.001 1.001 1.001 1.001	25:71:2 25:0:38 26:0:24; 26:46; 27:46; 26:25 27:46; 27:46; 28:6:22 28:6:22	2468994,66 2467471,58 2467349,29 2467349,29 2467856,56 2468286,56 2468869,56 2468869,93 2468869,93	20 APR 2045 20 APR 2045 30 APR 2045 22 AUG 2046 32 AUG 2046 32 AUG 2046 33 AUG 2046 34 AUG 2046 35 AUG 2046
3.83.8 6.63.9 6.63.9 7.13.1 7.60.6 7.50.6	7.002 2.701 2.15 2.36 3.36 5.085 7.17	8.2 1.081 1.881 2.5 2.531 2.531 8.365	3.54 6.78 6.57 7.55 6.81 8.58	0.8- 951- 2.2.2 2.2 2.4.9.6 2.4.4.2 2.5-271- 2.7-32.3 6.31-21- 4.4.4 16.00 16	7.4.6.1 2.4.7 2.4.7 2.5.2 2.5.3 3.7.3 2.8.3 3.8.3 3.8.3 3.6.	8276.0 8276.0 8276.0 8320.1 4346.0 3380.1 7623.0 8183.0 7846.0	8050.00 9014.00 9050.00 9050.00 9050.10 9050.11 9050.11 9050.00 905	127 132 147 147 162 119 124 124 134	7 A A T A A T A A T A A T A A T A A T A A T A A T A A T A A T A A T A	2.99 7.99 2.901 7.001 8.101 8.201 8.201 8.501 8.501	75.04:2 8 :74:8 13:32:65 14:03:46 15:52:46 17:12:64 17:13:46 11:36:19	246525.61 2465429.07 2465607.06 24656135.54 246539.39 246633.36 246663.30 2466639.39 2466837.57	13 JUL 2037 5 JAN 2038 2 JUL 2038 21 JUN 2039 11 MAY 2040 11 MAY 2040 21 JUN 2039 21 JUN 2039 21 JUN 2039 21 JUN 2039
CENTRAL DURATION	HTA9 HTGIW	Z¥ N∩S	NUS	LONGITUDE	<b>BOUTITAL</b>	MAGNITUDE	CAMMA	SOAAS	<b>34YT</b>	DELTA	GREATEST ECLIPSE	STAG MAIJUL	DATE

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12 SEP 2072

19 MAR 2072

23 SEP 2071

31 MAR 2071

78.7908742

**45.1297742** 

22.8477742

2477567.13

2.44.3

3.541

145.8

142.1

**991** 

ØSI

142

ØÞI

9996'Ø

60+I'I-

Ø.2621

1.0558

7817.0

2550.I

Z.A- 20I- 6.84 68

3.81 @E

8. E4 87

0.11-27-

14 13.9

T. &AS

8.002

733.2

I.BII

3:12:8

8. QI: E

p.pI

8.47

61:69:8

92:01:02

17:20:25

# :I :9I

E478.0-6166'Ø 0.54-81-Ø.89 1.73 88 **ØLØZ 130 ₹** 340.6 **08.88877**≱2 9:19:0 8. QE 141.4 7: 8:53 132 Ø967'Ø-1.13-28-IE76.0 1.82-08-II APR 2070 2.08 2.44:2 E. ØII **≱.**61 8:36:2 18.2127742 140.8 13Q 1.8472 Ø398'Ø 4.2 62 -136 -6.3 16 OCT 2069 163.2 3.89 88. AEQTTAS P. P : P 168.3 4:18:62 138'8 152 \$629. Ø 9Z9Z'I-8.85-17-2.82 3 **50 MAY 2069** 17:53:17 2476887.25 ЬВ £.951 128 £780.0 -1'4822 9.34-89-0.23 63 21 APR 2Ø69 24.78857.92 139.2 9:11:01 **JZ**® 1.0622 7.2 17 Z668'Ø E. BI IQI 04.0IT874S 24 NOV 2868 138.6 21:32:24 **123** 6016.0 1.0299 Q. IE 89 131 Ø.5 31 MAY 2068 2476532.68 3:56:37 **6.751** 4767.8-148 OTTO'T -123-16.3 1.5- 15-8 DEC 2087 3.838 Q. TE 9:9:1 7.28 90.83E87AS 137.2 14: 3:38 143 TA IIØØ'I 4482.8 6.2- 8-3.67 32 19.6 190Z NOC II 7.7 : Q 2.4 1.281 20:42:2P 2476178.36 ٧ 136.5 138 Ø786. Ø 1650.0a.I IS 130 8.4 Ø'6II 9.748 2.78 2476001.52 11 DEC 5088 4: 8:4 Q:53:32 132.8 5404.Q-133 2.22-74-9140.I 8.64-371-**55 704 2066** 8.635 6.39 2475824.31 162.3 3:14:8 14:9Z:6I 128 136.1 9846. Ø 8287. Ø 2.12 86 0.8 QT 8.24 **51 DEC 5082** 198.2 2475646,86 6:68:4 £.8&£ 134.4 29:62:8 123 Ч 889Ø'T-8.62-39-6978. ® 2.8 6 L 2 AUG 2085 2476499.73 2:34:14 133.8 2872.1-128 Ы 7.24-28-6884. Q 6.IE-84-2476470.23 3 10r 50ee 1.551 17:33:49 1.4615 118 d 448I.0 £.64 49.3 7.83-17-2 FEB 2085 16.1283742 8:25:25 121 1.881 Ы 3880.I PII6'Ø SI 24'4 7.6 28 12 AUG 2064 3:97:71 2475145.24 148 132.5 1 9997.0-3640°I 9'99 96 2.73-01-2.28 7.22 7.72:4 183.8 67.786474S 17 FEB 2064 81:Ø:L 131.8 8698'Ø ItI 2926.@ E.S T 6.89 I.84-69-24 AUG 2063 126.8 99.0674742 9:99:8 8.462 1:55: 8 I.IEI Tars. @ 136 0970.I 25 32.3 5.82-891-8.57 **58 LEB 5083** 210.3 2474613.82 1.64:3 1.232 73:84:7 Ā 130.4 131 @888.@-£626.8 8.61-32-0.84-TT-Ø.828 E. QL 78.3544742 3 SEP 2062 S. Ih: Y 8.672 8:64:24 129.8 TSIQ. I 126 Ы 4476. Q E:81 19 @. 72-@31-II WYK S085 88.6324742 4:28:12 1.921 -1.0239 121 d 9186. Ø £.83-@9-8.63 841 13 OCL 5081 P6.QIIP7PZ 10:35: e 128.5 £196.0-124 ٧ 6976'Ø Ø.6- 29-8. PI 54 28.5 8.87 28 APR 2861 9.947 28.4565742 9. I4: E 7:26:51 127.9 67T Ā 1.0475 9736. Ø 6.1E 48 9.81-63-**₽.7**6 16.2 24 OCT 2060 88.837ETAS 4.7E:S 8.733 b:24: 4 2.721 744 8282.Q-8729. Ø I.84-32-Ø.11-82-9.47 38 APR 2868 9.082 4.82 I :ØI:ØI 2473679.92 8:3:8 126.6 138 Ø242.0 1 Ø99Ø'I 7.73-82-8.83 YS 1.881 8,37 2473482.89 6902 NON 9 5:15:3 **6.122** ØI:8I:6 172.9 134 Z944.0 7146.8 8.8- TA-8.54 8 T. EQZ 8.58 9:69:9 5.852 II WYY 2059 2473225.31 156.3 19:22:14 Ø8Ø9'Ø-129 Τ 1.0242 5.54-QI-100 20.2 9.69 18 NOV 2058 8.48 338.0 473Ø48.64 2:23:5 124.8 3:23:2 154 d 1.1221 848T. @ 0.43 28 **₽.81-₽71-**SI JUN 2068 13.0062742 \$:13:34 121 84 124.1 6987'I Ø9ZI'Ø 4.33-6-**0.73 33** 55 MYA 5028 2472870.94 10:38:5E 0. 42I 6II 96IE'I-9814.Q 8.16-68-9.41-19-**58 DEC 5021** 2472723.55 1:14:33 153.6 125 4.64-48-TAEQ. I 7046.Q-2.86-12-I TOF SOEL 2.91 Ø.33E 2.141 2472646.49 7:64:I 23:40:13 122.8 4347. Q 147 4946. Ø £.62 IT 4.771 9.14 1.8 871 E JAN 2057 1.862 16.8852742 4:22:5 Ø9: L7:6 122.2 142 @#82.@-7820.I **▶.31-38-**Ø. +I-6E-8.738 2.87 15 1NL 2056 8.82:2 a. Iai 89:17:07 2472192.35 3.121 137 9240'Ø-19 26.3 8786. ® 16 JAN 2056 321.7 I.78 123 40.0 1:52:6 Z. £4 22:18:42 2472014.43 120.9 135 ٧ **0979.0** 96I4.0 153 27.2 8.53 8 24 10L 2055 4.46 2.871 2.39 67:49:6 24.7581742 2:52.3 120.3 121 1.0369 ZIØ8'Ø-9.13-92-6.8I-EE-4.7 8.88 T. IQZ 3:16.8 DATE JULIAN DATE TYPE SAROS ECLIPSE MAGNITUDE LATITUDE LONGITUDE CAMMA ZΥ TJA **NOITARUQ MIDTH** DELTA **CREATEST** NOS NOS CENTRAL HTA9

LOCAL CIRCUMSTANCES AT GREATEST ECLIPSE CANON OF SOLAR ECLIPSES

Table 11

## FOCAL CIRCUMSTANCES AT GREATEST ECLIPSE CANON OF SOLAR ECLIPSES

8.73:8 1.88:2 8.83:0 2.41:8	0.871 1.311 0.08 0.311	8.481 19.6 7.148 3.002	4.38 3.73 8.07 3.17	7.56-721- 7.56-721- 7.56-61- 7.56-61- 7.66-61- 7.66-61- 7.61-61-61- 7.61-61-61- 7.61-61-61- 7.61-61- 7.61-61- 7.61-61- 7.61-61- 7.61-61- 7.61-61- 7.61-61- 7.61-61- 7.61-61- 7.61-	7.82 78 7.82 78 7.81 87 7.81 88 8.83 88 88 88 88 88 88 88 88 88 88 88 88 88	2138.0 2138.0 6813.0 6813.0 4694.0 4740.1 6169.0 6880.1 6887.0	7610.1 7611.1 6814.1- 2614.0 2614.0 2016.0- 8812.0 2601.1-	168 128 128 128 128 128 168	₽₽₽₽₩₩₩	168.6 168.6 169.6 171.3 172.2 173.1 173.1	538:51 13:34:01 13:34:14 14:48: 2 14:48: 2 14:48: 3 14:48: 3 14:48: 3 14:48: 3 14:48: 3	2483296.74 2483473.26 2483472.56 2483619.99 2483797.35 2484328.65 2484506.65	6 DEC 2086 2 MAY 2087 2 JUN 2087 26 OCT 2088 14 OCT 2088 10 APR 2089 4 OCT 2089 31 MAR 2090
0.84:1	6.38	6. <b>0</b>	7.54	-12-28.4	2.41-22-	ATIQ. I	9127.Q-	148	Ĭ	Ø. 791	11:7:11	84.7118842	11 JUN 2086
8.11:8 0.1:4 1.32:4 6.83:5 5:4:3	9.75.9 6.331 8.778 7.341 7.841 7.801 5.801	8.42 8.42 8.222 1.745 198.9	6.07 4.33 6.46 8.63 8.87	2.8 74 4.34-131- 6.98 78 9.98 78 6.18 78 6.18-74- 7.14-74- 8.8 981 8.81-181-	8.32 6 4.81-01- 6.81-61- 6.81-61- 6.81-7- 7.7 69.0 7.7 69.0 7.7 69.0 7.7 69.0 7.7 69.0 7.7 69.0 7.1 69.0	8626.0 1340.1 1340.0 5710.0 6710.0 0510.0 0278.0 0620.1 1766.0	2988.0 8004.0- 0710.1 8043.1 8043.1- 804.1- 804.0- 804.0- 7872.0	145 146 153 153 153 153 143 141	4TPPPP4T4	8.681 4.681 5.181 6.181 6.181 8.581 8.581 8.681 8.681 8.681	33:34:41 81:31:1 14:19 14:19 15:44:38 16:19 16:19 17:1	2481563.12 2481730.66 2481730.53 2482785.23 2482785.23 2482785.68 2482785.69 2482785.69 2482785.64	27 FEB 2082 27 AUG 2083 27 JUL 2084 3 JUL 2084 15 JUL 2084 16 FEB 20884 27 DEC 2084 3 JUL 2084 3 JUL 2084
7:36.3 5:33.2	8.772 2.742	2.728 2.212	3.88 2.07	2.85-53- 36 42.9 2.85-54.9	6.85 42 6.85 42 6.85 42 6.86	1278.0 8578.0 4089.0 0270.1	7730.1- 0270.1 2338.0- 8788.0	136 126 127 121	9 А	1.731 1.731 7.831	12:23:26 16:38: 6 16:38:11	28845.01 24818921.19 2481199.14 2481375.88	3 SEP 2080 18 MAR 2081 23 SEP 2080
2.63.7 7.63.8 6.40.1 6.43.3 8.38.8	118.9 262.4 262.1 287.5 287.6 405.7	3.242 2.002 3.131 3.13 3.17	65.9 61.9 2.97 6.8 8.3 8.32	8.24 84 8.24 89 8.24 88 8.81 88 8.81 84 8.82 881	7.8- EI- 2.8 82 8.03-72- 0.01 88 0.01 88	0620.1 1786.0 1070.1 3329.0 1130.1	8273.0- 1074.0 7881.0 8223.0- 1808.0 8429.0-	124 144 136 136 137	T A T A T	162.6 162.6 164.8 164.8 164.8	4:48:7 47:7:7:56:58 47:56:38 48:58:38 48:58:12 48:58:12 48:58:12 48:58:12 48:58:12 48:58:12 48:58:12 48:58:12 48:58:58 48:58:58 48:58:58 48:58:58 48:58:58 48:58:58 48:58:58 48:58:58 48:58:58 48:58:58 48:58:58 48:58:58 48:58:58 48	2479988.21 2489165.25 2480542.21 2480519.95 2480696.26	22 AAN 22 11 MAY 2878 11 MAY 2878 12 AAN 1 24 C5 T50 24 C5 T50 25 C5 T5
2:29.3 2:21.2 2:41.9 4:44.6 1:49.3	3.802 8.97 7.73 7.92 8.262 9.348	2.21 2.271 2.2 3.138 8.138 4.202	8.82 8.58 6.67 3.84 7.91	8.52 98 8.52 98 8.44-87- 8.51-89- 7.4 49 9.81 871 8.81 871 8.81-84- 8.81-84-	0.82 07 6.25 0 6.25 0 1.74 21 6.25 0 6.11-78- 7.7 60 8.7 60 0.52-40- 0.73 00 0.53-40-	1773.0 4620.1 8676.0 8889.0 1180.1 7349.0 2480.1 7187.0	2978.0- 6424.0 2421.0- 2421.0- 2823.0- 3789.0- 5789.0- 5839.0 7986.1- 1998.1-	122 132 147 147 147 147 152 154 154 154	₽ТАТТАРР	9.44.9 1.65.1 1.65.1 1.65.1 1.69.1 1.69.1 1.69.1 1.69.1 1.69.1 1.69.1	15:52:22 5:51:71 5:61:8 1:58:81 6:61:8 14:3:5 14:3:5 15:51 16:2:5 17:2:5 17:2:5 17:2:5 17:2:5	2478423.22 2478423.22 2478423.22 247854.28 2479131.75 2479131.75 2479456.23 2479456.79 2479633.99	7 FEB 2073 2 AUG 2073 27 JAN 2074 16 JAN 2076 13 JUL 2076 13 JUL 2076 14 JUL 2076 26 MOV 2076
CENTRAL DURATION	HTA9 HTGIW	Z¥ N∩S	NUS TJA	LONGITUDE	E LATITUDE	MAGNITUDE	CAMMA	SORAS	<b>3</b> 4YT	DELTA T	GREATEST ECLIPSE	JULIAN DATE	DATE

Table 12

## COCAL CIRCUMSTANCES AT GREATEST ECLIPSE CANON OF SOLAR ECLIPSES

3.28:8	142.2	1.82	2.0T	7.73-86-	▶.6Z-@I-	1.0402	8888.Q-	146	- <b>T</b>	8.461	8:49:16	2488315.87	4 SEP 2100
£.62:7	3.732	125.9	Ø.27	8.72 281	4.73 II	8889.Q	TT&E. &	141	Y	7.591	22:28: 6	2488138.44	10 MAR 2100
6.11:3	0.14S	2.812	T.88	4.03 S8.4	23 2Ø.4	1.8884	8666.Q	136	T	7.291	16:57:48	12,1867842	14 SEP 2099
₽.SE:T	1.372	3.728	8.88	2.4 4.2	1.1- QS-	8189.Q	8104.Q-	131	A	7.19I	72:43:22	34.4877842	21 MAR 2099
				ø. 88 39	7.34-19-	7800.0	-1.6412	184	89	6.0er	10:36: 6	\$487635.94	24 OCT 2098
				100 64.6	9'9 19	3987.Q	Ø811.1	156	ď	7.0er	11:18:0	2487606.52	SE SEP 2098
				38 I.4	-61 -2.5	Ø767. Ø	9001:I-	121	d	7.68I	2Ø: 2:26	2487430.34	1 APR 2098
3:35:6	8.114	<b>4.</b> 78	26.3	7.68-88-	2.74-38-	\$6\$6.8	Ø£68. Ø-	124	¥	6.88I	Z: 1:20	2487281.58	16ØZ ∧ON ₹
9:18:8	4.688	4. IZI	8.18	8.18 941	£.≱2 78	1.0538	\$138.0	671	ĺ	6.78I	18:34:31	72.3017842	TENS YAM II 4
8:52.5	7.882	£.81	1.87	1.71-591-	3.44-62-	7829.8	1202.0-	771	Ā	6.88I	7 :88:Q	2486927.53	TE NOA 5080
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3.81:8	8.441	3.845	2. Ø3	4.7- 7E-	5.24-81-	2880.1	9689.8-	129	i	Ø. 48I	10: 7:38	2486395.92	2 2 NN 2095
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FIFTY YEAR CANON OF SOLAR ECLIPSES: 1986 - 2035

SECTION 2 - WORLD MAPS OF ECLIPSE PATHS: 1901 - 2100

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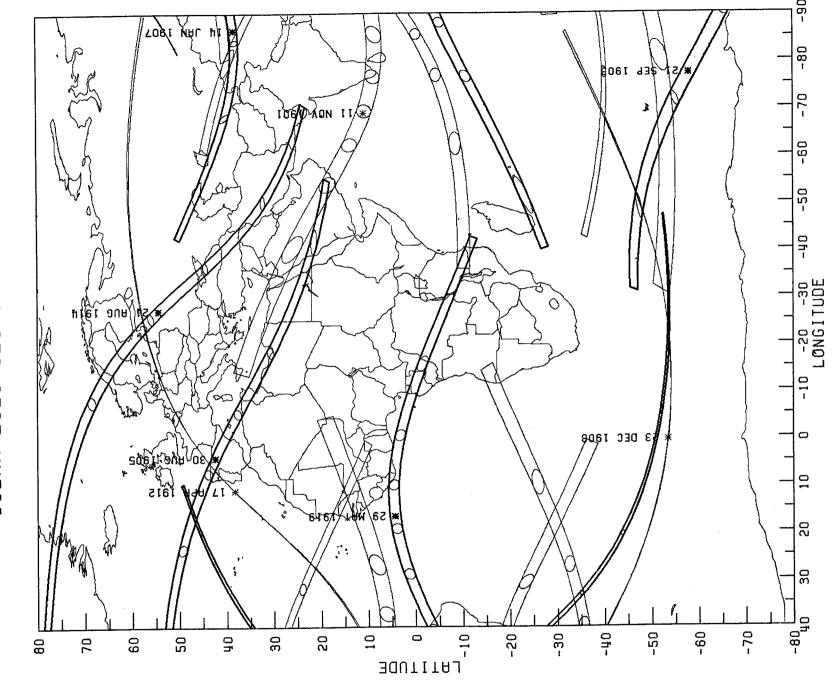
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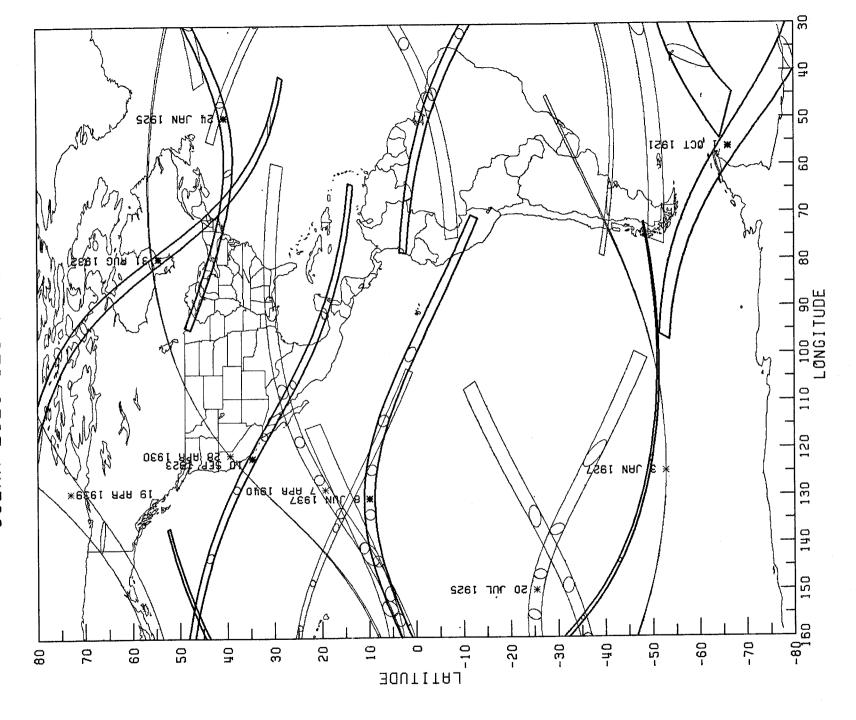
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Figure 3





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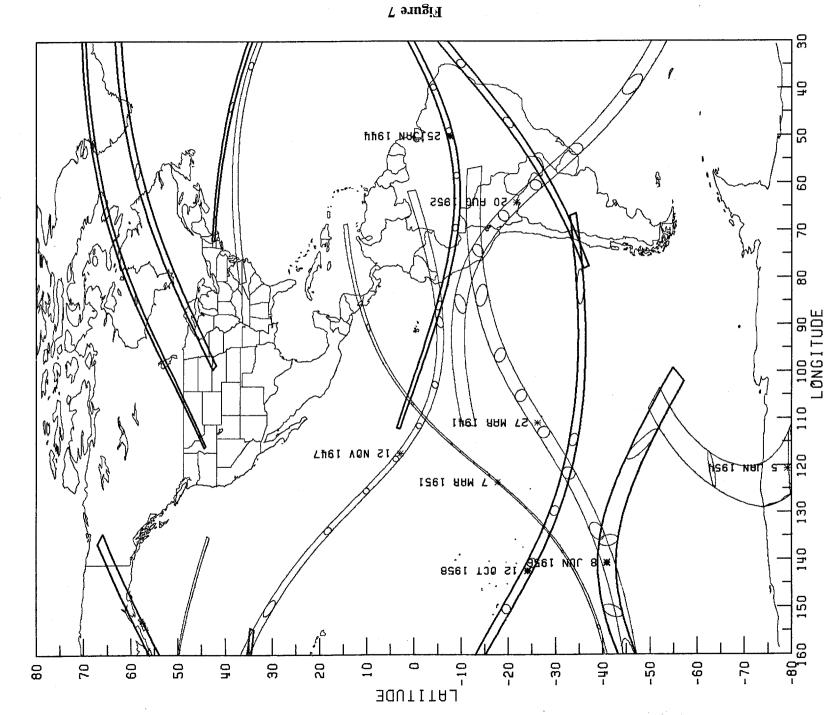
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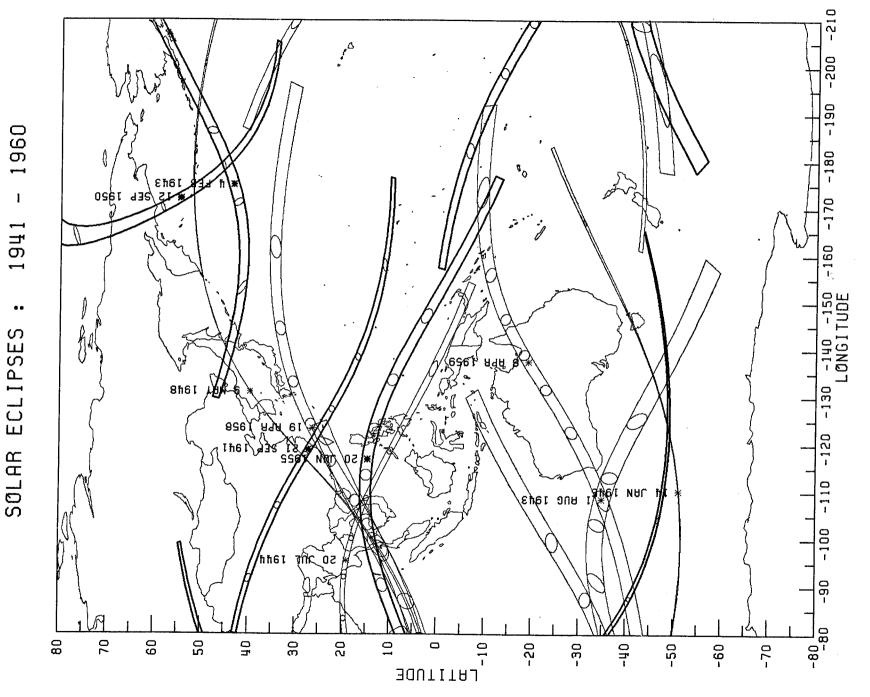
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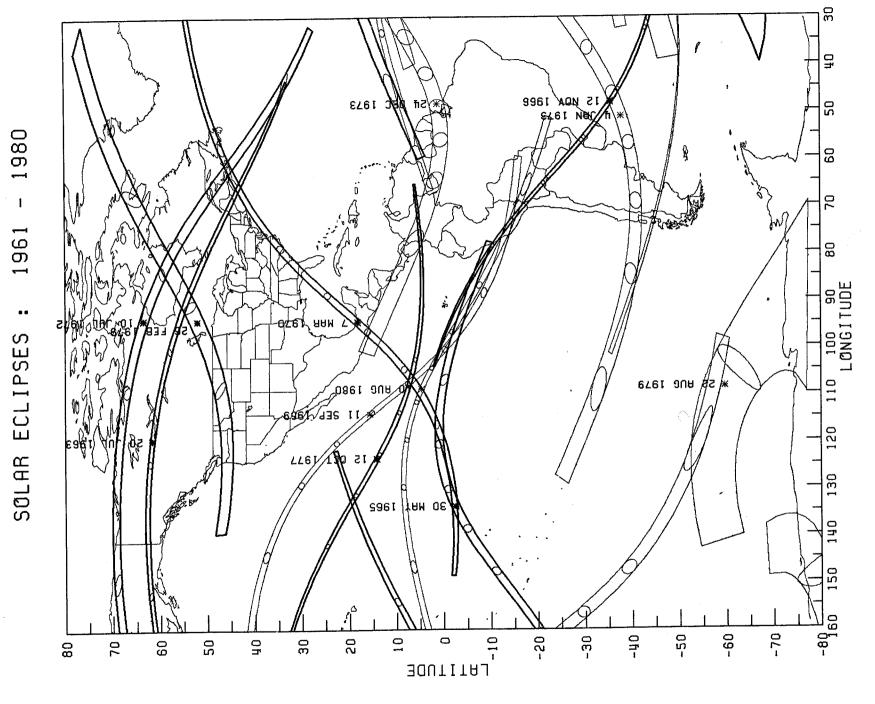
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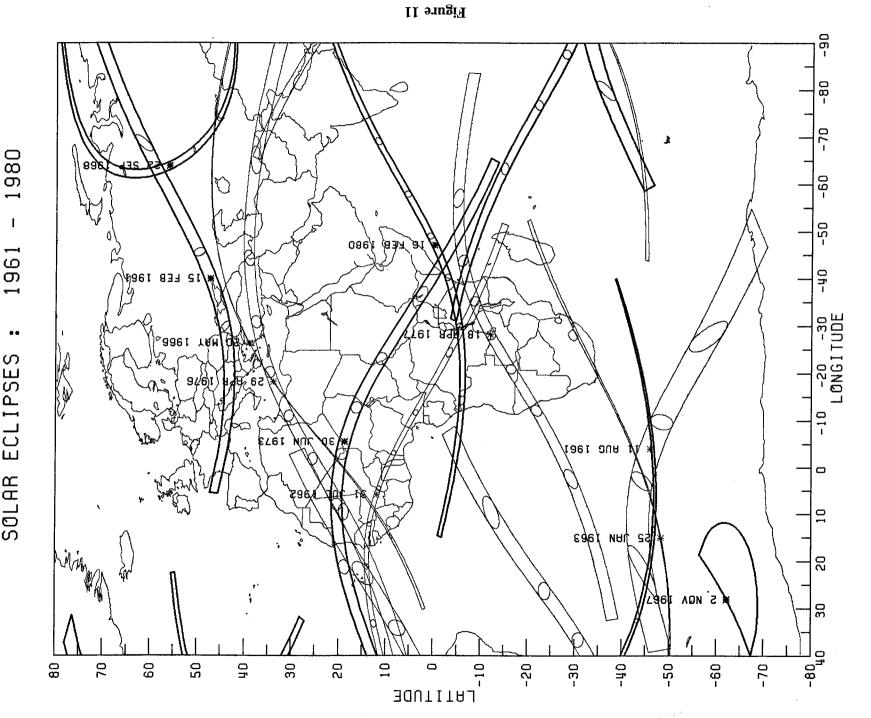
SOLAR ECLIPSES: 1941 - 1960



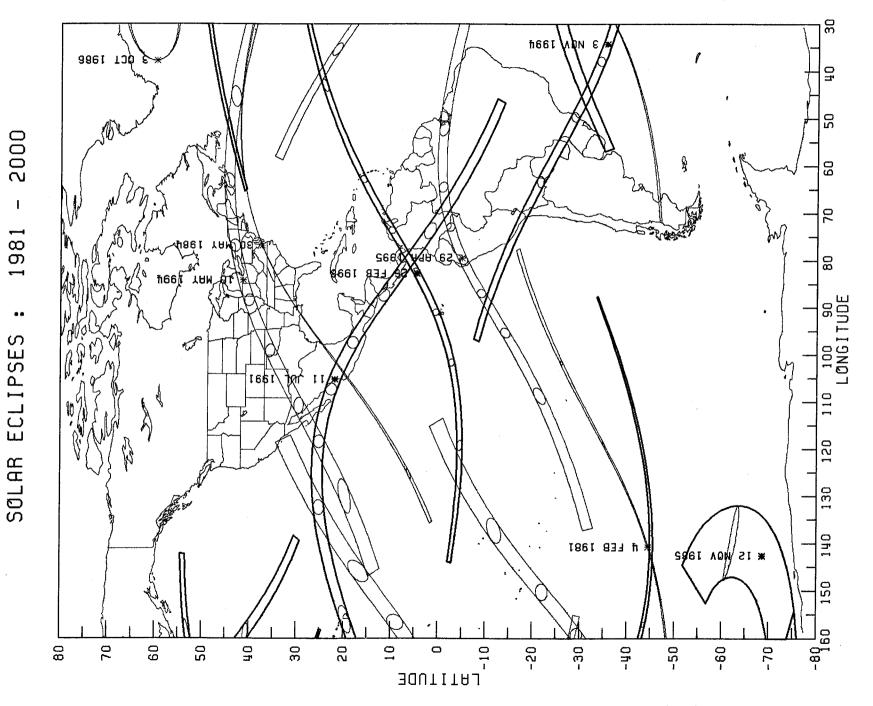




1961 **ECLIPSES** SOLAR



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Figure 14

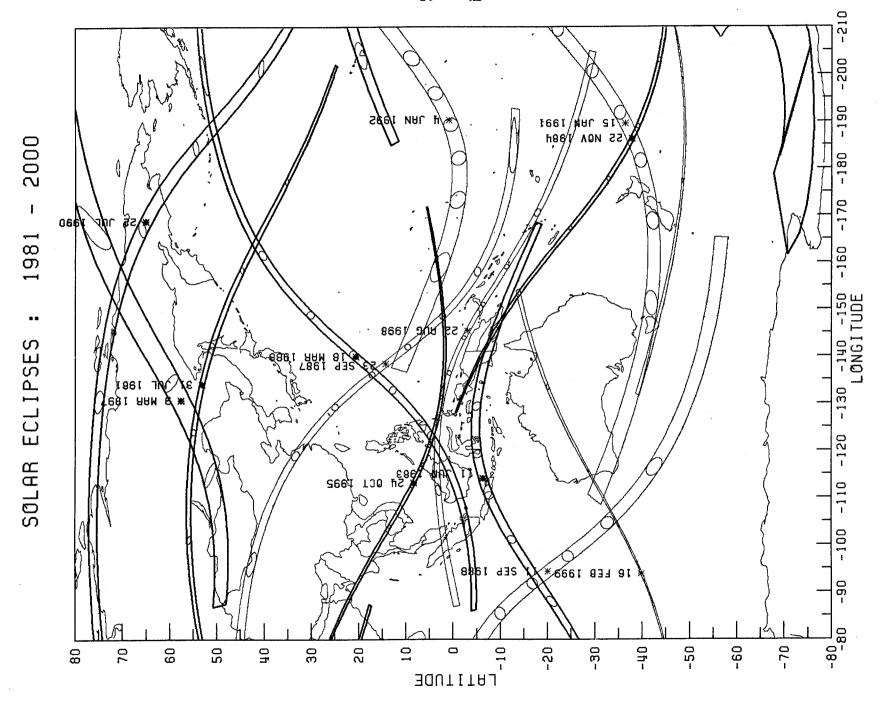
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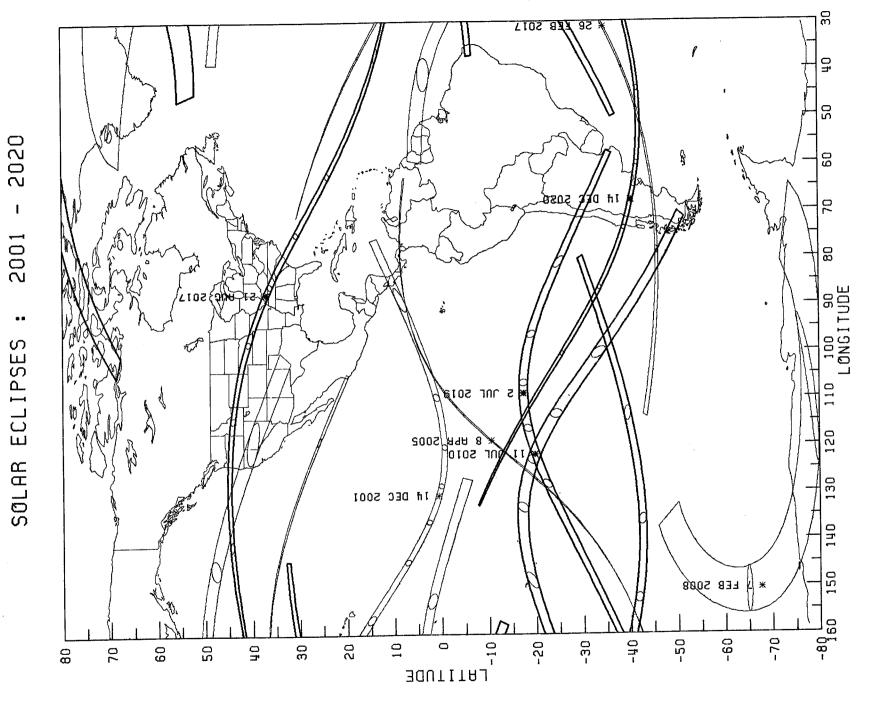
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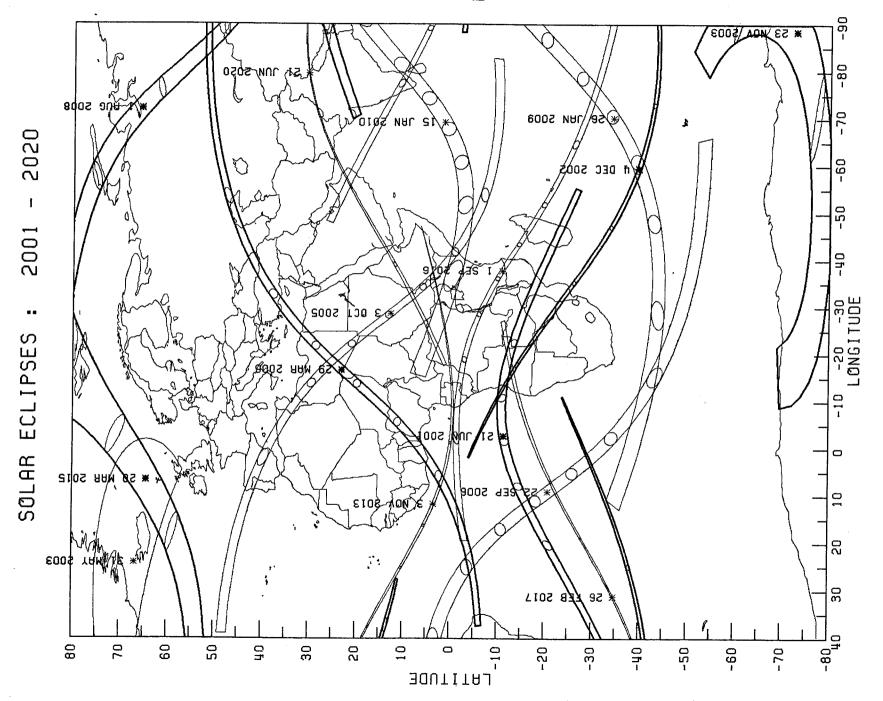
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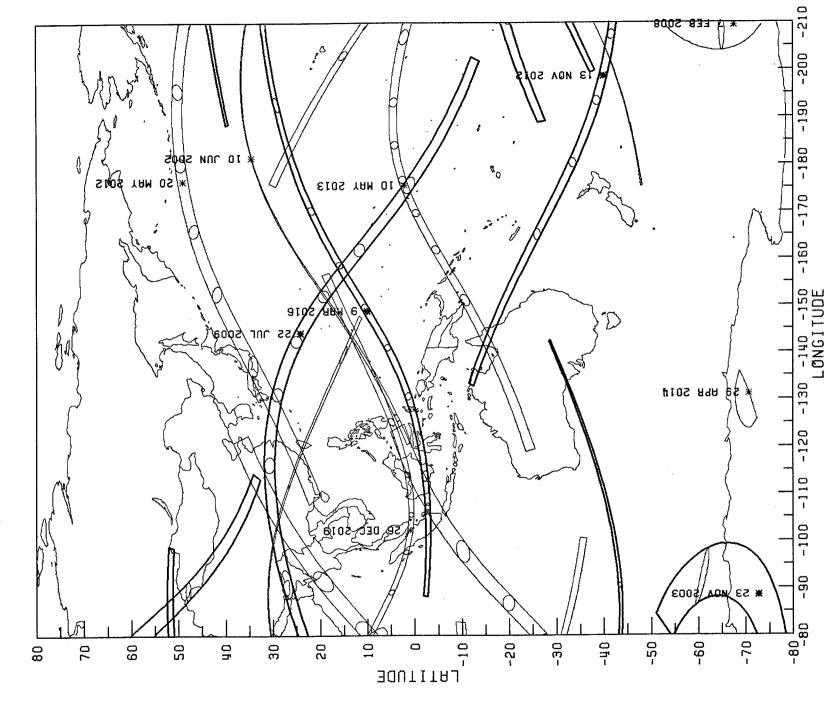
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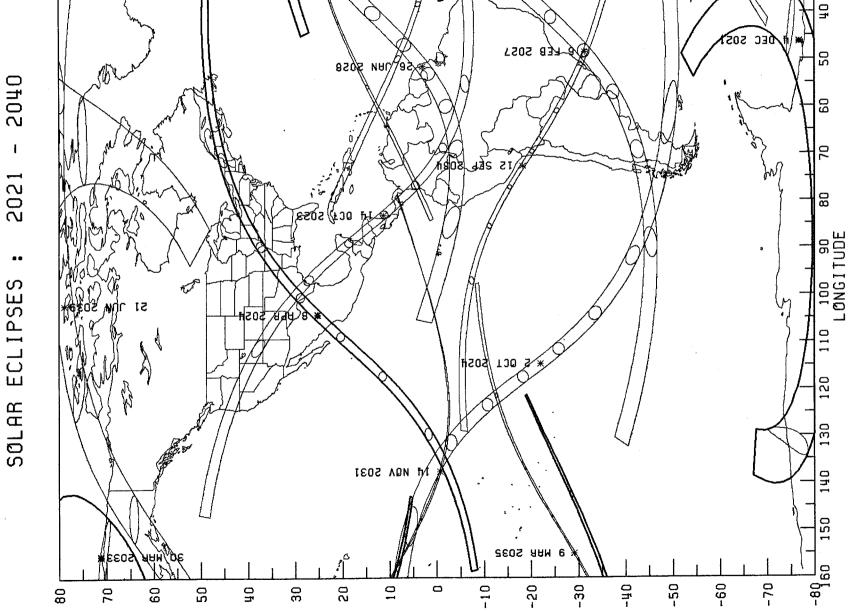








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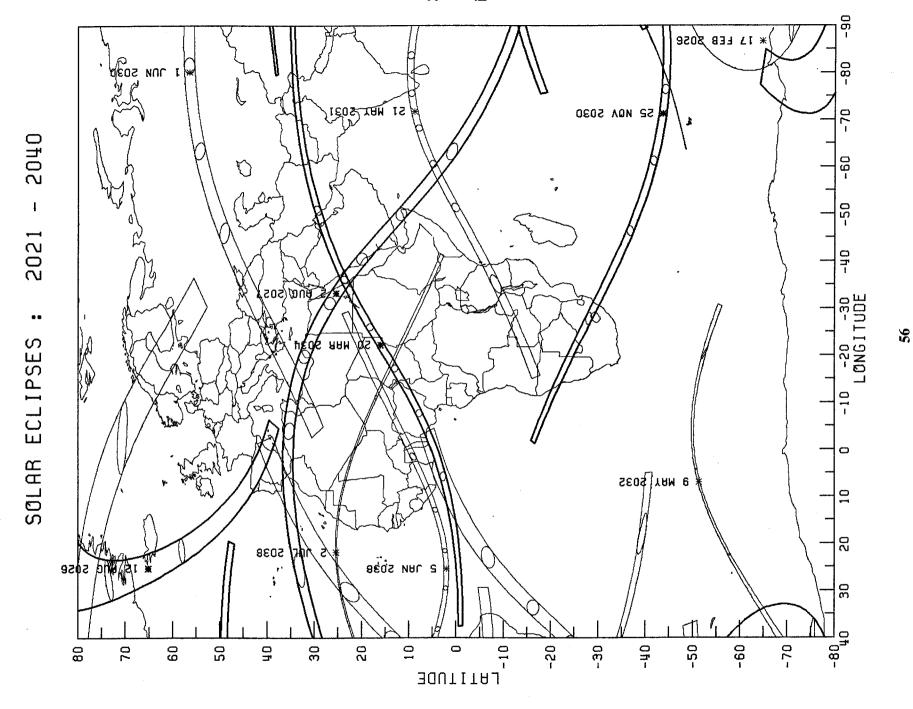
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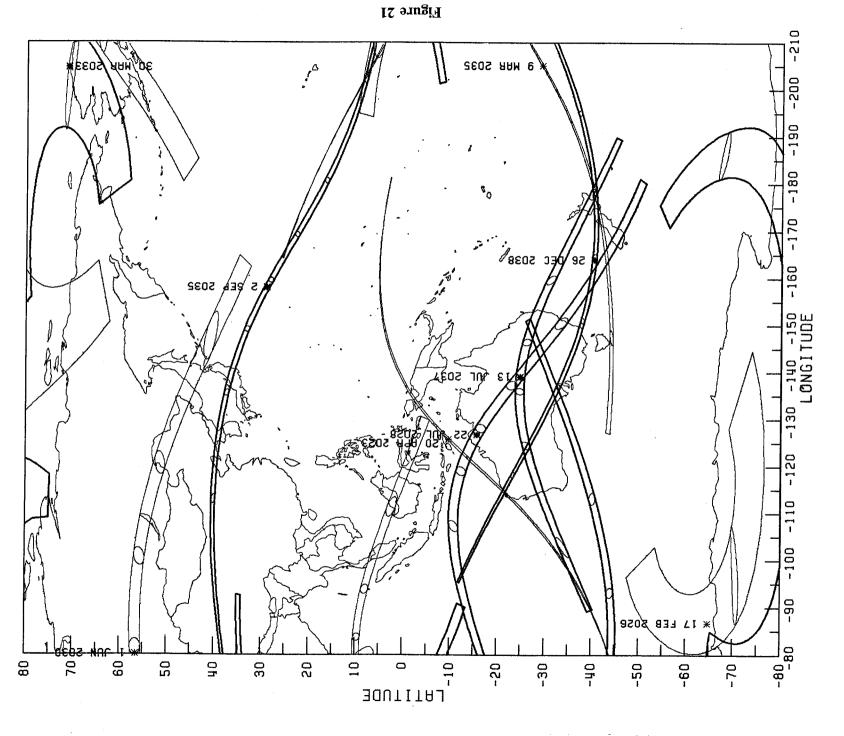
Figure 19

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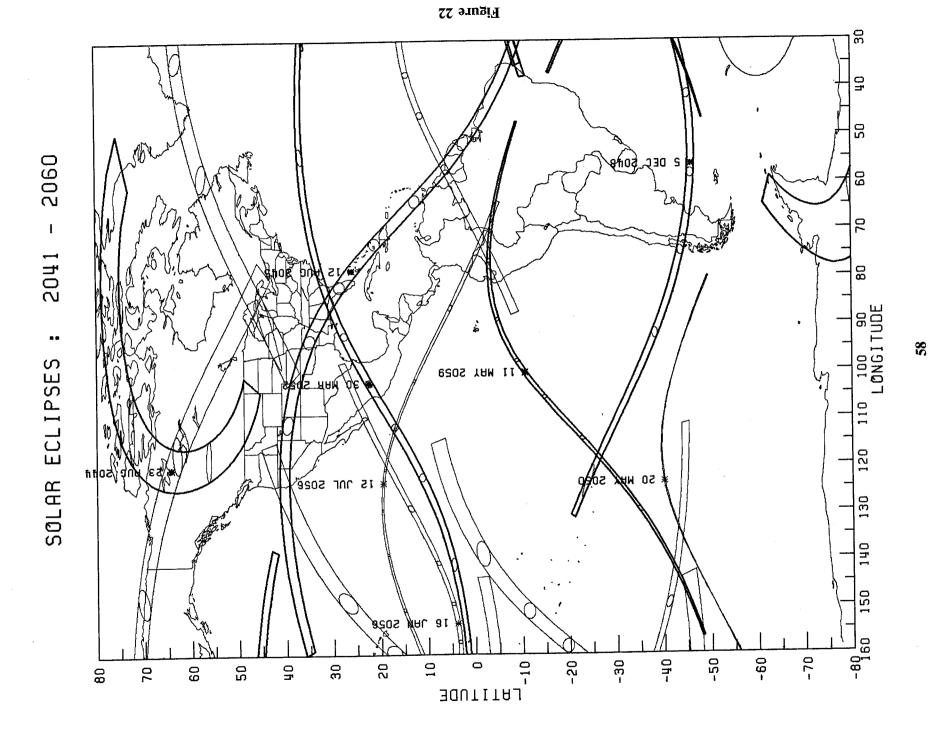
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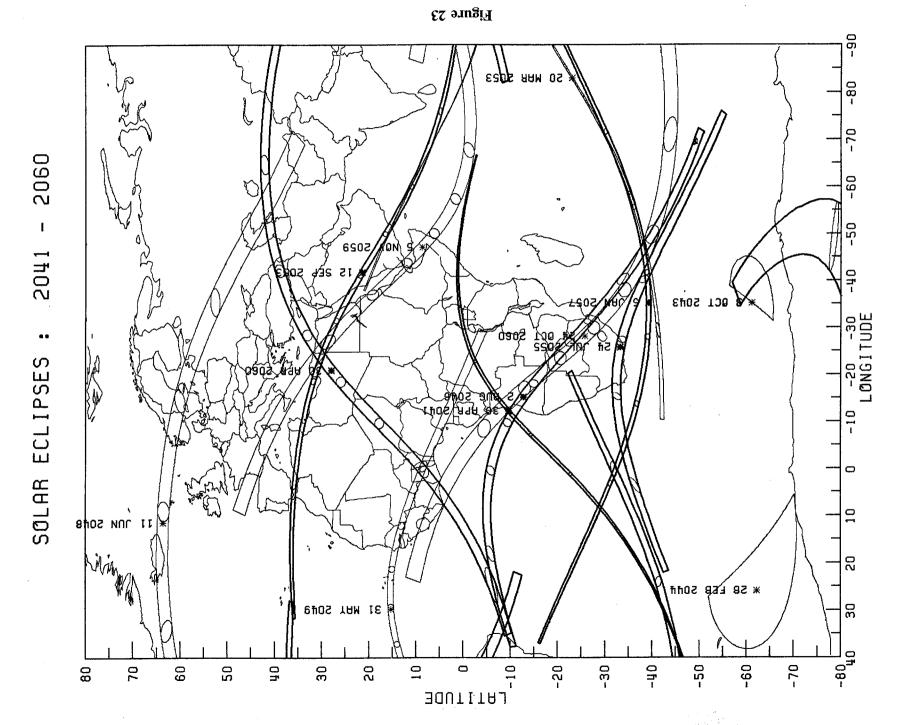
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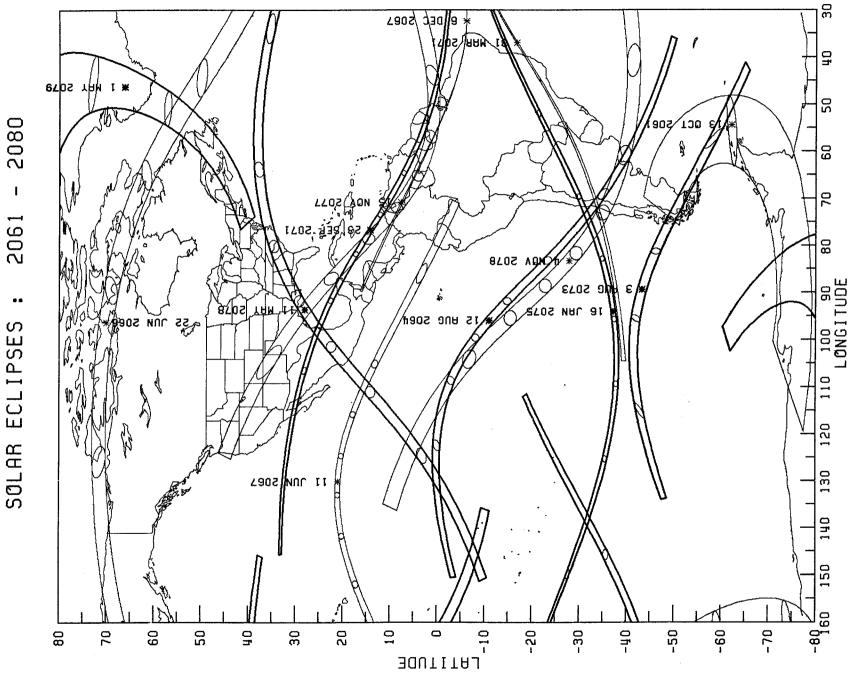
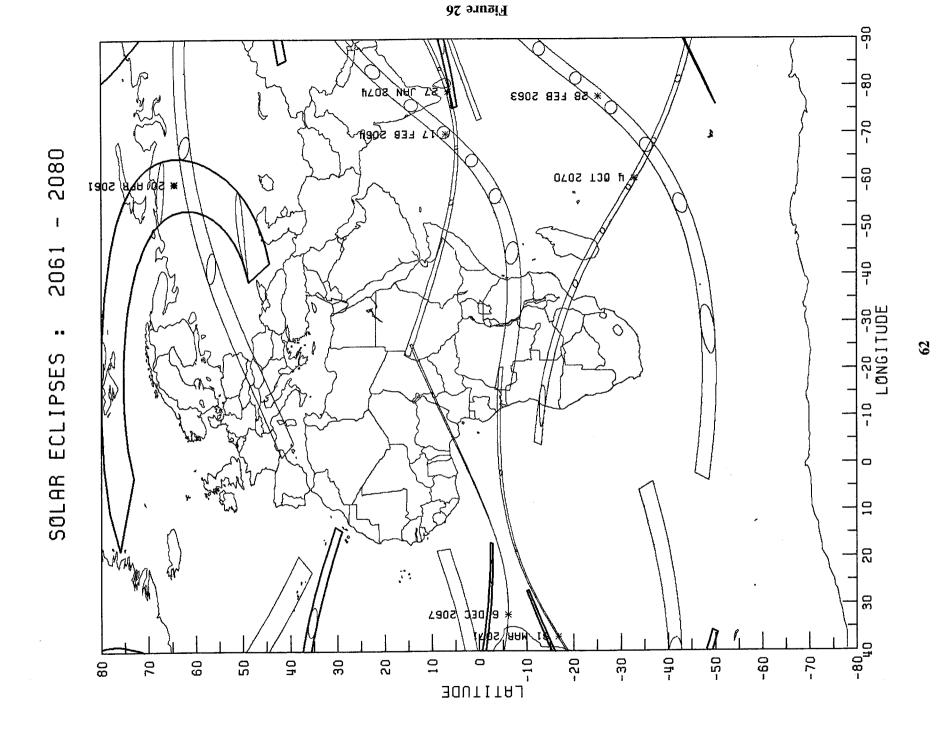
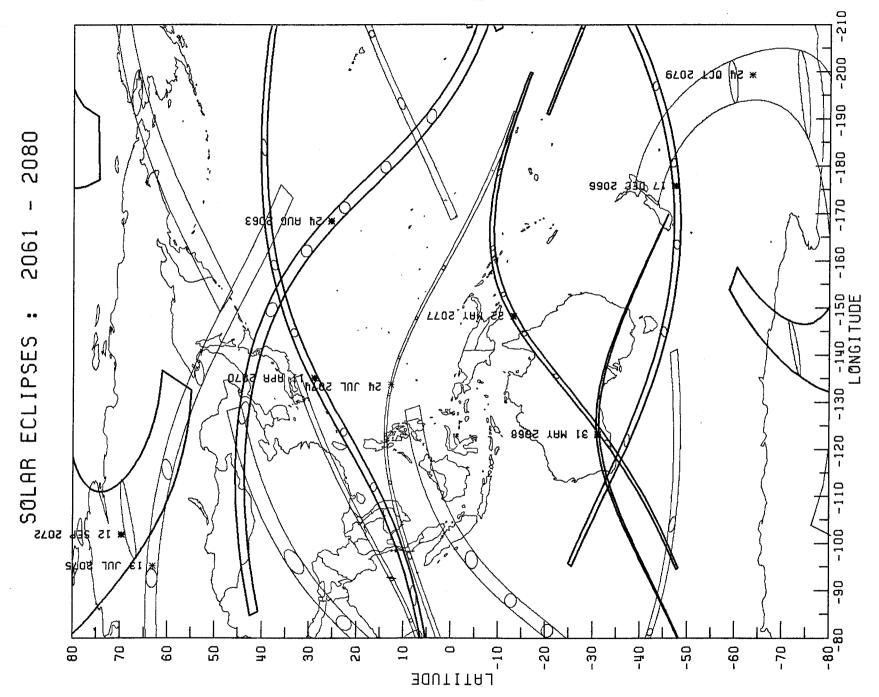
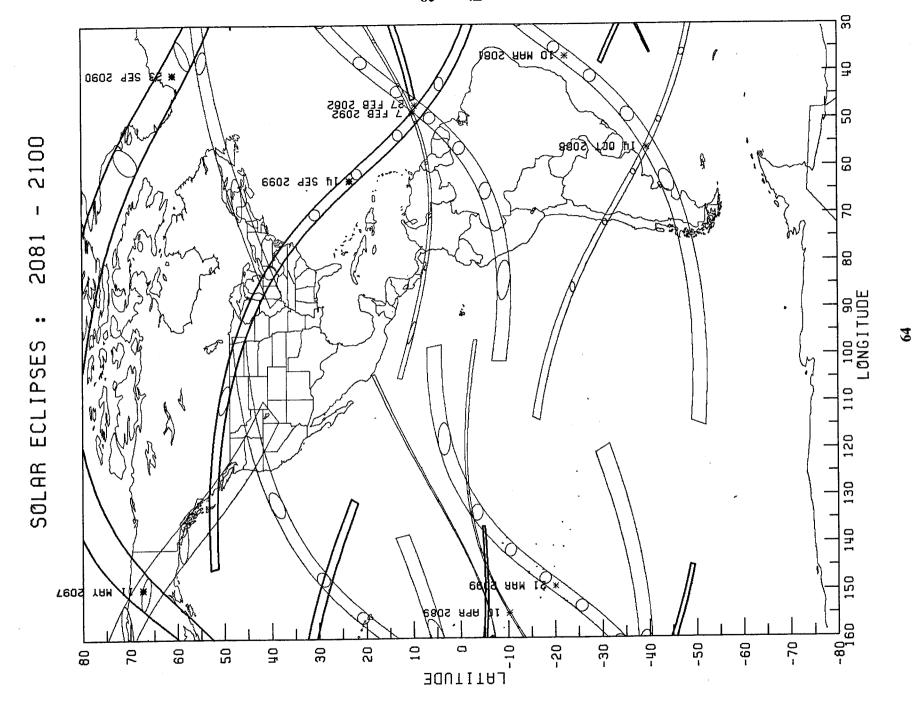
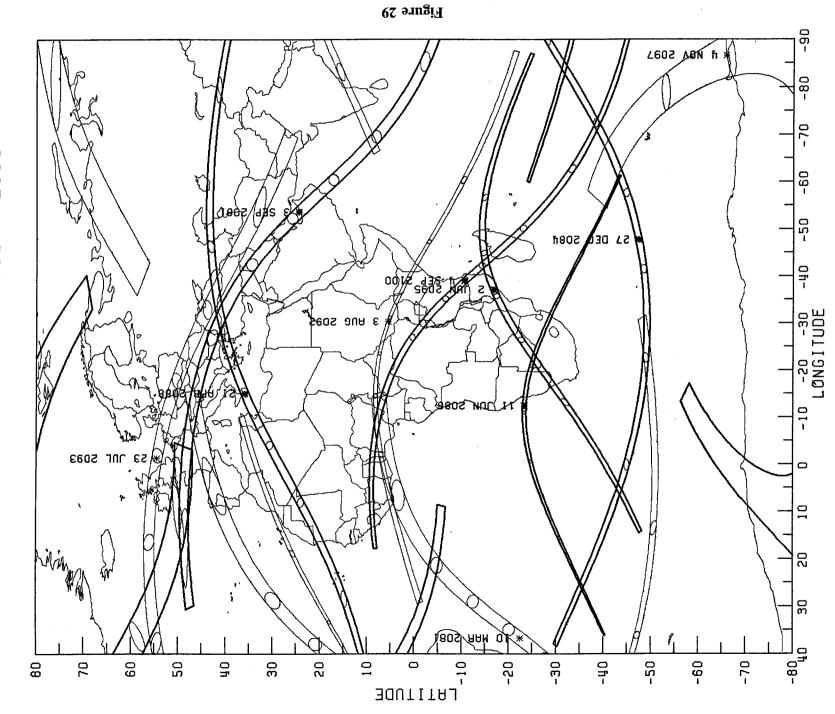


Figure 25









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FIFTY YEAR CANON OF SOLAR ECLIPSES: 1986 - 2035

SECTION 3 - CENTRAL PATH CATALOG: 1986 - 2035

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# Table 13

188F	120	8	HΩ	ECLIPSE	SOLAK	TOT\NNA

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6.0 :0 2.0 :0 0.0 :0 11.0 :0 12.0 :0 12.0 :0 11.0 :0	2.5 4.5 2.2 2.3 2.3 2.3 2.3 1.8	261.9 261.7 261.9 262.8 262.8 262.9 263.3 263.3	7.024655642	8666.0 8666.0 9000.1 1000.1 1000.1 1000.1 6666.0 6666.0 8666.0	5.11 98 6.11 48 6.8 78 6.81 78 7.12	9.7 83 6.8 63 7.8 63 7.	3. 81 88 3. 44 88 3. 44 88 6. 82 78 8. 42 78 8. 42 78 8. 42 78 8. 42 78 8. 83 88 8. 83 88 8. 83 88 8. 83 88	6.64 28 6.64 28 6.68 88 6.68 88 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	5.8 85 5.85 85 5.85 85 5.85 75 6.82 75 6.82 75 7.52 75 7.52 75 7.52 75 7.53 75 7.54 75 7.54 75 7.54 75 7.54 75 7.54 75 7.55	3.13 23 3.13 23 3.5 83 3.5 83 3.5 83 3.5 83 3.5 83 3.5 83 3.7 83	\$ :61 \$ :61 \$ :61 \$ :61 \$ :61 \$ :61 \$ :61
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TY.8:0 T8.3:0 T3.4:0 T0.1:0 T0.1:0 T.0:0 S.5:0 T.8:0 P.9:0	8.5 8.5 6.1 6.0 7.0 8.4 7.2 8.4 7.3	303.08 303.08 295.7 280.5 277.2 277.2 272.5 272.5 272.5	0.13 0.13 0.13 7.83 0.13 7.83 0.13 0.13 0.63	2100.1 8000.1 8000.1 8000.1 8000.1 8860.0 8860.0 1860.0	3.7- 0 3.74-2- 3.74-2- 3.74-2- 9.11-4- 9.98-3- 9.21-7- 7.98-01- 7.98-01- 8.34-41-	6.72-6- 6.32-7- 6.32-8- 7.73-4- 8.62-6- 7.36-0 7.36-0 8.41 2 8.41 2 8.42 8	8.85-1- 8.25-1- 2.74-2- 3.11-4- 3.11-4- 3.65-3- 3.66-31- 3.	2.72-6- 2.6-26.2 2.6-67- 2.6-67- 2.6-67- 2.6-67- 2.6-67- 3.6-6	4.8- % 4.72-1- 5.82-2-4.72-1- 6.82-2-4-38-38-38-38-38-38-38-31- 7.44-41-41-41-41-41-41-41-41-41-41-41-41-4	7.82-6- 3.73-7- 5.72-8- 6.83-4- 6.82-8- 0.32-3- 7.08-0 7.08-0 7.08-0 7.08-0 7.08-0	\$ : \$1 \$ : \$ : \$ : \$ : \$ : \$ : \$ : \$ : \$ : \$ :
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### ANNULAR SOLAR ECLIPSE OF 23 SEP 1987

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8.88:8	8.691	275.5	ε.εε	9739.0	6.83-581-	8.4- 8-	Ø.81-881-	E. 7E-8-	£.8E-49I-	8.1E-Y-	24:4
8.88:8	4.88I	2.572	1.88	3836.0	Ø. 54-091-		3.4- 09I-		8.12-191-	I.4- 8-	98:4
3.40.5	5.531	8.472	4.24	4636.0	1.0- 831-		4.82-731-		£.78-831-		Ø8:4
					9'68-991-		0.4- 88I-		-156-15.3		42:4
6.14:E	160.3	Ø. 472	4.34	1096.0			0.I- 83I-		1.01-431-		81:4
1.54:5	167.6	8.272	ø. ø3	700.0	-163-35.4				1.81-231-		71:4
1.44:5	1.431	2.172	4.63	2196.Q	-121-44.2		9.01-131-		7100 007	0.01.1	9:1
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3.64:8	137.2	8.112	8.67	4896.8			9.84-8£I-		E.84-7EI-		9:8
4.64:8	7.8EI	a. ras	3.57	££86.0	3.81-781-				3.86-361-		ğ : E
3:49.5	136.5	7.0er	8.27	2889. Q	8.8- 881-	8-81 71	5.75-351-	2 83 81	3 96 961	8 26 21	
8.64:8	136.5	<b>₽.</b> 181	3.17	1896.Q	-134-62.9	18 46.3	-134-53.5	18 22.3	-132-55.6		2:54
7.64:8	7.8EI	£. £71	8.69	6296.8	1.88-881-	8.91 QZ	8.8- 881-	Ø:39 6T	9.3- 461-		84:2
7.64:8	2.781	Z.881	T. 78	7286.8	5.31-251-		Z.84-IEI-		9.44-261-	2.91 22	24:2
8.64:8	9.78I	Z.09I	4.39	4286.8	7.64-0EI-		7.02-0EI-		8.81-161-	23 65.2	2:38
	9.881	154.9	8.28	0296.0	9.71-921-		1.84-821-		8.84-621-		8E:2
3.64:8			I.08	7196.Q	3.86-721-		1.01-721-		1.7- 821-		₹3:2
2.64:8	140.2	120.3					-125-21.9		Ø.81-921-		81:2
8.84:8	8.141	1.841	1.73	Z196.0	8.64-221-				2.71-421-	1.20 00	2:12
8.84:8	143.6	2,241	Ø.43	T@86.@	7.64-621-		-123-22.4		8.1- 221-	7 00 DC	8:2
<b>3.</b> Υ₄: ε	146.8	138.5	9.03	1096.0	-121-35.3		9.8- ISI-	8.11.18			Ø : Z
8.84:8	148.4	8.481	Ø. TA	₽636.0	6.S- ell-	4.72 EE	6.7E-8II-	1.63 SE	1.82-011-	9 1 PE	ю ·с
3:45.6	121.4	1.181	1.54	7836.0	E.T- 811-	1.81 38	2.44-311-	9.88 AE	4.08-311-	8.64 38	1:24
3.44.8	Ø.331	2.721	6.88	8736.8	6.04-2II-	6.0 78	8.02-211-	9.12 88	6.8- EII-		8 <b>†</b> :I
3:42.5	£.631	9.221	3.48	7836.8	8.1E-8@I-		1.81-801-	3.8 9.2	7.84-801-	8.88 98	7:45
3.04:8	7.481	Ø.811	8.82	4339.Q	Ø.81-801-		1.01-501-		8.42-EQI-	41 30.3	1:38
	8.171	8.111	1.22	8839.8	7.81-86-		3.02-96-			8. QE E4	Ø€:I
2.78:8								6.24 E4	å. 9£-£8-	Ø. 35 34	1:24
8.28:8	183.3	102.5	12.5	£136.8	£.04-48-	2 88 77	0 10 10	• • • • • • • • • • • • • • • • • • • •			
8.82:8	1.661	1.06	ø.ø	1846.Q	£.0- 89-	45 33.6	9.03-79-	6.68 44	1.18-78-	4.72 84	STIMIL
YTIAAJUNAA	HTGIW	Z∀	TJA	OITAЯ	LONGITUDE	<b>AUTITAL</b>	LONGITUDE	<b>BULTITAL</b>	LONGITUDE	<b>BULLITA</b>	LIME
NOITARUG	HTA9	NOS	NOS	RETER	TMTT V	31122	N LIMIT	שטוטפ	ITWT7 N	ИОВТНЕВ	UNIVERSAL
					R LINE	コエルコン	TTMT I M	63HTI 103		33,123017	
55.8 Sec	= T st!	Del								1	SAROS 134

Ø.88:1	7.801	<b>₽.</b> 892	ø.ø	1.0295	8.78 241 3.8 43	53 34.4 142 20.4	54 33.5 142 11.5	LIMITS
7:19.4 1:58.3	129.2 129.8	240.2 253.4	8.12 5.11	1.0330 1.0330	49 56.5 175 23.9 52 45.9 168 37.6	49 14.3 175 41.5 52 2.8 161 50.3	8, 8 37 1 8, 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	3:24 3:30
8.45:S	Ø.381	Ø.282	7.82	7850.I	9.01-871- 8.12 TA	4.11-871- 8.04 84	2.21-871- 2.8 84	3:18
Ø. 94: S	9.6EI	225.6	3.48	7680.1	1.6- 871- 8.33 AA	3.61-071- 0.81 44	7.63-631- 2.88 34	3:15
2:56.2	143.4	1.022	6.88	0140.1	2.72-381- 1.78 SA	41 28.4 -165-44.1	43 16.3 -165-11.Ø	3:6
3: 5.2	7.841	215.Ø	1.54	1.0420	9.86-181- 1.45 @4	39 46.5 -161-58.3	8.31-151- 1.5 14	3: Ø
8:13.Ø	7.641	0.0I2	6.94	1.0429	38 15.8 -158-22.4	2.74-831- 2.68 78	38 52.8 -157-57.9	5:24
8:19.9	152.3	205.1	5.03	1.0436	8.46-33I- 7.II 88	9.1- 881- 0.86 38	3.7- 331- T.74 88	2:48
3:25.9	164.8	ø.øøs	53.4	1.0443	0.8- 531- 1.11 45	33 36.2 -163-35.3	34 46.2 -152-36.8	2:42
3:31:1	1.731	9.461	1.93	8440.I	32 13.6 -150 63.0	8.62-131- 4.66 18	\$2.22-\delta = 150-22.3	2:36
3:36.4	129.2	8.881	9.83	1.0453 1.0453	1.0- 741- 4.82 82 9.13-841- 8.81 08	27 53.6 -147-33.1 29 45.3 -149-24.0	28 69.5 -146-27.1 30 62.5 -148-19.9	7:24 ∑:30
1.68:8	2.191	182.5	3.28 7.08	9340.I	26 36.3 -145-15.5 1 2- 145-15.5	1 65-711- 9 53 79	8.14-441- 8.8 TS	2:18
2.44:8 8.24:8	8.43I 1.631	168.2 175.6	8.88	2940.I	24 48.1 -143-36.4 3 31-311- 5 95 90	24 16.2 -144-10.9	8.1- 541- 1.02 32	21:2
3:45.6	8.881 8.881	8.09I	7.48 9.58	5940.I	8. I- S4I- 8. I 82	5. 36-241- S. 85 . 25	23 33.2 -141-2.85 S2	8:5
3.46.4	1.881	1.521	2.33	4840.I	9.82-041- 7.81 IS	20 45.6 -141 -4.4	5.63-951- 0.84 IS	ø : z
V 3V.E	1 091							
4.84:6	3.691	6.E41	1.39	1940.I	1.83-821- 6.66 91	19 2.5 -139-34.0	1.22-138-22.1	1:24
3:45.8	8. \\ \T	6.381	64.5	1.0464	7. 72-781- 1.13 71	9.6- 8EI- 3.02 TI	18 21.8 -136-51.3	1:48
4.44:8	Ø.STI	128.5	63.5	1.0462	3.83-351- 1.01 SI	1.66-861- 7.66 31	16 40.6 -135-20.0	1:42
3:42.4	9.271	7.121	ø.58	0940.I	8.52-134-2.05 41	3.0- 381- 6.63 81	0.74-851- 8.0 BI	98:I
3.88:8	173.5	116.7	1.09	1.0458	12 51.2 -132-48.1	12 21.0 -133-25.0	0.11-251- 4.12 EI	ØE:I
0.88:E	8.571	3.011	6.73	1.0454	Ø:8- IEI- I:EI II	1.34-161- 0.64 01	8.08-081- 2.84 11	1:54
9:18:8	7.871	Ø. 90I	8.23 4.33	1.0445 1.0450	7 69.2 -127-29.8 9 35.8 -129-22.3	4.8- 811- 2.82 7 6.63-621- 7.8 6	8 29.3 -128-61.3 10 5.9 -128-44.8	1:18 1:18
3:26.4	Ø.ETI	2.201	8.64 3.03	9840.I	8.23-721- 4.62 8	5 53.4 -126 -3.5	6.54-42.9	9:1
3:20.4	9.171	≱.8e \$.ee	45.8	1840.1 0510 !	0.0I-82I- 2.84 4	9.74-123- 2.81 4 3.5-251- 1.53 3	7.18-221- 0.81 d	ø:t
4.81:8	1691	V 90	8 37	1 6431				
3: 5.4	166.4	2.46	6.IA	1.0423	2.78-02I- 8.8I E	3.31-121- T.EA S	3.83-911- 4.64 8	<b>₹9:</b> Ø
2.83:2	162.2	92.5	9.7£	1.0415	4.14-711- 7.98 I	4.02-8II- 0.0I I	8.1- 711- E.9 S	84:Q
9.34:2	126.6	2.19	7.28	ØØÞØ.I	A.SI-AII- 8.8 0	8.22-411- 6.22-8	3.18-811- 9.38 @	24: Ø
Ø.88:2	2.641	£.06	8.82	1.0384	2.13-601- 8.32-1-	-1-64.6 -110-34.2	4.7- 601- 8.88-0	98:Ø
1.71:2	8.8££	ø. øe	5.61	7.0362	-2-56.7 -103-50.3	-3-24.2 -104-40.1	-2-27.5 -1Ø2-58.7	ØE:Ø
9.64:1	2.611	3.0e	5.3	eien.i	0.81-19- 4.91-4-	6.31-69- I.TA-A-	8.81-88- 8.13-6-	\$2:8
1:40.5	212.3	6.06	ø.ø	I.øsø2	8.81-88- 8.52-4-	-4-52.5 -86-1Ø.5	7.83-38- 3.13-£-	LIMITS
YTIJATOT	WIDTH	Z∀	TJA	OITAR	LATITUDE LONGITUDE	LATITUDE LONGITUDE	LATITUDE LONGITUDE	TIME
VII IATOT	HTA9	NOS		DIAMETER				ONIVERSAL
HOTTAGIN	HTAG	MIS	14112	77411144	CENTER LINE	SOUTHERN LIMIT	NORTHERN LIMIT	HOUSER

SAROS 139

VANOLAR SOLAR ECLIPSE OF 11 SEP 1988

4.62:3 5.418 0.972 0.0

5:43.3	£.062	6.762	2.41	4826.0	9.31-2+1-	#:1- cc-	5.24-441-	6:9- 99-	9.68-041-	*'6I-I9-	6:24
0.88:8	0.872 5.800	8.70E	8.22	8089.0	8.65-151-		4.8- 28I-	T'66-16-	-131-23.5		81:9
							-124-56.3		8.71-821-		ZI:9
4.8 :8	S. &YS	3.418	1.82	7159.0	-125 -4.2				7.24-021-		9:9
1.81:8	264.5	0.02E	9.28	7289. à	9.41-021-		4.64-6II-		2.4- 7II-		ø : 9
7.61:8	2.092	8.428	Ø. Υε	9889.Q	7.72-811-	3.72-24-	0.23-311-	T.88-84-	2 M- 711-	7 81-11-	ט יט
4.32:9	6.832	8.628	7.04	£456.0	8.12-811-	Z.8I-04-	<b>₽.</b> 68-211-	9.42-14-	4.8- AII-		<b>2:2</b>
3. <u>8</u> £:8	254.3	3.555	Ø. 44	6459.8	8.54-QII-		8.73-601-	8.71-68-	9.62-111-	7.41-78-	2:48
Ø.35:8	252.3	8.755	Ø. 74	9986. g	8.72-80I-		0.68-701-		0.81-601-		27:9
6.88:3	2.030	1.248	8.64	9359.8	8.72-801-		2.78-301-	Z.12-66-	Ø.81-701-	1.62-88-	2:38
			8.23	£856.8	9.04-40I-		7.84-EQI-		-106-32.1		98:3
4.24:8	0.032	3.848					4.01-201-		9.33-EQI-	8.88-8Z-	2:54
3.34:8	9.642	351.2	8.43	788. Q	4.8- EQI-				8.72-201-		2:18
2.84:8	8.642	326.1	3.83	6986. Q	I.48-10I-		E.04-001-				21:3
3.03:8	1.032	Þ.I	1.83	2729. ®	0.11-001-		9.91-66-		8.4- 101-		9:3
6:52.5	6.032	Ø.T	8,63	₽789.@	7.23-86-	4.64-32-	6.73-76-			2.2- 32-	
6:54.1	2.232	12.9	T.08	3759.@	2.88-76-	0.41-42-	6.24-86-	9.1- 32-	6.28-86-	8.72-82-	ø :9
6:55.4	6.832	ø:6I	3.13	9759.Q	4.82-86-	7.04-22-	7.0E-36-	7.72-82-	9.12-76-	6.43-12-	4:24
4.83:8	Ø. 832	25.3	9.13	8759.8	3.81-86-	Z.e- IZ-	5.02-46-	-21-55.9	Ø.2I-86-	8.62-02-	87:7
0.73:8	4.832 258.4	7. IE	Ø. 29	7759.8	8.7- 46-	9.68-61-	0.11-59-	9.32-82-	3.8- 38-	-18-64.3	ZÞ: Þ
						4. II-8I- 3 05 01	9.I- 29-	6.73-81-		5.82-71-	4:36
5.57.2	261.3	0.8£	8.13	87.59.0	Ø:69-26-			3. IE-YI-		7.63-31-	4:30
1.73:8	4.482	Ø. 44	2.13	3789.0	6.64-16-	6.44-8I-	6.23-06-		• • • • •	5.45-41-	42:4
8.56.6	6.782	8.64	S. 08	4789.Q	8.68-06-	6.61-31-	£.14-68-	7.8- 81-	0.76-19-		81:4
7.33:8	7.172	1.33	ø:69	£7£6.0	2.72-68-	-13-28.2	<b>▶.8</b> 2-88-	9.54-41-	6.32-06-	-13-1ø.2	• • •
4.43:8	275.6	6.63	4.73	1759. Q	1.21-88-	0.48-21-	3.21-78-	<b>9.12-21-</b>	6.01-68-	4.74-II-	4:15
6:52.5	7.672	8.48	9.33	8986.Q	2.63-88-	11-13-1	7.23-58-	8.1- SI-		7.32-01-	9:1
5.68.2	8.882	2.89	3.53	3986.0	9.62-38-	3.83-6-	®.82-⊁8-	2.84-01-	Z.&E-88-	£.3- 6-	ø : Þ
4.74:8	6.782	9.17	2.13	1986.0	6.63-68-	6.35-8-	1.73-28-	1.82-6-	7.1- 38-	Ø.8≯-7-	3:24
6.54:8 A 71:3	8.162	3.47	9.84	7359.8	8.22-28-	8.81-7-	3.81-18-	9.01-8-	6.32-28-	Ø'8Z-9-	3:48
8.98:9	4.36Z	I.77	7.34	2359.8 7350.8	2.8E-88-	E.E- 8-	I.0E-67-	6.83-8-	Ø. I4-18-	£.11-3-	3:42
						7.64-4-	2.62-77-	6.44-3-	8.44-67-	1.88-E-	3:38
Ø:38:9	8.862	8.67	9.24	9459. Q	7.78-87-			2.35-4-	3.88-77-	3.54-S-	3:30
4.62:9	S. I Ø E	2.18	1.68	6889. Ø	8.62-87-	Ø.8ε-ε-	-75-12.3		8.2- 37-	8.1E-1-	3:24
8.22:8	9.60E	7.28	8.35	2889. ®	4.64-87-	8.82-2-	3.55-27-	0.82-E-			31:5
6:15.1	305.3	6.58	e.ae	2228. Ø	0.84-07-	-1-22.2	9.62-69-	-2-24.3	0.3- 27-	6.12-0	3:12
6:3:9	8.808	8.48	7.32	Ø166.0	-66-58.3	6.61-8	<b>-</b> 62-24.4	<b>▶.</b> 32-1-	7.82-88-	8.84 Q	
6:54.3	2.8&£	<b>₽</b> .38	2.91	3626. Ø	Ø:09-19-	⊅.38 @	₽.03-63-	9.35-Q	0.8E-E9-	4.84 I	9:8
5:36.2	3.118	8.38	9.8	6926.0	8.04-23-	9. ØI I	Ø.43-84-	8.42-Q	9.43-33-	7.62 S	9: Ø
6:23:9	9. <b>Þ</b> IE	9.38	ø.a	6+26.0	<b>7.6- 3</b> 4-	I.43 @	7.31-44-	£.8E-@	7.04-44-	2.71.2	LIMITS
6.03	9 F16	9 JO	<i>v v</i>	0700 9	, 0 1,	. 73 2	U 11 //		,		
YTIAAJUNNA	нтаім	Z∀	ΤJA	OITAR	LONGITUDE	3/017177	LONGITUDE	TVITIONE	LONGITUDE	<b>EAUTITAL</b>	TIME
DURATION YITAA	HTA9	NOS	NUS	DIAMETER	EGITTONO I	SQLITTTA 1	70117TO140 1				NNIVERSAL
					R LINE	CENTE	N LIMIT	SOUTHER	N LIMIT	иовтнев	
56.4 Sec	= T st	Del									SAR0S 144
		-									

LIMITS -56-16.4 -165-20.2 -58 -7.7 -165-15.0 -56-35.4 -164 -3.6 0.9250

											•
4.4 :2	6.864	243.3	ø.ø	9296.0	8 22.3	2.14-84-	6.4 A	4.28-94-	4.04 8	£.8- 84-	LIMITS
				L+00:0	1.21 91	-25-54.4	8.61 3	ø. ø3-e4-	נינג נג	9.84-63-	z :øz
2: 3.5	2.184	8.642	2.8	4496.0				8.3- 53-	3.78 22	1.8- 88-	ø :øz
8.8 :2	471.5	8.132	ø. øt	6496.Q	8.0 81	9.32-43-	11 25.5	8 3- 53-	3 22 E	1 3- 33-	טשי ש
I.8 :S	461.5	3.532	4.11	£396.0	19 22.6	1.84-33-	1.84 81	2.13-43-	6.04 ES	£:61-99-	18:61
6.2 : S	451.6	255.1	12.6	9996.8	I.82 02	1.3- 73-	16 24.4	6.0Z-83-	24 34.4	3.0E-73-	<b>18:2</b> 8
			3.61	8396.8	21 21.2	4.8I-83-	16 35.6	4.24-73-	Z2 ZQ:7	<b>₽.88-83-</b>	79:6T
8.2 :2	442.1	2.66.5			22 4.4	Ø.62-63-	0.05 TI	8.83-83-	25 58.3	9.84-63-	Z9:6I
7.2 :2	0.884	8.732	14.5	1996.8			3.11.81	8.II-@9-	8. 8g. 92	-6ø-52.3	Ø9:61
7.2 :2	454.6	Ø.632	15.3	£986.0	2.68 22	8.78-08-				0.73-18-	87:61
9.2 :2	416.5	I.092	6.3I	₱996.@	7.8 ES	8.44-18-	18 42.3	-61-22.1	8.73 82		
8.Z : Z	Z.604	1.192	3.81	9996.Q	₽.72 ES	4.03-28-	8.E et	9.0E-29-	8.91 TS	6.0- £8-	97:61
2: 2.6	482.5	1.292	Ø. TI	1996.0	23 41.6	1.33-58-	3.81 91	A.7E-E8-	₽.88 TS	Ø.4- 48-	79:6T
8.2 : S	≯.8e£	ø. £32	4.71	8996. Ø	23 49.3	1.63-43-	ø. 12 et	1.84-43-1	2.84 T2	T.8- 38-	79:6T
			7.71	6996.8	23 50.5	3.2- 88-	Ø. TI el	8.74-39-	8.43 TS	Ø.6- 88-	ØÞ:61
8.2 : S	6.0e£	8.63.8	2 21	0990 9	2 22 50	1 0 00	2 21 01	0 2. 20	• • • • • • • • • • • • • • • • • • • •		
8.2 :2	1.985	2.492	Ø.81	6996'Ø	8.44.8	₽.3- T8-	£.4 eI	8.13-88-	2.83 72	Ø.11-78-	88:6I
			2.81	6996. Q	8.18 £2	ø.8- 88-	18 42.4	8.43-79-	8.13 72	6.21-89-	98:6I
7.2 :2	381.8	265.1			8.01 52	Z.@I-69-	E. 01 81	£.73-88-	I.IA TZ	9. PI-69-	18:34
7.2 :2	2.878	8.382	18.3	@799.@			9.82 TI	2.63-69-	8.82 T2	E.81-07-	78:61
8.2 :2	1.378	582.9	4.81	@786.@	7.04 22	1.21-07-					ØE:61
8.2 :2	7.278	1.882	4.81	@78e.@	8.0 SS	8.51-17-	9. أ 9I	4.0- IT-	9.73 82	0.81-17-	
6.Z : Z	8.0Y£	1.882	£.8I	6996'Ø	8.7 12	6.3I-2T-	£.61 31	0.1- 27-	₽.22 82	T. 61-27-	19:28
ø.g :2	3.698	8.392	2.81	6996.0	0.1 0S	3.81-67-	13 EQ.4	8.0- ET-	ZE 36.1	-73-21.5	<b>18:5</b> 8
2:3.1	8.888	265.3	Ø.81	8996.0	Ø. 78 81	2.71-47-	12 Ø.4	₽.63-ET-	4.88 42	£.£2-₽7-	78:St
		264.4	8.71	8996.8	1.23 91	4.71-87-	1.34 6	7.83-47-	I. ØZ EZ	1.32-37-	19:22
2.8:2	7.888			788.0	I. [4 4]	7.81-87-	1.63 8	0.23-37-	21 43.2	7.82-87-	ØZ:61
8.8 :2	8.698	1.692	3.71	7990 M	LIVVI	2 81 82	1038	D 01 12	0 07 10	2 00 02	20 01
3.8 :2	3.075	2.192	I.TI	9996'Ø	1.73 11	3.41-77-	7.38 E	3.44-87-	1.04 91	8.72-77-	81:61
8.8 : 2	3.272	7.832	7.81	4996. Ø	8.88	E.QI-87-	Ø.εε−@	1.88-77-	ø.ε TΙ	2.82-87-	91:61
	3.375	255.4	1.91	2996. g	8.71 A	6.2- eT-	6.35-3-	Ø.81-87-	8.I4 EI	1.72-67-	<b>⊅</b> I:6I
7.8 :2			3.31	1886.8	1.2-1-	7.03-67-	6.88-11-		6.12.6	-80-23.5	ZI:6I
9.8 :2	<b>6.87</b> £	250.9				2.18-08-	8.74-81-		3 45.4	8.31-18-	ØI:6I
2: 4.1	383.5	2,345	8.41	6996'Ø	2.88-7-	-			6.8 <u>2</u> -£-	4. I - 28-	8 :61
ε.₄ :3	8.688	Ø.8E2	Ø. Þſ	9396.0	<b>7.68-31-</b>	2.1- 18-	5.73-82-				9:61
p. p : 2	≯.96£	3.622	ø.er	£396.@	0.2- 32-	1.81-18-	3.13-38-		1.98-21-	3.86-28-	
7.4 :2	1.304	Ø. ØZZ	6.II	Ø996'Ø	-32-22.®	Ø.11-18-	-42 -2.5	0.88-87-	1.34-62-	6.33-28-	7 : 6T
6.4.2	Ø. 914	210.3	9. ØI		2.48-84-	4.04-08-	2.63-63-	3.41-77-	<b>▶.</b> 6- 8£-	7.63-28-	Z :6I
		2.102	6.8	248e.8	9.74-33-	£.8E-67-	6.62-29-	3.46-47-	7.35-84-	@.32-28-	ø :61
2.8 :2	6.62Þ	6 106	0 0	6780 £	3 27 33	0 00 02	, , , ,				
						+10 O.I	8.I4-88-	0'a- T/-	£.34-08-	0.22-17-	LIMITS
2.8 :2	6.164	185.6	0.0	2296.0	6.8- ET-	4.8- £7-	9 17-99-	8.0- IT-	-94-15	D 00-12-	STINI I
		74	TJA	OITAR	⊒dó LT9N0°	LATITUDE L	ONGTIODE	LATITUDE L	CONGITUDE	LATITUDE I	TIME
NOTTANU . PURATION	HTA9 HTGIW	Z¥ N∩S	NUS T 14	DIAMETER							NNIVERSAL
		• • • • =			FINE	CENTER	LIMIL	SOUTHERN	4 LIMIT	иовтневі	
59.3 Sec	= 1 63	l <del>o</del> (l									SAROS 121
							/700 NN/70N	k 10. /			

ANNULAR SOLAR ECLIPSE OF 26 JAN 1990 Table 18

Table 19

## TOTAL SOLAR ECLIPSE OF 22 JUL 1990

Delta T = 57.6

1:22.3	8.09I	293.5	ø.ø	£720.1	139 24.8	6.8	ø٤	8.32 98	t ø	. QS	53	8.02	138	I.QE	Øε	LIMITS
9.88:1	1.381	2.782	2.11	9050.1	9.4 Ø31	<b>4</b> .8	32	52 23.1	το	. 92	32	1.82	741	4.24	34	8 : 1
7.74: <u>r</u>	£.361	1.582	7.91		9.7 33 <u>1</u>	8.21		9.83 99		ŽΪ	38	2.11	123	3.3	38	<b>7</b> : 7
1:54.6	Z. IQZ	8.672 1.000	7. QZ		158 43.8	Ø. 24		Ø. 42 Øð		. 95		ø.ø	121	2.24	ØÞ	Ø:Þ
														7.00	74	3:56
£. Ø : S	6.40S	8.872	6.52		7.98 191	1.43		3.41 69		. 74		2.2	Ø9T	2.63		
2: 5.3	I.702	Q.ETS	9.92		164 12.5	6.33		2.44 39		42		8.88		8.4		3:62
9.6 :2	4.8QZ	9.692	6.82		166 30.5	£. &3	97	3.0 89		. 7ε		2.83			74	3:48
5:13'2	6.802	2.882	ø. IE	398Ø:I	8.88 881	39.6	87	e. r ar		72		A.T	<b>79</b> 1	8.63		3:44
6.91:2	Ø.602	7.282	8.28	alea.1	6.04 &TI	8.42	Ø9	8.6 27			Ø9	6.6	69T	6.14		3:4Ø
Ø.02:2	8.802	1.632	8.48	AYEQ.I	£.68 SYI	8.3	25	Ø.8 AT	1 8	. 84	23	2.8	171	8.32		3:38
7.22:2	2,882	255.3	7.38	8750.1	0.88 ATI	4.34		6.4 97	τ ε΄	23	23	8.4	173	8.8	<b>79</b>	3:32
2:25.1	9. Y&S	221.4	6.98		Ø. EE 971	2.25		£.2 87	ΪØΊ	. 83	24	Ø.I	<b>11</b> 2	9.34		3:28
1.72:2	7.982	4.742	8.78		7.18 871	2.73		3.83-67		. ØE	99	ø:69	941	8.22	<b>L</b> 9	3:24
8.82:2	8.202	2.542	7.88		1.82-971-			8.33-77	ī- ø	·ž	89	9.0		Ø.83	89	3:2Ø
2.88:2	9.402	8.862	5.95		7.81-771-			0.84-37					-871-	Ø.28	Ø9	3:16
2.31.4	9.882 9.882	2.482	8.68		5.4- 371-			4.88-87				9.68	-921-	8.4	<b>Z9</b>	3:15
2.28:2	6 ZØZ	4.622	I.04		8.04-271-			0.01-17				8.41	-174-	6.38	63	8 : 8
					9.3- 07I-			8.35-89					-171-			3: 4
7.28:2	6.102	4.422	E.04					7.74-38					-891-			ø : E
8.28:2	e.mas	1.912	2.04	1680.1	8.81-781-	. 5 33	38	L LV-38		31	30	2 23	00.		••	
7.28:2	0.002	213.5	1.04	1680.1	8.6- 491-	8.61	<b>L9</b>	2.64-29					-182-			5:56
2:32:3	Ø.661	9. T&S	7.68	Ø68Ø.1	2.14-@31-	42.3	89	3.81-63					-185			2:62
2:31.5	1.861	2. IQZ	3.68	Ø68ذI	Ø.84-831-	. 2.2	Ø۷	6.62-33	I- 6'	<b>1</b> 4°	69		-128			2:48
4.0E:2	2.791	4.4er	3.88	88£0.1	-122-18.2	18.8	īΖ	9'Ø1-19	t- Ø'	. 62	ØΖ		-123-			2:44
Ø.82:2	£.961	6.88I	7.75	9850.I	8.01-741-	. Z. IE	72	1.81-84	t- Ø'	39.	17	4.01	-148-	8.62	73	2:4Ø
2.72:2	195.5	7.871	7.88	1.0384	8.31-141-	. T. TE	73	7.68-84	T- +	43.	72		-1+1-			2:38
2:25.1	9.461	7.691	3.35		1.34-25.1			34-14.4	T- 9	٩b	73	35.6	-134-	Ø.εε	97	2:32
2:22.6	7.591	7.931	I.48		8.12-321-			26-54.6				8.6-	-158	8.12	9L	82:2
7.91:2	8.291	7.841	3.58		0.88-711-			1.75-81				9.91	-911-	6.43	97	2:24
2:16.3	8.191	6.8£I	7.08		I.88-701-			I.42-60				8.22	-102-	7.7	LL	82:2
2:12.5	8.0er	5.421	5.82		3.84-86-	3.6		6.42-66		. SS		6.54		9.33		5:18
2.8:2	9.68I	3.111	2.92		3.35-38-	Δ. 7.E		2.33-88		. 73		3.03		Ø. Þ.I	97	2:12
1.8 :2	1.881	9.86	23.4		8.22-47-	9.3E		1.51-87		. 5		4.01		4.63	7L	8 : 2
2.73:1	1.881	8.88	2.82		0.12-68-	1.73		8. 8E-78	_	42.		54.3		ø. 9	73	7 · 4
0.03:I	5.581	8.47 8.80	Ø. 91		2.02-23-	δ. E.E		8.64-83	-	. 98		3.54		4.02		ø : z
ייבמ מ	5 501	8 72	ש פו	1 0350	0 20 03	ש ככ	W.L	0 0, 01	_	•	~_	2 0.	_,			
1.84:1	2.871	6.18	Z. أ	1.ø312	4.01-04-	8.84	99	6.8- 34	- Þ	. ⊅2	79	8.24	-34-	2.84	99	1:56
	01007	T	~.~	707017	0.12 +2	۲.۵	<b>a</b> 0	8.63-42	_ 0	• 9 T	60	₽.38	-22-	8.51	ag	STIMIL
1:24.9	£.89I	1.74	ø.ø	1.0282	8.72-42 <del>-</del>	4.3	Ø9	9 63-FG	- 8	91	03	7 36	55	3 61	20	OLLITA I
	ate	74	170	OTIV	LONGITUDE	יספי	T 1 W7	NGITUDE	OT 24	10 I T	רעו	3401	гоисі	HODE	TIVT	TIME
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					ant i g	CENTCI		TIMI	NGSI	11 IU		-1	n±,1 N	,		

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VANNULAR SOLAR ECLIPSE OF 15 JAN 1991

8.48:3	₽.998	6.842	ø.ø	9916.0	114 42.4	8.71 Q	7.42 EII	2.83-@	4.8 311	8.03 I	STIMI
	0:050	9.642	9. Þ.I	Ø616.0	126 43.8	7.81 <b>-</b> 8-	7.18 ES1	-6-22.9	Ø. 92 621	Z'69-7-	1:45
9:49:9	6.948			1129.8		▶. <u>I</u> - <u>e</u> -	3.63 ØET	8.0E-6-	135 8.2	6.62-8-	1:38
3.8 : 8	4.688	550.9	23.2			5.53-11-	136 36.6	9.82-21-	3.7 981	9.31-11-	ØE:I
4.91:8	9.288	252.4	29.5	8.9225 8.9225			9.8 esr	1.83-41-	142 18.2		1:24
ø.62:8	8.828	1.432	7.48	9236. Ø		4.81-41-				-16-46.3	81:1
8.78:8	9.12E	Ø.832	2.68	9776.0	143 32.5	-16-28.5	145 1.9	9. QI-7I-	6.63 441		21:1
6:45.9	312.6	1.832	43.4	£326.0	142 60.0	<b>-18-27.5</b>	3.48 441	3.11-61-	147 22.5		
6:53.6	3.018	3.09Z	2.74	6976'Ø	1.81 841	8.71-02-	148 61.9	-21 -3.5	6.18 eal		9 : 1
8.0 :Y	3.885	2.532	7.03	9976'0	7.81 Ø31	E.1- SS-	148 68.4	-22-48°E	7.18 131	2.41-12-	ø:ī
0 0 .7	2 300	0 000		2000	• • • • • • •						
	S.I&E	2.882	0.43	Ø726.8	162 12.Ø	6.88-82-	15Ø 57.2	3.72-42-	163 24.6	-22-5Ø.4	<b>₹9:</b> Ø
7.7 :7			1.73	4729.8	154 2.6	-25-11.4	162 50.5	3.1- 82-	1.21 331	9.12-42-	87:Ø
2.41:7	2.762	7.692		8729.8 A700.8	8.64 33 <u>1</u>	9.65-32-	164 4Ø.Ø	0.18-72-	156 67.4		ZÞ:Ø
2.02:T	293.5	8.872	ø. ø9		367 34.6	4.8-82-	156 27.3	-28-56.4	6.68 831		98:Ø
6.32: <i>T</i>	1.062	2.872	7.28	1826.0	• . •		5.51 831	0.8I-0E-	E.12 091		øs:ø
2.18:7	2.782	283.5	2.39	4826.0	• • • • • • • • • • • • • • • • • • • •	-29-23.5					Ø:24
1.38:7	9.482	7.682	3.79	9826.Q	9.1 19I	0.04-0E-	2.63 ear	Ø.8E-1E-	162 2.4		
3.04:7	8.282	6.862	9.69	7826.@	1.34 S21	9.63-16-	161 45.8	7.03-2E-	0.44 ESI		81:Ø
5.44:7	4.082	305.4	8.17	6826'Ø	1.18 481	7.2- EE-	8.88 EBI	Ø.S- ≯£-	165 26.8		8:15
8. T4: T	6.872	315.3	9. <u>27</u>	6826.0	166 18.5	0.6- 48-	165 24.Ø	6.6- 36-	3.11 731	₽.8- ££-	9 : Ø
	7.772	326.3	3.57	Ø6Z6.Ø	9.8 89I	-36-12.Ø	I.TI TƏI	9.41-98-	7.83 831	7.6- 4E-	ø :ø
4.03:T	L LLG	2 906	3 62	2000 D	0 0 00.	• • • • • •					
		71000	6.57	Ø6Z6'Ø	Ø.S ØTI	9.11-86-	8.EI 69I	6.31-75-	6.84 &TI	8.7- 38-	53:24
4.23:7	8.872	3.888			5.63 171 8.0 871	7.7- 78-	T.AI ITI	8.51-85-	172 42.6		23:48
6.83: <i>T</i>	2.872	35Ø.3	7.87	Ø626.Ø		Z.0- 8E-	3.02 EYI	0.8- 98-	8.04 47I		23:42
9.43:7	Ø.87S	1.2	ø.er	6826. Ø	0. I 47I				2.54 87I		23:36
9.43:T	1.872	12.9	8.17	8826.0	9.7 87I	6.84-86-	8.18 371	<b>4</b> .83-68-			23:38
8.63:7	4.872	8.22	S. &T	9826.Q		7.88-98-		6.44-04-	1.13 871		
7:52.2	1.772	1.18	2.89	₽826.Ø	T.02-671-	2.41-04-		. Q. TS-IA-		- 1.S- ee-	23:24
8.64:7	2.872	7.85	ø. 99	Z8Z6.0	8.43-871-	Z. Ø3-Ø4-		· Þ.Þ- SÞ-		- 7.8E-9E-	23:18
8.84:T	3.672	45.5	8.69	6729. Ø	2.12-471-	E.12-14-		- 6.86-24-		- 3.8- 04-	23:12
3.24:7	2.182	7.13	6. øa	3729. Q	1.68-171-	I.74-I4-	2.34-171-	- 8.E- E4-	£.2E-171	- 48-31.2 <b>-</b>	23: 8
			1.83	1729.0	9.74-891-	0.1- SA-	8.34-831-	- 43-24.6	168-48.2	- 40-50.2 -	23: Ø
8.7E:T	8.882	8.73	1 03	1200 B	0 27 001	<b>.</b>					
		0170	a	7926.0	7.84-391-	+·0Z-Z+-	T'98-99T-	. 7.85-E4-	£.44-48I	- 6'Z- Ib-	55:24
9.18:7	9.382	9.29	Ø.33		9.16-291-			- 43-45.Ø		- 7.8- IA-	22:48
£.32:7	6.882	T. T.	8.13	Z926.0				· 8.24-64-		- p.8- Ib-	22:42
<b>6.71:7</b>	4.262	8.ST	4.84	926.0	7.4- 631-					- I.33-04-	22:38
9.6 :T	8.862	4.77	7.44	6426.0	-166-21.5			0.0E-E4-			08:22
4.0 :T	3.108	1.28	7. Q4	2420.0	Ø:61-191-			-43 -5.1		- 8.SE-04-	
2.03:5	4. TØE	6.88	8.88	££26.@	7.13-841-	1.11-14-		- 42-24.9		- 1.73-6E-	22:24
8.88:8	314.4	8.19	4.IE	ZZZ6.0	-141-50.2		6.6I-0 <b>&gt;</b> I-	- 2.42-14-	143-11.5	- 3.4- 98-	22:18
8.32:8	8.62E	1.79	9.32	6026.0	-132-22.8		133-58.4	- 0.63-66-	2.04-781	- 8.84-78-	22:12
			1.81	1919.8	8.81-821-			- 8.62-76-	6.84-08I	- 3.84-38-	9:22
1.01:9	334.5	ø.eøi	1 01	1010 0	0 0. 00.	0 00 00			-		
F.00.0	4.098	2.411	ø.ø	9+16.0	e.t- att-	8.1- &£-	9.1E-8@I-	-31-14.1	9.88-011	- 7.62-82-	STIMIT
₽.88:3	7 69 S	OFF	שש	07 LU 10	J		<del></del> -	_			
YTIAAJUNNA	MIDTH	Z∀	TJA	OITAR	LONGITUDE	<b>EATITUDE</b>	ONGITUDE	LATITUDE L	DNGITUDE	LATITUDE L	
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DURATION	HTA9	141.12	14113	0111110	EK LINE	CENTE	4 FIMIL	SOUTHERN	LIMIT	NORTHERN	
					2017 1 03	J-11-0					
58.0 Sec	= 1 63	เอด									SAROS 131

7.01:5	782.4	7.262	ø.ø	8090°T	1.81 84	8.73-SI <del>-</del>	3.78 84	4.84-EI-	3.74 34	A'AT-7T-	OLTHITI
4.72:8	L:077	~				0 23 01	3 26 87	N 9N-21-	3 27 37	0.01-21-	STIMIL
4.E : 4 A 70.E	210.4	Ø.46S	ε. Τ	1.0632	6.74 23	⊅.8- @1-	9.71 43	-10-26.3	6.0 I3	4.23-6-	84:02
	225.1	9.362	ø. IS	9790.I	63 21.4	4.81-4-	3.74 48	<b>4.</b> 43-4-	9.23 29	2.04-8-	20:42
4:26.3	8,282	6.362	6.82	@@T@.I	p.08 69	7.81-0	0.22 @T	4.0E-I-	6.88 88	2.8- Q	98: 0Z
4:45.2	8.782	8.362	35.2	8170.I	8.04 ET	8.83 I	7.08 47	7.21 I	3.64 ST	0.04 Z	8E:0Z
6:I:9	8.142	9.362	7.04	2.ETQ.I	8.3 <i>TT</i>	8.81 4	3.83 77	7.28 E	7.31.87	I'# 9	20:24
1.71:3	6.442	1,362	9.34	44T0.1	6.1 \@8	8.4.8	I.64 08	Ø.75 3	3.81 97	6. II Ţ	81:0Z
6.88:3	3.742	9.462	1.03	4370.I	8, 65 28	6.8I 8	Ø. 92 £8	4.62 T	81 52.5	Ĭ.Ţ. 9	21:02
5:43.7	248.6	Ø.46S	54.3	£970.I	9.4 98	3.5 QI	7.64 38	9.21.6	2.81 48	9. £3 QI	9:02
4.88:8	251.3	8.882	58.3	@TT@.I	7.61 T8	I. 04 II	6.ε 88	8.74 QI	4.48 88	1.25 21	20: 0
1.8:8	7.232	292.5	2.29	TTT0.1	6.72 <b>68</b>	6.6 EI	Ø'II Ø6	9.31 SI	8.64 88	p.8 ÞI	19:61
8:12:8	223.9	7,162	6.39	2870.I	1.18 19	8.88 <u>*1</u>	8. EI 26	2.88 81	8.84 0e	16 28.5	
8:24.5	Ø.332	8.062	9.69	7870.I	6.88 89	7.13 31	3.11 46	9.48 41	4.64.29 2 49.40		84:61
6:32.1	8.332	8.682	Ø. EY	1670.1	4.82 3e	7.4 71	3.7 86	3.8 8.5 0 h3 h1	9.84 48 6 4 48.5	18 2.5 16 48.1	19:42
7.88:8	9.932	8.882	4.87	4670.I	7.42 79	8.21 81	1.2 86	2. EI 7. I	3.84.89 3.84.60		98:61
1.44:8	2.732	8.782	8.67	7670. I	9. 02 66 5. 02 50	2.81 91	2.83 66	8.31 81 2 £1 71		19 12.0	ØE:6I
4.84:9	9.732	8.882	1.58	8670.I	6.81 101	0.31 02	3.03 101	19 12.9	2.44 86	8.81 02	19:24
4.13:8	6.732	2,882	8.38	9670.I	2.41 501	4.6 IZ	7.34 801	I.8 &Z	8.54 001	6.91 12	81:61
8:53.2	Ø.832	3.708	2.88	ØØ8Ø.I	5.81 301	8.63 IS	105 42.4		1.24 42.2	22 12.5	19:15
8:53.6	Ø.832	I'IØI	2.88	0080.I	8.41 T&I	8.44 SZ	8.14 TOI	2.88 12 20 64.9	104 43.8	3.5 52	9 :61
0.70.0					0 71 201	0 VV 00	E IV ZWI	2 98 12	0.84 80I	6.64 82	Ø :6T
8:53:8	7.732	E. WOI	Ø. £8	6670.I	£.61 9@1	23 25.3	0.54 eqi	1.91 22	108 65.3	24 31.6	18:24
9.03:9	257.3	1.66	7.97	7670.I	E. TS III	24 1.3	0.84 III	22 54.3	3.8 III	2.8 32	18:48
6.84:8	7.932	9.76	€.87	3670.I	8.68 EII	24 32.3	113 511	7.42 82	1.22 211	9.98 32	18:42
6.14:8	8.332	1.96	9.27	2670.I	115 56.8	24 68.1	0.11 SII	23 50.1	116 42.9	1.8 82	18:36
9:38:9	264.6	9.46	4.69	8870.I	8.61 811	\$ 18.4	4.0E 8II	1.01 12	9.6 811	8.82 8S	Ø8:81
9.72:8	253.3	8.26	8.39	4870.I	120 49.4	7.28 32.7	120 56.3	24 24.4	128 43.2	8. I4 8S	18:24
9:81:9	221.6	Ø.16	1.29	8770.I	123 26.7	26 40.5	8.62 821	24 32.5	1.42 221	8.84 82	81:81
6.7 :8	7.642	2.68	5.83	STT0.I	126 13.2	25 41.3	126 12.2	7.88 42	126 15.4	8.84 82	21:81
6.33:3	247.5	£.78	5.43	4970.I	7.01 est	25 34.Ø	129 6.4	1.72 \$2	8.71 est	7.04 8S	9:81
8.42.8	245.0	2.38	0.03	8370.I	132 21.4	26 17.4	132 11.8	7.11 42	7.28 281	ğ. £2 82	Ø :81
8.72:3	242.1	1.58	4.34	9470.I	1.64 381	8.03 PS	136 34.9	8.845.8	136 5.2	0.43 BS	17:54
p:11:9	7.882	6.08	40.5	4870.I	9.88 <u>esi</u>	2.6 42	9.91 981	9.8 ES	2.0 04I	26 11.1 26 11.1	84:7I
4:53.2	8.482	9.8Y	32'I	0270.I	I.0 AAI	8. 01 ES	7.38 841	8. II .S	1.72 441		
4.38:4	8.622	Ø. 97	8.82	Z&T&.I	Ø. Ø1 641	9.84 IS	5.65 841	7.03 02	7,84 94I		17:42
a.7 :4	1.822	1.57	8. ØZ	8780.I	155 52.1	8.88 eI	155 12.1	2.84 8I 7 83 80		22 42.3	98:7I
3.82:8	I.QIZ	Ø:69	6.9	££80.I	168 12.2	9.8 3I	2,64 881	I.48 4I	1.73 931 5.85 331	6.72 \@S	Ø8:71
					0 01 001	D C 31	0 07 881	1 10 11	3 73 091	15 22.2	<b>₽</b> 2:71
3:11:6	£.£02	4.78	ø.ø	1190.1	9.62 ATI	12 30.4	I.II ATI	11 38.4	▶.1 371	s. Ti ei	LIMITS
YTIJATOT	111.07.	70									
VITARUQ VIT 14TOT	HTA9 HTGIW	ZY	TJĄ	OITAR	LONGITUDE	LATITUDE	LONGITUDE	<b>BOUTITAL</b>	LONGITUDE	LATITUDE	TIME
MATTAGIN	UTAQ	NUS	NUS 9	DIAMETER							NNIAEBSYL
					R LINE	CENTE	M LIMIT	SOUTHER	SN LIMIT		• •
58.3 Sec	= T sJ1	84									
3 6 63	- 1 A41	-4			700 :-					9	SAROS 13
				1661	inc ii 40	AR ECLIPSE	ATOTAL SOL				

**SIIWI7** 

## Table 22

1,12:7	T. 378	5 676	שש	OFEC D	0 10 000		•	
				9806.0	25 20.9 132 42.3	23 31.2 132 35.5	27 20.0 132 35.4	84:Q
4.2 :8	326.4	7.482	1.91		2.14 851 4.24 12	5. PI 8EI 0.0 02	8.2 82.8 239 2.6	24:Q
1.72:8	3.848	2.182	7.82	4019.0		5.21 241 3.62 11	8.71 841 9.88 02	98:Ø
3.74:8	342.8	9.822	29.5	7116.0	3.84 SAI 9.93 8I		18 15.5 146 33.8	Ø8:Ø
8.3 :6	8.888	8.822	8.48	8216.0	16 45.8 145 58.4	7.02 341 0.01 3I	70 70 70 70 70 70 70 70 70 70 70 70 70 7	8:24
	335.8	2.422	3.88	9819.Q	4.88 841 9.94 4 <u>1</u>	13 25.4 147 58.8	Z.81 941 9.81 81	
8.22:8			2.24	8419.0	1.73 031 2.7 81	3.81 Q31 8.44 11	2.86 131 4.26 41	81:Ø
8.88:6	8.888	221.9		Ø319.8	8.0 EBI 8.48 II	3.91 231 0.81 QI	12 68.8 153 40.3	ZI:Ø
Ø.43:6	932.Ø	9.612	7.84			8.11 431 7.64 8	11 34.1 155 32.7	9 : Ø
£.8 : 01	a.ree	1.712	8.84	9916.0	0 02 722	7 33 1 155 55.6	5.81 731 6.81 QI	ø :ø
10:22.0	₽.@EE	4.412	7.13	Ø916. Ø	8 54.0 156 36.4	9 33 331 1 66 2	0 01 221 0 01 21	-
						1.88 731 3.22 8	9.63 831 1.8 9	53:24
8.48:QI	8. QEE	4.112	5.43	4916.0	7 43.3 158 13.5		4.1 160 24.4	23:48
6.84:01	9.0EE	Ø.802	8.83	7916.0	4.34 931 2.88 8	9.3 159 5.6		23:42
10:58.0	8. IEE	2.402	6.83	ØLIE. Ø	5.81 181 13.3	6.48 New 34.3		23:38
			6.03	£719.8	2.88 281 8.24 4	1.0 231 8.02 g	8.21 63 15.8	
1.8 :11	332.3	6.66I		3719.8	8 51 5 164 1.0	8.82 831 1.62 2	8.78 <b>4</b> 81 7.31 8	23:38
2.71:11	8.888	1.361	62.5		3 4.5 165 22.1	0.84 481 4.14 I	7.73 331 4.62 4	53:24
11:25:11	335.Ø	7.68I	6.69	9719.0		4.7 881 8.78 Q	8.81 T81 1.74 E	23:18
8. IE: II	7.988	6.E8I	6.48	8719.Q		8.82 731 4.71 Q	8.831 7.8 8	23:12
8.88:11	4.888	7.771	9.39	8719.0	1.2 881 2.24 1		9.83 991 2.48 2	23: 6
4.04:11	1.04E	8. ITI	8.39	6716.Q	0.22 e31 8.8 I	8.64 831 6.81-0		23: Ø
4.24:11	7. IAE	8.491	7.38	6719. Ø	4.24 &TI 1.38 &	8.11 <b>0</b> 71 8.13-0	6.21 171 4.8 S	9.50
A CA.II	7 116	0 131	2 30	0210 2				
		O' OOT	Z.39	8719.Q	8.5 271 1.7 Q	9.48 ITI 3.02-I-	6.28 271 4.88 I	22:54
11:42.8	3.848	128.5			9.82 ETI 0.TI-0	3.63 271 8.84-1-	1 13.2 173 54.3	22:48
£.14:11	344.5	125.5	4.48	8719.Q	8-37.3 174 52.8	5.82 ATI 6.8- 2-	7.71 371 9.83 Q	Z⊅:ZZ
11:38:11	345.6	Ø. TAI	2.89	8719. Q		7.88 871 1.42-2-	7.84 871 8.88 Q	22:38
1.88:11	8.846	142.1	7.13	3719.Q	8.61 871 8.83-0	8.82 \\ \T\ \\ \Z\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \	8.21 871 4.72 Q	22:38
11:26.3	8.848	8.781	6.63	£719.0	4.03 TTI T.3- I-		7.34 971 3.02 0	22:24
7.71:11	I.748	Ø. 481	8.73	Ø719.0	0.32 971 3.51-I-	7.4 871 8.84-S-		22:18
	2.748	8.0£1	3.23	7916.8	8.33-871- 3.31-1-	S. 41-671- 8.64-2-	7.85-871- 4.81 Q	
4.7:11		•	ğ. 53	£919.8	0.11-171- 3.41-1-	8.72-771- 7.84-2-	3.63-871- E.12 Q	22:12
10:55.5	1.748	Ø.821		6916.8	£. 61-371- 0.7- 1-	2.48-371- 1.54-2-	8.8- 371- 9.92 @	52: 6
9.I4:0I	6.84E	125.6	5.03		2.91-871- 1.83-0	8.28-271- 2.62-2-	3.4- 871- 8.44 Q	Ø : ZZ
6.82:01	6.94£	9.521	2.74	\$916.0	0 61-571-1 63 8	0 00 021 0 00 0		
					7.8- 171- 0.2E-0	7.02-171- 2.e- 2-	0.33-071- 0.7 1	51:24
4.01:01	Q. T48	6.121	6.54	6416.0	7 8- 171- 0 36 0	7.83-831- 8.84-I-	7.18-881- 0.88 1	21:48
9:23:6	4.748	120.5	£.04	2410.Q	8.44-168-44.8	7 33-091 0 DV 1	7.64-381- 9.91 2	27:12
2.88:9	3.848	E. 6II	8.38	\$216.Q	9.2- 331- 7.7E Q	-1 -2.1 -166-13.5		21:36
9:12.2	8.648	2.811	9.18	9ZI6'Ø	0.83-281- T.18 I	1.7- 881- 2.01-0	3 16.3 -162-41.4	
		ε. Υ <u>ΙΙ</u>	9.92	4116.0	8.81-931- 3.34 S	8.42-951- 4.0 I	9.13-831- 8.85 A	21:30
1.64:8	352.3		_	6606.0	8.31-431- 7.28 4	8.78-431- 7.14 S	6.28.6 -153-45.3	21:24
8.22:8	3.838	5.811	1.02		5.8- 8+1- 3.74 T	2.6- 741- 8.38 3	18 18.6 -144-23.3	21:18
Ø. Y♪: T	9.498	6.4II	ī. Øī	3706.0	2 9 9/1 1 2/ 2			
				700010	8.03-781- 1.31 II	3.78-881- 8.33 6	2.86-761- 3.11 EI	STIMIJ
9.61:7	2.4TE	4.EII	ø.ø	Z306.0	8 23-751 1 31 11	3 20 000 0 11 0		
				071101	LATITUDE LONGITUDE	LATITUDE LONGITUDE	LATITUDE LONGITUDE	TIME
YTIRAJUNNA	WIDTH	Z∀	TJA	OITAR	AGUITIONO I AGUITITA I	301210101 301224 1		ONIVERSAL
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58.7 Sec	= T &J	lθα					•	, , 50015
3 2 01	- '			766	NA ECLIPSE OF 4 JAN 1	A IO2. 9A IUNNA		

I.12:7 7.378 8.242 0.0 8408.0 8.18 811 8.28 28 2.83 811 2.81 18 7.08 811 8.82 48

## TOTAL SOLAR ECLIPSE OF 30 JUN 1992

2.63:2	r.ars	8.608	0.0	9740.I	1.78-78-	3.4- 13-	1.64-78-	-52-24.6	7.82-ee-	9.34-03-	STIMIL
\$.72:E	2.022	8.818	Ø.II	1.0508	7.22-82-	7.03-44-	7.64-82-	8.0E-TA-	0:10 +7	T.00 71	
8.34:8	8.722	8.828	8.9I	1.0526	5.85-82-	9.02-I4-	7.28-12-	8.31-54-	-24-61.3	1.68-24-	
7.63:8	6.682	9.728	6.02	6830.I	2.14-81-	9.83-88-	8.11-71-		7.63-61-	1.35-65-	
9:11:4	3.952	6.088	8.42	1.0548	7.35-51-	9.83-86-	8.23-51-		6.71-81-	4.8I-TE-	
6.12:4	8.442	6.888	1.72	1.0556	1.63-61-		8.7- II-	3.08-88-	2.62-21-		
				0220	1 03 21	M 01_35	8 2- 11-	3.74-88-	7.63-01-	8.13-55-	13: Ø
4:31.1	249.9	7.888	29.62	1.0563	7.14-8-	-33-52.6	9.44-8-	1.91-35-	8.14-8-	6.82-28-	15:28
4.98.4	8.452	3.688	9.18	6930°I	Ø.8£-8-	E.7E-2E-	9.98-9-	7.1- 4E-	4.14-8-	4.31-16-	
8.84:4	7.632	8,248	4.88	1.0673	9.44-4-	2.0E-IE-	7.68-4-	-32-53.1	8.03-4-	3.6- 0£-	
4:53.5	4.482	342.1	35.Ø	1.0678	7.83-2-	6.62-8E-	2.13-2-	7.13-15-	ε. <u>Υ</u> - ε-	Z.91-62-	
7.63:4	ø.692	8.7⊅€	3.98	1.0581	6.8I-I-	9.35-62-	2.e- I-	3.83-88-	3.62-I-	9.81-82-	
8.4:8	4.8TS	35Ø.7	7.78	1.0584	Z. 9I @	9.84-82-	8.72 à	7.8- 0E-	Ø. Þ. Ø	0.82-72-	
ø:6:9	<b>8.</b> 772	3.53.5	7.88	1.0586	7.74 I	ø.2- 82-	8. <u>0</u> .5	8.12-62-	I.48 I	9.84-82-	
5:12.8	281.5	326.4	39.5	1.0588	8.81 E	6.12-72-	8.88 £	5.14-82-	3.1.5	0.4- 82-	
8:12:8	2.382	329.3	2.04	Ø69Ø'I	4 42.8	8.6-45.8	4 58.5	9.4- 82-	9.72 A	1.82-32-	
5:18.1	<b>₽.</b> 882	2.2	7.04	1690.I	8.7 8	-26-13.5	6.24.5	4.28-72-	0.13 3 5 50 h	6.83-42-	
7.61:3	2,162	1.3	Ø.I4	1690.1	8.18 T	8.44-82-	8.64 T	8.E- TS-	2.41 7	8.72-42-	
8:2Ø.8	4.862	1.8	2.14	Z690.I	8 EE'4	9.61-52-	1.41 9	4.88-82-	6.88 8	1.2- 42-	21:21
7.02:3	Ø.362	ø.tt	2.14	1690.1	6.81 QI	8:73-42-	9.85 QI	9.81-82-	7.63 6	5.04-82-	12:8
5:20.1	Ø.86S	6.EI	Ø.I4	1690.1	0.54 II	9.65-42-	12 3.5	4.83-32-	0.82 II 7 03 0		
5:18.7	2,862	8.81	9.04	Ø63Ø.I	9.7 EI	8.42-42-	13 29.5	8.64-32-		6.12-62-	15: 4
						8 VG-VG-	13 00 E	-2E-43 A	2.74 SI	9.8- ES-	12: Ø
9:18:8	7.362	7.61	1.04	1.0588	14 34.4	-24-13.2	14 26.9	-25-32.3	14 12.8	-22-55.4	11:28
2:13:6	4.462	22.5	4.68	1.0586	8.2 at	4.8- 42-	16 26.4	9.42-22-	16 40.3	4.74-22-	11:25
6:6:9	2,262	2.32	38.5	1.0584	6.88 TI	5.I- 42-	17 58.6	7.02-22-	E. ŠI ŽI	1.54-22-	87:11
<b>5: 5.4</b>	4.682	<b>6.7</b> 2	3.75	1890.1	2.8 er	1.1- 42-	8.48 eI	6.02-32-	18 43.5	7.24-22-	44: II
5:0:3	7.382	3.08	2.98	1730.I	9.84 QZ	2.3- 42-	21 14.3	-25-25.3	2.02 02	4.84-22-	ØÞ: [ [
4:64.1	4.182	1.88	8.48	1.0673	1.08 22	6.61-42-	7.63 22	9.45-32-	2. 2. 4	7.43-22-	98:11
2.74:4	4.872	35.6	1.88	1'0296	24 19.9	8.72-42-	24 52.Ø	-25-49.1	23 58.3	8-8- £2-	28:11
4.98:4	8. <b>&amp;</b> 7.2	1.88	2.18	1.0563	6.71 as	8.74-42-	26 52.9	8.6- 82-	7.84 82 25 45.7	£.72-E2-	11:28
8.08:4	8.482	3.04	1.62	7330.I	28 26.3	-25-14.4	29 5.3	6.78-82-	7.03 72	8.23-52-	11:24
6.02:4	8.732	Ø.54	9.92	0990'I	8.84 QE	8.64-32-	δ. <u>ε</u> ε <u>τε</u>	2.31-72-	3.8 %£	8.82-22-	11:20
8.6 :4	72®.4	42.5	7.52	1,8641	2.08 88	6.86-82-	34 22.5	7.4- 82-	3.54.25	7.01-32-	91:11
3.57.2	242.3	I.84	E. QZ	1.8531	3.14 88	3.85-72-	E. 84 TE	0.21-62-	3.44.38	0.6- 82-	
3:42.1	6.282	1.13	Ø. 9I	7130.I	40 42.3	4.8- 62-	4.81 S4	8.03-08-	4.82 ge	0.62-72-	11:12
8.12:8	8.122	ø:99	L. 6	7640. I	9.84 84	0.28-18-	8.83 e4	3.1- 46-			8 : 11
			_ •	20.2	0 07 07	D 00 16	6 93 9V	-34 -1 E	6.48 44	8.16-62-	<i>†</i> : [ ]
7.83:2	2.702	8.09	ø.ø	6940.I	4.04 33	8.82-36-	56 13.2	0.84-8E-	T. 03 83	-34-55.4	CIMITS
YTIJATOT	MIDTH	Z∀	TJA	OITAR	LONGITUDE	TODITIONE	LONGITUDE	PAULTING	TOWATIONE	34017123	TMT
NOITARUG	HTA9	NOS		DIAMETER		7-41 ITTT 4	TOME I	aditta i	LONGITUDE	⊒(I) ITTT 4	TIME
					ER LINE	CENTE	M LIMIT	2001UE	N LIMIT	MONINE	UNIVERSAL
							TT/1T   140	III 103	TTUT I NO	JUTOUK	
59. Ø Sec	= T stl	e₫								c	SAROS 14
				Z66I	NUC BE HU	אג בנדזאפב	וחושר פחר			8	*

# ANNULAR SOLAR ECLIPSE OF 10 MAY 1994

Delta T = 60.4 Sec

6.28:4	£.8&£	6.062	ø.ø	1086.0	4.84 4	8.72 28	2.2 3 6.4 I	8 2.4.2 8.82 8	EE STIMIJ
/:00:±	6.382	6.672	9.91	1489.0	22 4.4	3.23 78	1.88 42 4.31 7		
7.83:4		3.572	24.1	6359.8	7.33 62	7.0 Q4	8.34 IS 0.11 9		
2.3 :3	4.882 8.472	Ø.892	8.62	2759.8	35 53.3	41 25.2	2.02 TE 6.62 0		
9:14:9		7.282	34.5	2859.8	Ø.33 ØÞ	42 26.Ø	1.8 24 4.72 1.	4 3.78 98 3.4S	
5:22.9	9.632		7.88	1989. Q	45 21.8	T. QI EA	8.02 84 0.01 S	4 I.8I 44 T.II 1	78:30 v
4.0E:3	223.9	9.732		8659. Q	4.42 64	1.54 54	8.21 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	4 45.6 48 32.1 4	78:24 44
2.78:3	1,642	252.5	3.24		3.8 63	7.8 44	3.74 83 8.2 8		38:38 <b>4</b> 8
4.64:3	244.9	2.742	6.34	4046.0	1.88 93	6.61 44	7.8 73 3.81 8		18:15 4 <sub>8</sub>
Ø.64:3	4.142	8.142	Ø.64	6016.0	7.88 68	44 26.8	7.81 00 E.ES E		
0.43:3	238.5	236.3	6.13	4146.Q	0.8 88	8.72 AA	9.81 £3 8.52 £		
5:58.5	Ø.862	₽.@£Z	3.43	8146.Q	62 3 0	6 20 VV	0 01 00 0 00 0		
6:2.5	6.882	2.422	6.93	1246.0	9.1 99	44 22.Ø	9.01 88 T.81 E		
8.3 :9	232.3	8,712	ø:69	4246.0	2.23 88	4. II. 44	4.33 89 4.8 E		
8.8 :8	8.1E2	210.5	6. Ø 9	9246.Q	0.88 IT	43 55.9	2 63.6 71 33.6	•	
8. ØT: 9	Z. Ø8.Z	0.502	8,28	8246.Q	74 13.5	8.38 84	7.8 AT 0.48 S		
6.12.3	8.622	Ø'96T	6.69	Ø846.0	9.34 87	3.11.54	2 10.4 76 32.6		
£.£1:8	4.622	9.98I	6.49	1649.Q	8.21 <b>9</b> 7	1.84 24	1 42.8 78 55.Ø		
7.51:8	9.622	6.771	9.39	1649.Q	81 36.2	8.	1.61 18 A.11 I		
9.51:9	0.082	6.89I	Ţ. 39	1649. Q	83 23.9	6.48 IA	7.72 88 4.88 Ø		
6.21:8	8.8£2	Ø. Ø91	9.39	1649.Q	£.6 88	40 E5.3	2.68 38 8.73 6		
8.11:8	231.9	121.4	Ø.39	Ø848. Ø	<b>6.12 88</b>	4Ø 12.3	1.84 78 7.31 9	8 6.83 88 3.6	14 Ø : 71
			I.48	6246.0	8.28 <b>0</b> 6	8.32 98	0.33 89 E.QE 8	ε φ.11 19 θ.12 i	J6:54 40
8.6 :9	4.882	143.1			I.IA 29	38 35.9	4.0 Se 4.14 Y		66 8 <del>1</del> :91
3.7 :8	235.2	135.4	6.29	8246.0	0.64 46	3.24 78	0.3 49 I.94 8		16:42 38
8.4 :8	237.3	128.3	8.13	9246.0	7.83 86	36 45.6	4.9 89 E.E3 3		76 36:31
3.1:8	8.682	7.121	9.69	8248.8 Ø.9423	0.3 66 7 33 80	35 45.1	9.41 89 6.83 4	• • • • • • • • • • • • • • • • • • •	
<b>6.73:</b> 3	7.242	8.31 <u>1</u>	4.73	0246.0	181 15.8	8. Q4 4g.8	4.12 001 8.03 E		
5:53.8	6.345	110.6	ø:99	7146.0	8.72 EQI	4.28 EE	8.02 301 4.24 2		16:18 34
5:49.3	2.642	105.6	4.23	£146.0	8 70 501	3.91 28	4.44 401 7.18 I	• • • • • • • • • • • • • • • • • • • •	
4.44.8	2.632	I. IQI	9.64	8019.0		8.I IE	8.8 TOI I.3I O	<u> </u>	
5:39.2	<b>6.73</b> 2	1.76	9.84	£046.0		2.88.92	8.18 901 9.23 8		
5:33.5	7.282	8.89	Σ.εμ	9886. Q	I.04 QII	2 86 3	2 10 001 0 02 0		
4.72:3	6.782	8.68	3.68	68£6.0	113 24.2	ø.8 82	7 24.1 112 10.2		
8.02:3	3.572	9.88	3.35	1886.0	116 25.6	1.62 92	1.3 311 1.74 3		
9.51:3	9.672	3.58	8. å£	1789.8	119 63.2	8.88 42	7.82 811 E.93 E		
8.8.8	4.882	a. 88	4.82	8359. Ø	124 3.3	22 31.5	8.61 221 <b>0.8</b> 8 1		
8.88:4	8.462	4.77	18.4	2459.8	129 36.8	19 63.9	\$ 26.4 127 25.4	21 7.4 281 7.71	72:30 SQ
8 33.1	2 100	V 22						T OTHE OUT THE	FIWITS I
8.48:4	S. &IE	Ø.ST	ø.ø	7626.0	145 36.3	9.24 EI	8.12 341 4.81 2	47:1 146 64:3 1:	Ar STIMI
		711	170	OITAR	AUU I TANU.	LATITUDE L	TITUDE LONGITUDE	ITUDE LONGITUDE LA	TIME LAT
DURATION YTIRALUNNA	HTA9 HTGIW	Z∀ N∩S	SUN TJA	DIAMETER					NNINEBSAL
1102210110					FINE	CENTER	SOUTHERN LIMIT	ORTHERN LIMIT	IN.
5e2 4.08	= T st	le0							SAR05 128

Table 25

### TOTAL SOLAR ECLIPSE OF 3 NOV 1994

50.8 Sec	= T st	Del								1	SAR0S 133
					R LINE	CENTE	TIMIT N	SOUTHER	N LIMIT	иовтнев	
VOITARUO YTIJATOT	HTA9 HTGIW	Z∀ N∩S	SUN TJA	DIAMETER OITAR	LONGITUDE	<b>EATITUDE</b>	LONGITUDE	LATITUDE	LONGITUDE	<b>BOUTITAL</b>	UNIVERSAL TIME
1:52.3	135.6	105.2	0.0	0980.1	<b>4.24</b> 86	0.73-7-	3. %I 76	3.72-8-	4.7£ 86	2.02-7-	STIMIL
8.81:2	163.8	T.SQI	1.41	1.0405	1.83 58	1.1- 21-	85 21.Ø	-12-15.1	8.04 28	0.34-II-	12: 6
2:39.3	165.2	Ø.001	7.82	1.8434	1.8 87	Z.QI-3I-	2.3 77	7.88-31-	Ø.6 37	6.34-41-	15:15
8.43:2	8.271	3.79	4.0E	1.0454	Z. E3 &Y	2.28-71-	71 45.2	7.63-71-	T.S &T	0.4- TI-	15:18
8.7 : E	E. 771	7.46	9.38	6940.I	9.34 99	2.55-91-	7. EE 78	4.8- \\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	9.83 39	4.2- 91-	12:24
8.61:8	Ø.181	7.16	7.0A	1840.1	7.41 59	1.12-12-	2.0 49	-21-53.6	2. 8£ 28	Z.84-02-	12:30
3.29.5	8.581	3.88	Ø.34	2640.I	£.7 <u>0</u> 8	-22-59.9	6.03 09	2.48-82-	7.42 63	-22-25.2	12:36
Ø.88:E	182.8	8.48	6.84	1.0500	Ø. 91 73	-24-31.5	6. 73 <u>73</u>	2.Y- 2S-	Ø.35 93	-23-65.2	12:42
8.74:8	4.78I	7.08	5.53	1.0508	6.35.43	£.73-32-	5.81 25	8.48-82-	3.83 53	4.61-32-	12:48
3:54.8	188.5	Ø. 97	7.33	1.0514	8.8 23	0.8I-72-	9.24.29	ø. 73-72-	6.32 13	8.85-82-	15:24
4: 1.5	£.68I	T. QT	7.83	1.0520	2.78 ex	£.4£-82-	5.41 &3	7.41-62-	8.0 et	8.83-72-	13: Ø
2.7 :4	7.681	8.48	4.13	1.0524	2.41 TA	7.84-62-	7.84 TA	8.82-0E-	46 39.5	6.4- es-	13: 8
4:12.2	ø.8e1	8.73	8.69	1.0528	44 53.4	-30-65.3	1.72 34	1.85-15-	44 20.4	₽.SI-@E-	13:15
Z.8I:4	ø.0e1	9.64	8.39	1.0531	4.88 24	8.0- SE-	43 6.2	-32-44.3	42 2.2	£.81-1E-	
4.01:4	6.68I	3.04	4.78	1.0533	9.51 04	9.1- EE-	7.24 Q4	0.74-EE-	6.84 68	6.81-28-	13:24
4:21.6	7.68I	4.QE	3.89	1.0534	8,13 78	2.0- 4E-	8.81 88	2.84-48-	37 24.4	2.41-66-	
4:23.0	£.68I	9.61	1.69	1.0535	4.72 38	-34-22.1	8.23 38	-36-42.Ø	35 2.8	1.8- 46-	13:36
4.23.4	188.8	8.8	1.69	1.0535	2.0 EE	9.84-36-	33 22.5	6.46-86-	8.88 28	8.83-46-	13:42
4:22.9	1.881	3.738	3.89	1.0535	8.62 8E	4.48-88-	8.84 QE	8.52-78-	6.9 å£	9.94-3E-	13:48
4:21.4	4.781	4.748	4.78	1.0533	8.23 72	7.81-78-	6.8 82	6.7- 8£-	8.8£ 72	9.62-98-	13:24
6.8I:4	186.5	Ø.888	8.39	1.0531	7.01 32	1.63-78-	2.62 32	7.84-8E-	0.83 AS	3.6- 78-	Ø : ÞT
4:31:4	182.5	3.928	8.88	1.0529	22 21.5	-38-35.3	22 30.3	-39-25.3	22 12.5	3.34-78-	
Ø.11:4	184.3	7.128	4.13	1.0525	2.42 e1	1.7- ee-	19 28.8	2,73-68-	2.61 61	1.71-88-	
8.3 :4	Ø. 581	7.418	7.83	1.0521	3.71 91	Ø.⊅£-6£-	8.71 BI	1.42-04-	7.81 BI	0.44-8E-	
3:69:8	3.181	8.808	7.33	1.0516	1.63 21	<b>▶</b> .33-6£-	15 ee'ù	-40-4E.3	13 3.4	7.3- 68-	
3:21.9	8.671	8.208	52.5	1.0609	8.82 6	8.01-04-	1.61 6	I.0- I4-	3.78 6	7.12-68-	
3.43.5	<b>6.771</b>	8.862	6.84	1.0502	4.24	2.91-04-	1.72 3	8.7- IA-	3.83 3	6.86-ee-	
0.4E:E	9.371	2,162	Ø.34	£640.I	6.88 I	4.61-04-	3.31 I	3.8- IA-	7.83 I	£.2E-8E-	
3:23.4	172.9	8.382	7.0A	I.0483	6.23-2-	9.6- @b-	0.12-E-	6.43-04-	7.82-2-	2.42-66-	
≯.11:E	7.691	4.08Z	6.38	I 7 ÞØ · I	2.33-7-	2.74-ee-	Ø.18-8-	I.0E-04-	7.12- <b>7</b> -	1.4- 98-	
0 23-0		0 720	7 86	1 00,68	9 M-51-	9 L- 05-	0 00-11-	0 8105	7 0 61	2 20 00	D - 21
8.73:2	165.6	9.472	4.08	9340.1	8.44-61-	8.Y- 68-	6.62-41-	6.84-85-		7.72-88-	ø :91
8.14:2	2.081	8.832	7.82	7840.I	8.63-02-	6.0- 88-	-21-52.4	7.48-88-		I.82-78-	9:31
2:20.5	121.4	£.182	1.41	80+0°I	9.8- IE-	-32-26.3	6.04-2E-	3.71-86-	0.44-62-	-36-32.5	71:31
1.63:1	7.881	252.1	Ø. Ø	£850.1	1,88-84-	1.2- 28-	6.3- TA-	Ø. 28-28-	1.82-84-	E.31-25.3	STIMI

 $\overline{\mathbf{x}}$ 

ANNULAR SOLAR ECLIPSE OF 29 APR 1995

Delta T = 61.2 Sec

£.3E:4	9.942	9.482	ø.ø	4356.0	8.82 £2	9.86-8 <del>-</del>	23 14.1	<b>⊅.</b> 13-7-	22 64.5	6.78-8-	LIMITS
						0107-0-	9. TE 8E	9.28-4-	8.43 TE	E. 7- 2-	81:61
1.63:4	1.282	Ø.882	7.31	£6£6.@	9.81 TE	8.81-6-	8.82 E4	8.8- E-	4.81 44	I.83-0	ZI:6I
	225.3	8.882	8.62	£146.0	43 53.3	8.1- 2-		4.22-2-	Ø. 74 84	I.8I-0	9 :6T
	8.022	3.782	8.62	7240.0	6.72 8≯	8.81-1-	3.7 8A		7.82 23	8.7 g	Ø :61
	4.712	2.882	8.48	9849. Ø	4.8 53	6.23- <u>0</u>	1.84 13	£.43-1-	EO 03	8 2 10	D - O.
3 36.3	7 210	0 000	•						0117.00	Z.12 @	18:24
8.44:3	7.412	8.682	Z.68	8446.Q	7. QI 33	6.7E-@	64 53.4	7.78-I-	5.72 33		18:48
	4.212.4 7 110	2.062	2.54	9946'Ø	8.13 73	0.18-0	8.4£ 73	E. 62-1-	1.8 83	8.82 Q	
		291.9	6.84	£946.0	7.31 Ø9	4.0E-Q	8.83 63	3.72-1-	1 28 09	2.82 Q	18:42
1.1 :9	210.5		Z.03	6946.8	9.92 29	Ø-32.Ø	<b>4.</b> 6 28	1.18-1-	S. & 43.2	8.02 Q	18:36
	8.802	7.862		4749.8	9.82 48	Ø. 44-Q	9.6 49	2.98-1-	0.44 48	9.01 Q	Ø8:8I
	E. TQZ	7.362	8.83	6746.8	1.61 99	Ø. 73-8	4.I 88	2.13-1-	9.88 88	€.E- \@	18:24
Ø.02:8	8.3\\	2.862	2.83		6.4 88	4.51-1-	4.84 T8	6.8- 2-	₽.22 89	9.02-0	18:18
8.42:9	204.5	I.IQE	6.83	£846.0	5.44 69	1.55-1-	8.32 69	8.32-2-	T.S &T	Ø.14-0	78:1S
6.82:9	2,802	3. 4QE	4.13	8846. Q		8.33-1-	8.0 IT	7.74-2-	4.88 IT	p.p- I-	9 :8I
6.38:3	e.røs	8.8&£	8.69	6846. Ø	3.91 IT		8. IE 27	-3-12.6	8.01 ET	9.08-1-	ø :81
8.48:9	7.002	8.818	8.38	2646.0	72 61.Ø	2.12-2-	8 12 02	00,0	0 27 02		
					0107 H	4.64-2-	7.63 ET	I.04-E-	8.68 AT	Z:69-I-	74:E4
8.38:3	₽.66I	9.916	8.78	£646.8	3.61 47		4.32 37 7 93 57	5.QI-4-	8.3 97	3.0E-2-	84:71
8.78:8	£.861	2.828	7.83	3646. Ø	8.84 87	1.02-E-	5.64 87	8.54-4-	3. å£ 77	5.4- 8-	24:71
6.7£:8	2.791	7.888	9.69	9646. Ø	6.6 TT	4.63-6-			0.43 87	4.04-E-	17:38
3.75:8	2.961	7. I 48	I.QT	7646. Q	Ø.εε 87	1.62-4-	1.21 87	2.81-3-	7.81 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	0.61-4-	ØE: 71
4.88:8	195.2	9.03E	Z. ØT	7649. Ø	4.33 eT	2.T- 3-	1.48 97	Ø.83-3-			17:24
8.48:8	3.461	£.83£	8.69	7646. Q	8.71 I8	6.74-3-	0.83 08	£.8E-8-	2.68 18	6.63-4-	81:71
	8.591	1.9	6.89	9676'Ø	2.04 28	Ø.18-8-	4.81 <u>28</u>	2.61-7-	1.2 88	6.64-3-	21:71
1.26:8	193.4	z. £ I	8.78	9676. Ø	7.E 48	7.81-Y-	7.14 E8	8.4- 8-	8.32 48	2.62-8-	
1.62:8		8.9 <u>r</u>	ø. 88	4649.8	7.82 38	Ø.∂- 8-	3.8 38	0.63-8-	Ø.13 38	8.71-7-	8 : 71
6:25.5	1.591		I.48	2649.8	Ø. 83 88	2.83-8-	7.EE 88	1.44-6-	4.81 T8	7.8- 8-	Ø :TI
4.12:8	1.591	1.32	1 19	3070 D	2 02 00	•				_	
		ø.ø£	6.19	Ø676. Ø	2.82 88	Z'Ø9-6-	8.E 88	£.8E-@1-	7.84 88	8.2- 6-	16:54
8.81:8	193.3		3.63	7849.8	Z.0 06	5.74-QI-	6.7E 68	7.35-11-	8.22 &e	3.63-6-	16:48
8.11.8	7.891	3.48	8.83	8849. Q	2.98 19	6.74-11-	Ø. TI 19	9.98-21-	9°I 26	7.63-01-	16:42
8.8 :8	3.491	6.7£		6749.8	E. 42 E6	-12-52.1	5.2 86	4.14-61-	8.84 £6	-12 -3.5	16:36
4.0 :8	196.5	2.14	Ø. 43		ε. ΥΙ 36 Σ. ΛΟ 00	9.0- 11-	7.33 46	9.03-41-	2.68 39	2.11-61-	76:3Ø
5.43:3	6.8er	1.44	6.03	4746.0	2.02 76	9.21-31-	2.63 86	7.4- 81-	3.14 Te	9.52-41-	78:2 <b>₹</b>
3.74:3	7.8er	8.84	8. TA	6946.0		7.28-81-	8.31 66	7.42-71-	9.83 66	4.14-31-	81:91
3.04:3	8.002	ε.6μ	Ø. 44	£946.0	6.38 66	3.83-71-	0.03 tot	9.23-81-	1.82 201	7.3- TI-	16:12
Ø.88:3	203.5	8.13	1.04	9976.0	7.8 201		4.84 40I	4.82-02-	105 22.5	5.85-81-	<b>36: 6</b>
Ø.32:3	8.8%2	2.43	8.35,	7446.Q	Ø'9 9ØT	Ø.88-91-	108 22.6	4.7I-SS-	108 50.2	-28-22.1	Ø :91
5:16.3	6.012	7.83	6. Ø E	9649.Q	108 35.8	2.91-12-	8 60 801	A 71-00	0 03 001	- L 00 20	
							112 65.6	7.32-42-	1.11 511	-22-22-	72:2 <del>4</del>
7.8 :3	2.812	9.63	2.32	£246.0	113 2.3	4.62-23-			Ø. 81 911	-24-53.4	12:48
1.88:4	8.522	5.59	T. TI	9016.0	8.02 ell	6.0- 82-	2.0E 911	6.01-72-	ש פו טוו	, 63 ,0	·
+ 22°			-				7105 007	L. 14-70-	9.81 TEI	3.78-08-	SIIWIT
8.28:4	8.842	9.27	ø.ø	2986. Q	136 32.6	8.46-16-	136 45.1	4.74-28-	9 91 721	3 40 80	V11- 1
J 00 · F											
					,		7401 705107	רעודוטטבו	DOMETIONS.	LATITUDE I	TIME
ANNULARITY	MIDTH	Z∀	TJA	0ITA9	ONGITUDE.	LATITUDE	ACHITIDE I	1 BQUTITAJ	3011770140	. ¬/11/4744 )	ONIVERSAL
DURATION	HTA9	พีกร	NOS	DIAMETER			1	W7111000	ITWT7 A	ИОКТНЕВ	110021121111
HOTTAGING	,,_,				S LINE	CENTE	TTMT I N	IA3HTU02	TTMT   L	403UTQUIA	
										•	SAROS 138
280 7110	= 1 83	ıeα									

Table 27

TOTAL SOLAR ECLIPSE OF 24 OCT 1995

3.0 :1 8.74:0 7.32:0	1.14	265.9 266.9 267.9	26.9 19.3 4.9	4810.1 4110.1 2700.1	-148 -5.4 -164-15.8 -164-15.8	2 41.3	-147-58.5 -154 -8.2 -166-43.3	1.62 2	4.22-12.4 -164-23.7 -164-22.4	₽.63.4	8 :8 8 :8 8 :12
2.4.5 1.57.6 1.57.6 1.58.1 1.35.6 1.35.6 1.28.2 1.28.2	4.87 2.37 7.57 7.17 6.93 8.33 4.93 4.93	6.362 6.363 7.363 6.263 6.263 8.633 8.	2.4.9 6.19 6.19 6.63.8 6.63.8 6.03.8	6020.1 6020.1 6010.1 6010.1 7810.1 7810.1 7810.1 2710.1 2010.1	6.63-021- 6.63-221- 6.32-521- 6.32-521- 6.32-521- 7.75-361- 7.75-361- 7.75-361- 7.75-361- 7.75-361- 8.84-651- 9.81-	9.50 2.53 5.20 5.20 5.20 5.20 5.20 5.20 5.20 5.20	2.42-61.3 2.42-61.7 2.62-62.1 2.62-62.1 2.62-62.1 7.05-62.1 7.05-62.1 7.05-62.1 7.05-62.1 7.05-62.1	8.7 6.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5	8.85-521- 8.83-521- 8.83-521- 8.83-621- 7.42-121- 7.42-121- 7.42-121- 8.85-581- 8.85-581- 8.85-581- 8.85-581- 8.85-581- 8.85-581- 8.85-581- 8.85-581- 8.85-581- 8.85-581- 8.85-881-	6.34 4 1.21 4 2.14 8 3.51 8 7.94 2 8.08 2 4.31 2 0.7 2	86:33 86:33 86:33 86:33 86:33 86:33 86:33 86:33
4.73:1 1.1 :2 1.4 :2 2.8 :2 2.8 :2 2.9 :2 2.9 :5 2.8 :2 3.8 :2 8.8 :2	4.87 7.47 8.37 7.37 4.77 1.87 1.87	4.431 2.601 3.601 3.471 8.281 8.281 7.101 7.101 8.002 3.002 2.712	5.29 5.49 6.49 8.79 6.69 6.69 7.89 7.89 7.89	8020.1 8020.1 1020.1 1120.1 5120.1 6120.1 8120.1 8120.1	7.63-501- 1.74-301- 6.18-701- 6.21-601- 7.23-011- 7.96-711- 7.94-311- 7.96-711- 7.96-711-	3.72 21 8.72 11 8.72 11 6.86 01 8.85 9 8.84 8 8.83 7 8.83 7	4.183-581- 2.22-781- 2.22-781- 4.20-4.11- 4.20-4.11- 4.20-4.11- 6.11-7-1	8.9 21 6.21 01 6.21 01 8.71 9 8.71 9 9.92 8 9.94 9 5.3 9	6.7- 401- 6.83-301- 6.85-701- 6.12-601- 6.12-601- 6.45-711- 6.85-711- 7.85-811- 7.85-811- 7.85-811-	7.34 21 6.34 11 6.94 01 6.33 6 6.82 6 7.41 8 8.8 6 8.8 7 7.54 8	\$\rm \text{96} \text{96} \text{13} \text{96} \text{13} \text{15} \
8.44.8 3.83.0 4.83.1 1.83.1 6.78.1 0.78:1 0.78:1 6.84:1	7.64 7.64 8.43 7.73 8.83 1.33	1.711 8.121 7.421 8.721 8.721 6.081 8.481 8.481 8.481 8.481	7. 02 6. 72 83. 7. 28 83. 86 84. 89 85. 99 7. 63 7. 63	8010.1 8210.1 8210.1 4210.1 4310.1 4310.1 8810.1 8810.1 8810.1	2.78-8- 3.12-78- 7.18-09-	8.14 S2 12 8.3 IS 19 37.5 18 18.3 16 88.8 16 45.8		4.81 42 8.72 22 8.06 02 7.12 91 7.12 91 8.93 71 8.12 31	8.63-87- 6.68-88- 7.82-78- 6.98-86- 7.82-89- 8.82-89-	16 2.3	\$ : 2 : 2 : 2 : 2 : 2 : 2 : 2 : 2 : 2 :
6.31:0 8.72:0		6.401 0.011	0.0 0.0	4400.1 1700.1		8.64 48.6 9.72 28	-61-15.4 1.31-18-		9.83-08-	3.45 4£ 3.78 SE	LIMITS 2:54
VOITARUQ YTIJATOT	HTA9 HTGIW	Z¥ N∩S	NUS 9:	STSMAIO OITAЯ	ER LINE		N LIMIT		RN LIMIT LONGITUDE	ЭНТЯОИ	UNIVERSAL TIME
5e2 3.18	= T stle	a		2227	100 17 10	70 IT707 W	700 71101			ε	SAROS 14

4.02:0 4.02 4.832 0.0 7300.1 7.34-171- 7.88 3 3.84-171- 8.88 3 3.74-171- 7.44 3 STIMIJ

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TOTAL SOLAR ECLIPSE OF 9 MAR 1997

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Delta T = 52.6 Sec

ა⊖გ მ. <u>ა</u> გ	= T edi	eα					\"	1700 71101						5	SAROS 120
DURATION	HTA9	NUS	NUS	DIAMETER	R LINE	CENTE		N LIMIT	RAHTU	os	ΤΙ	N LIM:	язнтя		
YTIJATOT	HTQIW	ZΨ	TJA	OITAR	LONGITUDE	30UT;	ITAJ	LONGITUDE	<b>B</b> aut	ITAJ	adut	гоисі.	<b>B</b> aut:	ITAJ	ONIVERSAL TIME
3. ø.s	7.362	7.86	ø.ø	1.0353	ø.ε- es-	3.71	67	<b>6.72-78-</b>	Ø.T	84	2.13	-98-	6.84	Ø9	LIMITS
7.41:2	325.9	T. BOI	ø.8	3750.1	-98-53.9	6. T	67	3.72-EQI-	55. Ø	LV	7 68	-ø6-	4.88	בש	שייש
Z.8Z:2	3.788	Ø. ØII	3. QI	£8£0.1	2.02-201-	20.5	67	7.81-801-	_			-26-			94:Q
8.42:2	3.848	1.211	12.4	8880.I	9 61-901-	4.78	67	6.46-801-					35.6		84:Q 9:48
2:28.3	323.1	112.2	Q. 4I	£650.1	9.24-T&I-	Ø. 73	67	9.68-011-				-101-			Ø9:Ø
2:31.5	3.835	3.711	15.3	8680.1	1.64-601-	18.4	Ø9	-112-32.2			1 88	-9ØI-	0.80	E4 91	29:0 9:54
2:34.3	7.285	9.611	16.5	1040.1	8.84-III-	41.4	Ø9	1.81-411-			1 27	-8ØI-	2.03	E4	43:0 93:0
7.88:2	6.398	7.121	17.5	1.0404	▶.82-££1-			0.63-311-				-ØII-			89:Ø 89:Ø
£ 06.0	5 555	_ 00,												70	00.4
8.68:2	2.888	7.521	18.4	TOAO. I	3.8- 311-			4.42-711-	3.52	Ø٩	A.QE	-115-	6.0Þ	23	ø:ī
9.04:2 7.04.0	8.698	1.321	2.91	6040.1	1.68-911-	8.73	23	5.13-811-				-114-			7:5 7:5
7.24:2	9. \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\	8.72I	9.91	IIÞØ.I	I.Y- 8II-	7.42	23	-120-14.5				-112-			<b>⊅</b> : [
2.44:2	8.07£	129.6	3. Q2	£140.1	3.16-911-	Ø. £3	29	7.48-121-				-111-			9 : [
2.45.5	3. \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\	131.5	1.12	3140.1	-150-25'8	5.22	23	-122-52.5				-811-			8 : 1
7.84:2 7.74:2	7.63£	133.4	21.5	8140.1	6.11-221-	4.23	23	2.8- 421-				-ISQ			ØI:I
3.84:2	3.888 8.788	2.381 1.781	21.9	7140.1	Ø.62-821-			-125-22.3				-121-			1:15
1.64:2	1.398	Ø.681	22.3	8140.1 9140.1	3.44-421-	4.84	24	-126-35.1			4.14	-122-	10.2	99	7:I*
8,64:2	Ø. 696	6.04I	7.22	0140.1 0040 1	4.83-321-	8.82	99	0.74-721-				-123-			91:1
	~	0 1 M = T	,	0240.1	<b>₽.</b> 21-721-	2.2	99	-128-58.2	<b>4.</b> 74	24	9. Þ.I	-152-	Ø.61	<b>L</b> 9	1:18
6.64:2	8. <b>0</b> 88	142.8	6.22	0240.I	▶.32-82I-	10 TE	27	r 0- msr-	0 10	23	3 00	90 F	~		~~ -
2:50.1	328'I	7.441	22.9	1.0420	2.88-921-	0.10	73	8 61-181-				-126-			7:50
2:50.1	322.4	3,841	Ø. 82	1.0420	7.130-621-			8.6I-ISI-				-121-			1:22
Ø. Ø3: S	352.6	148.5	6.22	1.0420	132 -4.5			7.08-281- 0.24-881-				-128-			1:24
T. 64: 2	7.648	120.5	8.22	1.0420	133-18.5	2.7	69	1.43-451-				-181-			1:26
2.64:2	7.848	162.5	7.22	6140.1	8.88-481-	8.74	69	2.7- 851-				-131-			1:28
8.84:2	7.548	154.5	4.22	8140.I	136-50.1	8.62	Ø9	7.12-781-				-134			1:35 7:38
9.74:2 0.84:2	3.848	156.5	1.52	TIPO.I	4.8- TEI-	£. EI	19	8.78-881-				-132-			7:3¢
9.84:2	3.788	158.6	8.12	9140.1	1.82-851-	4.83	19	1.83-681-				-136-			1:36
8.34:2	334.5	7.09I	4.12	1.0415	-139-52.5	42.3	79	0.71-141-				-138-			1:38
9.44:5	4.188	8.291	טשט	CLVN L											
1.84:2	328.3	Ø.301	6.02 8.02	2140.1 1.0412	4.6I-I4I-	2.48	29	1.14-241-				-139-			Ø7: T
2:41.4	325.3	£.791	7.61	Ø[\$Ø']	3.83-241-	4.62	48	9.8- 44I-				-141-			1:42
8.68:2	322.3	7.69I	6.81	7040.I	8.82-441-	1.61	99	5.14-341-				-145-		79	77:I
3.78:2	8.618	172.2	1.81	3040.I				8.61-741-				-144		89	97:I
2:35.1	4.818	6.47I	1.71	2040.I	4.0- 841- 3.1- 031-			2.4- 941- 7 73-831-				-9 <b>†</b> I-			87:1
2:32.5	313.5	8.771	1.91	86£0.1	1.62-16.1	0.61	90 9	7.73-03I-				-148-			Ø9: T
2:29.5	310.5	6.08I	8.41	\$650.I	Ø'67-79I-	5 67	80 80	1.2- 231-				-191-			Z9:I
1.82:2	9. T&E	184.5	13.4	Ø68Ø.1	£.84-731-	8.8	GL GI	-155-20.6 -157-58.4				-124-			79:I
2:22:2	9.40E	7.88I	T.II	7.0385	-161-28.2	8.04	£7	4.6-18I-				-191-			99:1
		•					0.1	L'O_ TOT	0.01	т,	T . 02.	-291-	7.60	91	1:28
4.7I:2	3.108	1.491	9.6	8780.1	1.02-391-	8.28	12	-164-50.2	42.1	72	9.11.	-ØLT-	5.81	67	S: Ø
6.63:I	9.262	1.822	ø.ø	1.0351	9 11 331	a a	00								
			~.~	*00G:T	8. ÞI 39I	0.0	7.9	152 41.5	T. 4G	T.R	Ø. Þ	991	9.99	83	STIMIL

TOTAL SOLAR ECLIPSE OF 26 FEB 1998

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1:30.2

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8.311 6.742 9.82

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5.94: 5.55:	148.0 148.0 148.6 143.6 143.6 143.6 143.6 148.6 148.0	2.012 2.013 2.025 2.026 2.026 2.036	6.69 2.79 5.43 7.73 1.43 7.73 1.63 8.85 8.85	0640.1 0640.1 0640.1 0640.1 0650.1 7040.1 8880.1 8780.1	6.22 87 6.22 87 6.23 8.5 6.33 8.5 6.34 8.5 6.34 8.5 6.34 8.5 6.35 8.5	1.73 8 1.2 01 2.91 21 2.12 51 3.14 41 3.17 41 3.17 41 3.17 41 3.18 59 3.18 50 3.18	0. 41 87 0. 41 87 0. 42 83 0. 43 17 0. 43 43 0. 43	7.82 6 5.46 01 5.46 01 5.44 11 5.73 21 5.51 41 5.52 01 6.73 81 6.73 81 6.73 81 7.84 12	6.03 E7 6.03 E7 7.47 T6 6.03 E8 6.03 E8 6.03 E8 6.03 E8 6.03 E8 6.03 E8	8.75. %I 8.75. %I 8.6.9 %I 7.5. %I 16. %I	8:81 8:81 8:81 8:81 8:81 8:81 8:81 8:81
Ø.E : 4	1.941	8.202	£.27				2.8 37	8.12.6	7.04 8Y	8.28 6	17:54
8 9 : 7	Ø. Ø3.I	4.89I			1.8 77	5.43 T	1.64 87	8.81 T	0. T2 TT	2. &E 8	84:71
9.7 :4	7.031	9.181	2.47	0440.I	8.13 87	9.83.8	8.28 8Y	7.71 8	6. QI 67	8.62 T	24:71
8.8 : h			3.37		6.88 \\ \psi \	8.43 3	7.41 \\ \&8	7.81 B	1.63 \@8	6. &E 8	38:71
8.8 :4 8.9 :4	121.3	7.891	1.87	I ppg. I	82 15.3	6.73 A	81 26.1	7.12 A	82 34.5	5.48.3	ØE:71
	121.6	1221	Ø. 97	1,041	8.83 58	6.2 A	7.7E E8	3.82.5	84 12.9	€.95 ₽	<b>₽</b> 2∶71
8.7 :4	1.131	142.4	Ø.37	Opto.I	1.68 38	8.6 &	8£ 20.2	8.88 2	82 28'I	8.84 €	81:71
7.3 :4	161.6	7.151	4.87	1.0438	1.62 78	2 18:5	4.4 T8	6.14 I	8.14 T8	1.33 2	21:71
4: 2.9	161.2	123.2	2.17	364Q.I	3.6 68	I.62 I	1.13 88	₽.23 Ø	<b>6.72 68</b>	7.3 2	9 : 71
1.63:5	150.6	9.911	7.89	£640.1	1.63 %6	8.14 Q	I.I4 00	6.4 Ø	£.71 16	£.81 I	Ø : LT
3:54.3	9.64I	9,111	6:39	1.0429	1.83 29	8.E- @	9.38 26	9.04-0	6. QI E6	8.28 à	18:24
8.84:8	148.3	T. Tar	6.29	1.0425	9,23 46	I.74-0	94 3E.4	7.62-1-	6.6 36	9.0I-0	16:48
6.14:E	9.941	T. POI	9.63	6140.I	7.83 8e	1.82-1-	1.24 86	3.4- S-	9.31 76	7.13-Q	16:42
8.48:8	144.6	102.4	1.83	1.0413	8. EI 66	3.8- 2-	2.73 89	7.24-2-	7.62 66	E.&E-1-	18:38
3:25.6	142.0	7.001	52.4	3040.I	3.85 IQI	0.24-2-	101 SS'6	Ø.81-£-	101 64.4	1.8- 2-	ØE:9T
ø.81∶£	6.881	<b>7</b> .66	4.84	7880.1	0.71 AQ1	E. 41-E-	104 2.0	8.64-6-	104 32.4	8.86-2-	16:24
3: 5.4	136.3	<b>4.</b> 86	1.44	88£0.1	9.21 T&1	9.24-6-	10e es'e	8.71-4-	8.72 T&I	8.T- E-	81:91
2:53.5	1.181	8.76	4.68	9750.I	11Ø 32.2	0.8- F-	E.SI QII	4.04-4-	7.84 QII	7.18-8-	16:12
2:40.3	Ø.821	3.79	1.48	1.0362	114 24.9	6.22-4-	A.II AII	9.88-4-		4.64-8-	9:91
2:25.3	7.611	<b>₽.</b> 76	6.72	1.0345	2.01 911		118 26.4	7.2- a-	7.42 911	8.73-6-	ø :9ī
2:7.1	<b>4.111</b>	9.76	1.02	1.0322	126 35.6	4-20.4	1.02 321	9.13-4-	126 61.9	4.64-8-	72:2 <del>1</del>
≯.78:I	9.36	<b>≯.</b> 86	8.3	7720.I	9.18 8EI	2.8- E-	9.13 781	8.66-6-	3.61 681	0.86-2-	12:48
1:27.6	3.68	8.86	ø.ø	1.0260	143 63.9	8.22-2-	144 3.4	1.84-2-	143 56.Ø	3.73-1-	STIMIL
DORATION YTIJATOT	HTA9 HTGIW	Z∀ N∩S	YLT SUN	DITAR OITAR	LONGITUDE	JAUTITAL	LONGITUDE	<b>EATITUDE</b>	LONGITUDE	<b>BOUTITA</b> J	UNIVERSAL TIME
					S LINE	CENTE	TIMIJ N	SOUTHER	N LIMIT	ИОКТНЕК	
59.3 Sec	= T stl	eQ.		0007	<b>43.1.67.16</b>	. 30 :5303 \"				9	2 <b>4</b> 602 136

29 50.2 19 5.2 1.0268

8.63 81 7.32 62

23 49.2 42 53.6

8.82 82

33 57.6

3.8 et 3.81 **0**8

24 54.0 42 58.8 1.04 55 8.72 72 CIMITS

9 :61

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# 98

## Table 30

## ANNULAR SOLAR ECLIPSE OF 22 AUG 1998

8.64:2	J26.Ø	9.882	ø.ø	7736.0	-29-25.Ø 155 22.1	8.61 331 2.6- \&s-	2.8 351 9.34-82-	STIMIJ
a:00:7	E.E4I	9.682	8.11	8ø96. ø	8.22 Tat 2.82-a2-	7.7 731 3.8- T2-	7.88 Tai 2.98-32-	3:64
8:53:2			8.12	3£96.8	4.72 871 T.22-82-	3.18 371 1.0- 42-	9.22 971 8 34-22-	3 - 48
Ø.83:2	133.Ø	294.3		Z996.0	8.E- 871- 2.21-12-	6.43-771- 2.84-12-	8.21-871- 3.8E-02-	3:42
2.83:2	126.4	5.762	28.5		3.83-571- 2.22-91-	7.34-671- 6.63-61-	4.7- 47I- T.03-8I-	3:38
ø. øə: s	121.4	8.662	Ø.48	9996'Ø	4.85-071- 8.44-71-	8.52-071- 8.41-81-	4.74-071- T.41-71-	98:E
3. I. 6	A. TII	1.208	8.88	9799.Q	A 35-071- 8 AA-71-	8.16-781- 2.44-81-	8.83-781- 0.74-81-	3:24
I.E :E	Ø. ÞII	8.4QE	I.64	3896.Q	5.44-781- 8.81-81-	4.1- 381- 8.02-31-	1.72-26.6 -165-27.	3:18
3: 4:5	1.111	4.8@E	۵.74	£696.0	-14-53.1 -165-14.3			3:12
Ž: 9 : Ē	9.80I	7.8&£	7.03	@@Ye.@	9.83-281- 0.8E-E1-	8.84-26.8	9.51-531- 4.9- 5I-	8 : 8
ē.ā :ξ	3.801	Z.IIE	1.43	9079.Q	3.73-031- 4.82-21-	4.44-031- 4.64-2 <u>1</u> -	8.0I-ISI- 8.73-II-	
ã.8 ∶£	T. POI	9.818	5.73	1179.0	3.4- 631- 8.41-11-	-11-40.0 -158-51.3	8.71-631- 2.64-01-	Ø : E
a.aa	T . O.	ø.718	£. Ø9	8179.Q	8.81-731- 1.9- @1-	7.3- 731- 0.4E-01-	6.15-731- 8.44-9-	5:24
ø.e : E	I.EQI		Z. E3	0279.0	8.65-331- 7.8- 6-	9-31- 2.18-9-	8.23-331- 2.24-8-	8≯∶2
a.ar:e	8. IQI	9.0ZE			8.6- 431- 0.7- 8-	-8-31.2 -153-5Ø.9	7.81-431- 6.24-7-	2 <b>7:</b> 2
6.01:E	8.00I	8.428	8.39	£279.8	8.28-231- 9.9- 7-	4.91-231- 6.88-7-	1.84-281- 0.84-8-	2:38
3.11:6	6.66	6.628	2,89	8279. Q	6-15.2 -151 -3.5	8.03-031- 1.66-8-	2.81-181- 8.18-8-	Ø8:2
3:12.3	8.66	1.888	E. \\	8279. Q	9'8- 191- 6 91-9-	Z.42-941- 8.84-3-	5.64-641- 2.63-4-	2:24
3:12.9	6.86	3,548	1.27	Ø879.0	7.86-941- 8.52-3-		7.82-841- 0.9- 4-	2:18
3:13.4	7.8e	325.4	3.87	2879.0	5.11-841- 8.26-4-	-4-56.4 -147-58.9		2:12
8.51:5	9.86	9.S	4.47	££79.@	8.84-841- 8.44-6-	4.46-841- 4.8- 4-	-3-20.9 -146-58.8	
3.14.8	7.86	13.5	1.47	££79.@	1.22-546 -145-22.1	6.01-341- 8.52-E-	1.45-34.8 -145-34.1	9 : 2
1.41:8	ø. 66	24.5	5.47	4879.Q	1.73-641- 7.41-2-	2.34-611- 8.86-2-	0.6- AAI- 7.03-I-	Ø : 2
T.LT.0	<b>4</b> .66	7.48	4.87	££79.@	1.18-241- 9.28-1-	4.61-241- 2.73-1-	8.24-241- 7.8- 1-	J:24
3:14.1		8.84 7.15	1.27	8879.8	7.8- IAI- I.83-0	1.23-041- 7.71-1-	2.81-141-3.82-à	1:48
6.EI:E	0.001		2.07	1879.8	Ø.48-981- 8.31-0	7.22-8£1- 4.04-0	4.34-881- 8.8 @	1:45
3:13.5	8.001	Ø:13			8 20.0 -138 -1.6	3.03-751- 4.3- 0	8.21-851- 1.34 Q	1:38
0.EI:E	8. LOI	1.73	1.89	Ø£79.8	8.52-851- 136-25.8	8.11-361- 8.72 Q	7.8E-8EI- 7.8I I	Ø8:I
3:12.3	9.2@r	6.13	7.39	7279.8	3.34-451- 8.82 I	8.45-431- 8.73 Q	4.83-481- 9.94 I	1:24
4.II:E	8.E&I	7.39	1.69	3279.0	9 97-781- 8 26 1	1 25.2 -132-49.6	8.01-551- 8.81 2	81:1
4.0I:E	I. 30I	8.89	S. 03	1279.0	Z. 0- 133 - 133 I	1.83-851- 6.94 1	9.81-181- 8.44 S	1:15
1.9 :5	3.80r	8.17	2.73	717e.0	3.8- 121- 8.71 2		8.61-621- 8.7 E	9 : I
7.7 :E	Z.801	2.87	Ø.43	£179.8	1.9- 621- 8.65 2	2 11.5 -128-58.9		Ø:I
1.8 :8	Ø. ØII	T.AT	9.03	T@T0.0	2.8- T2I- 4.83 S	2 29.5 -126-50.1	2.01-721- 2.72 £	Ø · L
015 10	1.211	6.37	6.84	I@76.@	4.68-421- 8.81 E	2 43.5 -124-29.4	8.64-42I- 6.24 £	<b>†</b> 9∶Ø
8.4.8			0.54 0.31	4696.0	\$ 23.4 -122 E	2 62.7 -121-63.6	3 54.0 -122-13.3	87:Ø
8.2.8	114.5	8.87		3896.0	3.7- 911- 7.72 g	2 65.8 -118-57.4	3.71-611- 4.63 8	24:Q
2. à : £	4.711	3.77	7.88		7.84-811- 8.42 8	2.55-311- 2.13 2	8.43-311- 3.73 g	98:Q
8.73:2	8.02I	<b>6.17</b>	9.58	3796.0	7 \$6-311- 3 60 C	2 35.4 -111-26.1	3 45.2 -111- 3.34 8	Ø8:Ø
2:55.2	125.Ø	2.8T	4.82	£996. @	7.78-III- 4.01 E		3 15.6 -106-31.1	\$3.8 8.24
2:52.1	T. ØEI	2.87	9.12	9496.Q	4.71-801- 4.86 2	0.5- 801- 8.0 S		8I:Ø
Q.84:2	9.9EI	1.87	3.11	0296.0	7.04-79- 0.22 I	2.21-79- 8.88 Q	3.8-89- T.4 S	01.0
2:44.4	6.03I	1.87	ø. ø	Ø696.Q	6.81-78- 8.88-@	2.3- 78- 1.62-1-	3.43-88- 3.1- 0	LIMITS
YTIÄAJUNNA	HTGIW	Z¥	TJA	DITAR RATIO	LATITUDE LONGITUDE	LATITUDE LONGITUDE	LATITUDE LONGITUDE	UNIVERSAL TIME
DURATION	HTA9	NUS	14112	DIAMETER	CENTER LINE	SOUTHERN LIMIT	NORTHERN LIMIT	
29:1 2ec	=   67	ιeα						2 <b>4</b> K02 135

VANULAR SOLAR ECLIPSE OF 16 FEB 1999

					R LINE	CENTE	N LIMIT	SOUTHER	N LIMIT	<b>ИО</b> ВТНЕВ	
DURATION YTIRAJUNNA	HTA9 HTGIW	Z¥ N∩S	TJA TJA	DIAMETER 0ITAR	LONGITUDE	I BOUTITAL	LONGITUDE	<b>BOUTITA</b> J	LONGITUDE	<b>AUTITAL</b>	ONIVERSAL TIME
4.81:1	ø. 96	106.5	ø.ø	3776.0	2.3- 8-	T.48-14-	7.36-7-	-41-55.2	T.T- 8-	2.8- 14-	LIMITS
8.81:I	3.08	6.36	7.11	8086.0	4.44-22-	8,18-44-	9.62-12-	2.14-44-	-23-52.Ø	1.12-44-	Ø :9
8.7 : t	ø.88	7.38	8.12	3886.Q	-34-52.6	6.81-84-	6.81-4E-	8.18-84-	-32-24.9	1.2- 84-	9:9
6.E :I	1.09	6. TT	7.72	£386.8	8.0- £4-	3.1- TA-	7.68-24-	4.81-74-	2.12-64-	7.84-84-	21:3
3.0 :I	54.1	Ø.17	32.9	9986.0	7.28-64-	6.6I-TA-		2.48-74-		7.3- TA-	2:18
3.73:0	2.64	4.48	8.78	7786.0	a. T- 88-	1.22-74-	-24-28.1			T.8- T4-	6:24
6.43:0	45.2	1.83	6.14	8886. Q	8.2- <b>0</b> 8-	8.21-74-	7.83-63-			I.Q- 74-	Ø8:3
Ø:52.4	6.14	8.13	8.44	≯686.0	6.82-48-	-46-54.3	8,42-49-			8.24-84-	5:36
1.03:0	1.68	3.34	6.74	1066.0	2.08-89-	7.82-84-	6.82-89-	7.68-84-		8.71-84-	27:9
I.84:0	7.88	Ø.68	7.03	T066.0	7.21-27-	6.73-34-	5.21-27-	3.Y- 84-		1.74-84-	2:48
£.84:0	7.48	4.28	53.3	2166.8	0.65-37-	-46-20.8	7.66-37-	4.08-34-	£.8E-3T-	2.11-34-	<b>79:9</b>
						2 22 , ,	- 02 02		~ ~ ~ ~ ~ ~		2 0
7.44:Q	Ø. EE	72.4	9.33	9166.8	3.13-87-	6.65-44-	1.83-87-	9.84-44-	0.03-87-	9.0E-44-	ø : 9
8.43.3	9. IE	1.81	4.73	6166.8	-81-52.3	1.33-54-	9.43-18-		0.03-I8-	7.84-84-	9:9
1.24:0	3.08	3.01	ø. 63	2266.8	6.24-48-		8.34-48-		0.04-48-		21:9
I. I4: 0	7.62	9. Ş	Z. Ø3	9266.8	8.42-78-			5.62-24-		0.8- S4-	81:8
8.04:0	1.62	3.438	1.18	9266.8		4.12-14-	5.8- 00-			1.41-14-	42:8
8.68:0	8.82	3.848	3.19	7269.8		8.42-04-		7.18-04-		3.71-04-	ØE:9
₽.68:@	7.82	6.755	9,19	8266.8		2.32-68-		1.25-95-		8.8I-6E-	98:9
£.6E:@	6.82	3.9.8	2.19	8266.8		5.52-85-		I.0E-8E-		8.81-85-	ZÞ:9
9.68:Q	8.62	322.Ø	4.09	7269.8	ø.72-66-			8.32-75-		4.2I-7E-	84:8
8.68:Q	ø.ø£	7.4IE	8.93	9266.0	9.14-101-	-36-12.5	8.14-101-	1.61-86-	1.48-101-	- 6.3- 88-	9:24
4.04:0	à. IE	e. Tae	8.73	4266.0	1,33-501.	- 36 -3.4	4.I- 40I-	- 35-10.1	6.8≯-£@I-	- 8,83-46-	ø : L
E.14:0	8.28	9.10E	6.33	2266.0		- 33-61.9		- 33-58.6		- 3.34-66-	9 : T
8.42.3	9.55	6.362	8.63	8166.0		- 8.78-28-		-32-44.6		- 8.0£-2£-	7:15
9.E4:0	35.8	7.062	51.3	\$166.0		- 3.02-1E-		- 3.72-16-		- 3.51-15-	
2.45.2	1.88	6.882	9,84	~		- 3.0- 0E-		- 3.7- &£-		- 29-63-1	42:T
Ø. 74: Ø	8.04	9.182	9.34			- 28-36.3		- 7.84-82-		- 8.82-82-	ØE:7
0.64:0	Ø. 44	7.772	42.1			- 0.8- 72-		- 7.31-72-		- E.Q- T2-	9E:7
4.13:0	8.74	274.1	8.88			- 26-34.3		-26-42.5		- 26-26,3	24: T
1.43:0	52.29	7.072	9.58			- 8.63-62-		- 2.3- 42-		- 23-45.5	8 <b>7</b> :48
2.73:0	9.73	3.732	6.82			- 8.6- 22-		-22-12.3		-21-64.9	
*****									_ 0 001	2 07 01	
Ø.1 :1	4.48	4.482	8.52			- 7.73-91-		- 20 - 6.5 -		- 0.64-61-	
Ø.8 : I	Ø.47	1.192	£.4I	6286.0	/ * T b = Ø b T ·	- 1.81-71-	Q'GZ-T+T-	- 17-25.Ø	6.0- 0+1-	- Ø: II-ZI-	9:8
1:13.5	8.68	2.732	ø.ø	6876.0	8.63-631	- 0.66-81-	154-18.3	- 13-61-	163-55.4	- T.EI-EI-	LIMITS

SAROS 140

SAROS 145

Table 32

TOTAL SOLAR ECLIPSE OF 11 AUG 1999

Delta T = 64.5 Sec

6:42:3	6.33	1.982	ø. ø	ØEIØ.I	6.8- T8-	17 35.4	0.6- T8-	6.61 <i>T</i> 1	6.42-78-	9.94 TI	STIMIL
4.7 :I	Ø.67	9.672	7.71	2810.1	8.82-49- 9.84-87-	26 54.2 23 11.1	0.83-63- 8.8- 07-	25 43.2 23 4.0	8.72-17-	8.4 82 8.71 62	12:24 12:30
4.9I:I	1.88	7.872	3.08 0.32	8120.1 1.0203	I.88-88-	0.7 82	6.22-63-	8. £3 <u>T</u> 2	T. T2-09-	1.02 82	12:18
1:53:1	Ø.99 8.49	I.882 9.172	35.2	1820.1	Ø.8- 88-	3.5 å£	2.46-33-	2.84 62	1.86-88-1	9.81 QE	12:12
8.44:I 4.78:I	102.5	1.492	8.98	1,020.1	-52-42.9	4.64 IE	1.61-23-	A. 28 18	Ø. E1-E3-	32 6.1	9 : 21
1:51.4	106.3	7.632	6.24	1.0250	6.8£-6≯-	2.72 88	1.01-64-	8.8 &&	2.8- @3-	33 45.4	12: Ø
£.73:1	4. TØI	1.882	ø. 94	1.0257	1.74-84-	8.83 48	0.61-84-	1.68 48	9.31-74-	36 18.3	11:24 11:48
8.2 : S	I.ear	Ø. Ø32	6.84	1.0264	8.8- pp-	36 25.1	1.88-84-	1.4 88	8.08-44-	7.8 88 8.34 88	24:II 84:II
£.7 :2	E. QII	244.5	4.13	1.0269	7.42-14-	8.84 TE	3.83-04-	7.42 TE	6.13-14-	5.72 95 7 8 85	11:36
2:11:3	2.111	238.5	9.63	1.0274	0.64-8E-	8.4 <b>6</b> 8	6.62-86-	1.14 88	8.41-68-	0.24 04 5 70 05	Ø8:II
8.41:2	8.111	Ø.282	9.33	1720.1	3.41-86-	Ø.81 Ø₽	3.03-38-	8.63 68	8.2- 48- 9.88-88-	0.83 IA	11:24
7.71:S	112.2	6.422	Ø. 73	1.028@	8.68-88-	41 28.Ø	6.81-88-	8.2 14	8.42-18-	4.0 E4	81:11
6.61:2	112.4	3.712	2.83	1.0283	e.s- 15-	42 34.4	7.14-0E-	4.8 24	9.24-82-	2.4 44	21:12
2:21.5	112.5	3.602	6.83	1.0284	2.82-82-	4.78 EA	7.8- 82-	3.01 E4	0.73-32-	45 4.3	9:11
2:22:6	112.3	E.IQZ	59.3	1.0286	6.66-32-	7.88 44	8.12-22-	1.6 44	7.3- 52-	8.0 84 5 1 3	ø:II
2:22.9	0.211	9.291	5.63	3820.1	1.03-22-	4.28 34	8.46-22-	1.4 34	7 3- 60-	8 20 81	
2:22:6	9.III	184.4	6.83	1.0286	9.43-61-	2.42 84	7.14-61-	46 65.3	8. T- \Q	ø. 63 84	79:01
7. IS: S	0.111	Ø. 971	I.83	1.0285	9.13-81-	6.11 TA	5.14-81-	8.24 84	8.1- TI-	2.14 74	10:48
I.02:2	E. OII	8.791	6.93	1.0283	7.68-81-	2.33 TA	-13-35.5	8.32 TA	6.84-81-	48 24.9	10:42
9.7I:S	4.60I	8.631	4.88	1820.1	Ø.81-01-	8.88 84	0.41-01-	9.8 84	8.12-01-	8.8 64	10:36
0.31:2	£.801	152.ø	3.53	8720.I	6.44-8-	Ø.7 6₽	3.44-8-	2.78 84	0.34-8-	6.88 64	Ø8:ØI
2:11.4	I.TOI	8.44 <u>I</u>	51.3	1.0275	6.83-2-	4.48 64	₽.S- E-	8.4 64	-2-65.1	1.4 03	10:24
1.7:2	105.6	ε. Υε <u>τ</u>	7.84	ALSO.1	8.I I	Z.33 64	I.43 Ø	0.82 et	6.6 I	5Ø 24.4	81:01
2:2:1	6.E&I	Z.0EI	6.34	1.0265	9.61 3	4.8 @3	4.7 B	6.68 64	5.28.8	6.88 &a	10:15 10:0
1:56.4	6. IQI	123.3	7.24	1.0258	8.73 <b>e</b>	8.21 \@3	3.04 6	8.34 64	6.41 QI	5.04 03	9 :01 9 :01
6.64:I	4.66	4.811	1.65	1.0250	3.63 AI	7.8 Q3	8.78 AI	9.04 ea	16 22.2	8.28 \\ \text{\alpha}_3	ומי פ
0 07-1	, 00	, , , ,							0.1 1S	4.11 03	<b>79:6</b>
1:45.5	9.96	₽.6ØI	Ø.35	1,0241	8.28 \QS	4.74 e4	20 6.5	49 23.2	8. E2 72	6.28 94	87:6
0.48:I	7.26	1.201	E.QE	47.0229	8.84 82	0.11 ea	76 15.4	4.64 84		5.72 84 5.25.91	Z7:6
1.42:1	8.78	9.46	8.42	1.0214	4. QI 48	8.6 84	8.62 88	8.13 74	44 35.8 34 52.2	1.35 34 1.35 34	98:6
9.11:1	3.08	8.38	I.TI	EEIQ.I	4.14 64	Ø. 4S 84	7.84 SA	1.21 84	N 3E 8	1 36 84	26.0
3.84:0	6.03	۲.69	ø.ø	1.0143	1.83 48	7.8 IA	6.63 49	4. TA 04	8.81 38	1.81 14	LIMITS
YTIJATOT	МІDТН	Z∀	Τ⊐Α	OITAЯ	ONGITUDE.	J BOUTITAJ	-ONGITUDE	LATITUDE L	ONGITUDE.	J BOUTITAL	TIME
VII MATOT	HTA9	กั∩ร	NOS	DIAMETER							ONIVERSAL
HOTTAGUIG	III	14110			FINE	CENTER	1 LIMIT	SOUTHERN	TIMIT I	NORTHERN	

TOTAL SOLAR ECLIPSE OF 21 JUN 2001

၁ဓင	е.	QQ.	= 1	Bυ	127

8.43:2	121.9	8.E&E	Ø.81	8040.I	Ø.64-88-	5.42-9I-	I.02-68-	Z.EZ-@Z-	8.1Z-8E-	6.82-81-	13:24
3:12.7	9.09I	8.908	Ø.32	1.0428	Ø.3- 55-	Ø.83-81-	-33-23.5	9.23-71-	-32-48.5		13:18
7.2E:E	3.731	3.608	4.0E	1.0443	-28-51.3	7.71-81-	9.4- 62-			4.42-41-	13:15
3.74:8	3.571	1.218	8.48	1.0454	-25-23.5	8.2- 11-	9.88-32-		-25-14.1	8.6- 51-	13: 6
7.0 : A	9.87I	9.418	7.85	£840.I	I.42-22-	1.3- 51-	9.28-22-	9.83-51-	2.81-22-	0.21-21-	73: Ø
,	0 02.	0 / 10	2 00	COVD	F 10 00-	r 3- 6r-	-33-33 6	-13-50 8	0 81-00-	8 CI-CI-	13.0
4.21:4	3.581	8.718	Ø.24	1740.1	2.44-61-	+12-20.4	ø:29-61-	0.41-EI-	1.75-61-	1.72-11-	15:64
7.22:4	6.78I	321.1	6.44	7740.I	E.81-71-	1.84-11-	9.32-71-	6.65-21-	7.11-71-	9.23-01-	12:48
7.18:4	3.191	3.428	3.74	1.0483	0.E- 3I-	9.0Z-II-	Ø.01-31-	3.41-21-	9.83-41-	6.82-01-	12:42
€.98:4	7.46I	328.4	7.64	7840.I	-12-55.8	8.2- 11-	7.2- EI-	6.83-11-	5.64-21-	0.6- QI-	12:36
9.34:4	1.791	332.6	9.19	0640.I	7.43-01-	9.23-01-	9.1- 11-	Z.84-II-	1.84-01-	Ø.83-9-	72:30
4:60.5	Ø.661	2.788	Ø. £3	£640.I	5.83-8-	3.74-01-	8.3- 6-	7.14-11-	3.13-8-	8.63-6-	12:24
Ø.43:4	1.002	342.0	1.43	4640.I	4.8- 7-	1.64-01-	8.21-7-	5.64-11-	5.83-8-	1.33-6-	12:18
1.93:4	9.002	I.748	8.43	3640. I	6.41-3-	4.88-QI-	4.22-3-	8.03-11-	8.Y- 3-	8.5- QI-	21:21
7.88:4	5.002	352.3	2.83	9640.I	8.82-E-	4.6- II-	7.88-8-	4.6- SI-	4.8I-E-	7.31-01-	12: 6
Ø. 93: 4	4.66I	3.738	1.33	3640.I	7.78-I-	9.72-II-	8.34-I- 7.56-6-	7.12-21-	8.62-1-	4.48-01- 7 31-01-	15: Ø
	, ,,,	0 230		3070 1	7 76-1-	0 20-11-	8 31-r-	7 10-01-	9 60-1-	A 65-01-	Ø .C!
6.53:4	6.7 <b>6</b> I	6.2	7.43	\$6\$Ø'I	8.01 Q	Ø.23-II-	8.2 Ø	-15-42.5	6.81 Q	7.83-01-	11:24
4.68.4	3°96T	1.8	6.63	2640.I	4.0 S	T.IZ-ZI-	1 52.4	Ø.31-81-	7.8 <u>2</u>	8.82-11-	84:11
7.34:4	1.591	ø.ei	7.23	6840.I	3.52.2	4.73-SI-	3.44.2	E.03-EI-	3.0 b	6.4- SI-	ZÞ: II
9.68:₽	I.06I	9.7I	1.13	9840.I	I.74 3	<b>₽.</b> 68-81-	5.95.3	9. IE-4I-	4.33 3	2.74-SI-	98:11
4:32.3	7.88£	6.IZ	2.64	2840.I	8.84 T	0.82-41-	I.85 7	2.02-31-	9:43 7	2.86-61-	ØE: II
4:23.8	6.281	Ø. 92	6.84	9740. I	9 52.2	0.42-3I-	2.34 6	6.31-31-	8.63 6	8.28-41-	11:24
4:14.2	6.87I	7.62	8.44	0740.I	12 6.0	4.82-81-	8.63 11	0.02-71-	9.21.21	8.75-31-	81:11
5.5 :4	3.471	2.88	2.14	£840.I	6.05 AI	4.24-7I-	14 25.8	8.88-81-	8.88 41	9.13-31-	21:11
8:51.3	8.69I	8.88	8.75	1.0454	9. 01 TI	1.8- 91-	3.7 TI				9:11
9.75:5	7.48I	8.68	8.55	1.8443	20 12.5			<b>7</b> :69-61-	E. 31 71	3.71-81-	
0 20.0	2 /31	30.6	33 0	EVVD L	3 61 96	7.84-02-	9.11.0S	2.04-12-	20 14.6	6.73-61-	ø : t t
8.22:8	Ø:69T	Ø. E4	2.62	1540.1	8.84 EZ	9.64-22-	7.64 ES	6.14-62-	8.34 ES	-21-68.2	79:01
3:3:5	122.4	46.5	23.5	4140.1	28 15.9	-25-22.ø	2.82 82	5.81-82-	8.7 82	8.82-42-	87:0I
7.84:2	6.5AI	6.03	6.31	1680.I	3.44 48	9.83-82-	9.81 38	5.83-62-	34 2Ø.3	9.73-72-	7ø:42
					• • • • • •	0 02 00	0 01 20	0 02 00	0 20 70	0 23 20	0, 2,
<b>6.8</b> : S	8.721	6.63	ø.ø	1.0343	2.88 64	8.82-88-	9.34 64	2. QI-7E-	8.71 &3	-36 -5.3	STIMIL
YTIJATOT	HIGIW	Z∀	TJA	OITAR	LONGITUDE	30017177	LONGITUDE	3001T1V7	LONGITUDE	3/017177	<b>JMIT</b>
DURATION	HTA9	Nns		DIAMETER	7.01 ITTOMU 1	adilttt 1	POLITION I	2011TTTA 1	EQUITTOING I		UNIVERSAL
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					311 1 G	コエはコン	TINI I N	934TI IO2	TINT I N	GOUTGON	
56.9 Sec	= T 631	θđ								,	SAROS 12
0 0 20	- 11	J		Taaz	NOC TZ IO	70 IT707 VI	7700 74101				OF SUGAS

7.01:5 8.151 3.862 0.0 4860.1 5.23-43- 1.85-82- 7.1- 33- 1.02-72- 8.45-33- 0.11-82- 21MIJ

ANNULAR SOLAR ECLIPSE OF 14 DEC 2001

\$2:38 I.3Z 68 I.75 7 I'Ø9 88 9.72 6 9.6 68 4.IE 8 1.191 243.1 ø. gt Ø196. Ø 8.12:E 2.48 9 22:24 5.84 8 2.43 36 €.63 4 9. Wh 36 £696'Ø 6.74 36 123'1 7.142 4.82 8.82:8 22:18 8.42 00I I.YI E 4.71 001 4.84 A Ø. I A 240.5 29.62 8096'0 100 21.4 3.88:8 6.74I 22:12 9.1 104 J.S 2 3 26.6 103 56.3 I.83 E&I E. 44.3 1296'Ø 2.952 34.6 Z.48:E 143.9 22: 8 0.8 TOT 3.8 I 7.8 TOI 9.84 I 2 26.6 1Ø7 1.3 IE96'Ø 6.752 Ø.6£ 3.7E:E 6.01I 8.84 801 4.04 I Ø : ZZ 4.84 601 8.12 Q I.34 80I 8.0 I 6896'Ø 7.04:5 138.4 **236.4** 6.24 51:24 8.6 ZII 7.4 I 8.21 112 12.83 Ø 8.41 ZII I.SI-0 9.94 7496.8 136.3 8.482 3:43.5 21:48 114 26.4 I.O O 4.62 AII 8.78-0 114 23.3 8.7£ Ø 7.64 £996'Ø 134.6 232.5 0.84:E 116 27.4 4.8I Q 27:12 3.48 SII 8.33-0 6.08 SII 9.81-@ 6996'Ø 1.881 7.0EZ 7.23 3.84:8 92: IZ 0.28 8II 8.8- I-8.52 811 8.3 @ 8. &£-& 4.33 ₱996.0 9.72 SII 2.722 8:68.8 131.9 -1-12.6 120 23.5 S1:38 120 14.2 €.1- Q 8996'Ø 12Ø 18.8 I.78-0 6.73 8.0EI 8.522 3:51.6 3.63 ISI 7.2- @ 21:24 0.01 221 0.51-I-122 4.8 0.8E-0 Z196'Ø 8.612 1.09 3:52.7 129.8 123 40.9 6.0 Ø 21:18 6.88-8 -1 -8.4 123 52.5 123 46.7 6.8ZI 215.3 6:19 4786.8 3:53:8 21:12 £.9 @ 125 31.9 I'69-Ø 0'61 9ZI Ø-25.Ø 3.59 LL96.0 125 25.4 128.Ø Ø. ØIZ 9:54.Ø 21: 6 8.8 T21 8.34-@ Ø 22.4 126 64.6 3.I 72I 9.II-Q 7.48 6786.8 127.2 2.402 3:54.1 Ø : 12 £.8 @ 3.54 821 0.72-0 128 28.2 6.68 Ø 128 35.8 9.39 Ø896'Ø 3:53.9 156.5 8.791 8.0 0EI 7.I I 78:64 0.71 0E1 3.4- 0 8.8 QEI 3.82 Ø 6.39 1896. Ø 125.8 1.191 8:53:5 7.64 IEI E.SS & 2.28 181 0.82 I 84:02 1896'Ø 9.04 ISI 0.44 0 184.2 8.39 152.2 3:52.3 20:42 9'89 I Ø 23.4 133 22.1 3.6 EEI 133 12.8 1 25.8 1896.8 3.771 5.39 1.13:5 124.7 3.88 S 28:38 1 28.8 134 54.9 134 35.4 134 45.1 Q.I S Ø896'Ø 3.64:8 124.3 I.ITI 4.49 Ø8:0Z 1.EI E 8.85 381 8.8 S 1.8 8.1 136 18.3 7.04 S 3:47.9 1.391 1.59 6796.8 124.0 78:0Z 8.8 8£I Ø. E3 S 137 42.4 8.73 E LL96'Ø 1.63 781 9.32 E 8.631 **₽.13** 3:45.9 124.0 8T:0Z 2.41 4 139 41.4 3.24 8 139 19.2 3.84 4 9196'Ø 5.0E 9EI 4.63 7.E4:E 1.421 1.881 141 22.2 3.85 4 14Ø 59.2 0.14 8 20:12 8.8 3 7.01 IPI 2.73 2736.8 3:41.4 124.5 6'Ø9T 9:02 5.7 541 4.85 3 142 43.6 2.14 8 142 66.4 9.8 8 7.43 6996'Ø 6.88:€ 125.2 2.741 Ø : ØZ 9.73 AAI E.SA 8 7.88 AAI 7.74 T 9996'Ø 144 45.7 8. Þ. T 6.13 4.88:8 1.821 Q. PPI 7.33 841 0.33 T 7°I 6 19:61 Ø.82 8 1.18 31.1 8.84 146 43.4 6996'0 7.55:5 4.72I I.IPI I.E 941 7.31 9 87:61 148 38.3 18 23.2 5.64 6 7996'Ø 148 50.6 1.921 138'2 42.5 8.8E:E 15Ø 58.4 6'#9 II Zp:6I 0.62 131 7.34 QI 7486.8 9'ØI I9I I. QZ II 8.14 1.82:E E.IEI 136.2 98:6T 13 2.8 5.0 ABI 2.72 SI 163 36.4 82 SI 153 48.2 7.78 8£96.8 133.9 3:25.2 1.481 3.2 781 0.42 AL 156 40.3 Ø. 65 3I Ø8:6T 8296.8 126 51.2 2.1 31 1.55 3:22:8 137.5 T.IEI 18:54 6.42 Ø91 7.2 8I 16 42.4 160 43.4 9.88 &a1 Z. 22 TI 8,72 9196'Ø 142.Ø 129.4 3:19.Ø 18:18 21 6.5 165 25.1 1.12 02 9.88 331 9.38 9I ØØ96'Ø 165 28.9 148.2 1.821 2.12 3:12:6 19:12 24 56.2 173 42.8 2.82 871 8.83 82 7.8 471 3.73 32 4736.0 122.6 S.II 8.II:8 128'6 1.2- 871- 1.84 QE **STIMIJ** 1.52-371- 8.12 62 2.3- 871- 4.43 62 ø.ø 4436.8 7.7 : 8 Ø.ITI 3.711 LATITUDE LONGITUDE LATITUDE LONGITUDE LATITUDE LONGITUDE TIME RATIO **YTIMAJUNNA** MIDTH ZΥ TJA NIVERSAL NOS DIAMETER SUN **HTA9** DURATION NORTHERN LIMIT CENTER LINE SOUTHERN LIMIT SAROS 132 Delta T = 66.3 Sec

4,4 4[

2.22 97

9.0

0.942

176.4

3.51:5

1896'Ø

7.32 EI

3.84 37

Z. 61 87

14 58.3

LIMITS

8

Table 35

### ANNULAR SOLAR ECLIPSE OF 10 JUN 2002

0.7 :I	8.27	7.462	ø.ø	1186.0	6.33 <b>1</b> 04 55.9	1 3.0 301 3.18 91	3.78 101 8.4 02	STIMIL
9:83:ø	8.33	7.882	1.81	8986.0	ø.73 811 8.13 5	2 5.22 e11 6.34 32	8.08 8II 3.73 32	ØE: I
ø.53.ø	46.5	1.482	Ø. 42	9789.8	9. £3 821 7. £ 9		8.75 321 8.6 92	1:24
7.84:0	I.04	Z. \\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	3.08	2686.0				81:1
Ø.84:0	35.2	4.872 0.880			1 5.2 132 33.5		31 13.2 132 22.8	
			ø. 9£	9066.0	2 36.3 137 14.8		8.8 TEI 0.44 SE	1:12
8.14:Q	31.2	7.272	T. 04	3166. Q	2,12 141 4,84 8		1.31 141 7.63 66	9 : 1
6.88:Q	6.72	Ø.692	1.34	£269.8	1.4 341 1.14 4	E 7.8 341 8.48 48	3.63 441 6.74 48	ø :t
2.8E:0	72.1	2.382	1.64	1866.8	5 23.4 148 30.0	3.66 841 1.71 36	3. 82 841 8. 62 38	<b>†9:</b> Ø
8.88:Q	7.52	261.3	8.23	7866. @	7.24 131 8.33 8	36 49.6 151 45.3	36 1.3 151 40.1	8 <b>†</b> :Ø
7.1E:Q	7.0Z	1.732	5.33	Z466.0	8.14.41. 3.81.8		36 24.0 164 42.9	ZÞ:Ø
7.62:@	Ø.61	7.232	9.69	7466. Q	0.88 731 7.88 8		8.85 731 7.85 85	9£:Ø
Ø.82:0	3.71	8.742	8.59	1369.8	8.62 631 8.14 8		36 46.3 16Ø 23.Ø	ØE:Ø
9.8Z:0	£.9I	4.242	8.39	4366.8	9.2 £81 Ø.84 8		8.2 881 4.74 88	Ø:24
8.32:0	15.3	2.882	9.83	7366.8	6.38.3 165 36.3		36 42.4 165 36.3	8I:Ø
8.24.3	9. Þ <u>r</u>	6.822	2.17	6369. Q				21:0
8:23.6 6.03.5	Ø. Þ.Ľ	228.1	9.57					9 : Q
0.52:0				1966.8	2.82 NTI 9.11 8		36 15.7 17ø 28.7	
M . CO . M	9.81	<b>₽.</b> 602	9.37	2996. à	8.74 271 6.03 3	8.84 271 8.74 38	4.84 271 3.43 38	Ø :Ø
7.22:Q	13.4	2.861	I.TT	Z966.@	5.26.8 175 3.2	36 21.4 175 2.2	35 28.5 175 4.3	Z3:24
9.22:Q	£.5I	7.08I	Ø.87	£966.8	8.81 771 E.48 4		34 57.7 177 16.8	23:48
8.22:Q	13.5	6.£9£	1.87	2966.8	0.32 971 9.81 A		34 22.4 179 26.5	23:42
Z.82:0	8.51	7.741	3.17	1966.8	1.82-871- 1.65 E		33 42.5 -178-226.4	23:36
6.83.9	£. Þ.Ľ	8.EEI	1.97	Ø966. Ø	2 54.7 -176-23.3		32 58.2 -176-21.3	82:52
8.42:Q	Ø.3I	1.221						
			2.47	8366.8	0.02-47I- 0.8 S		8.71-471- 8.6 28	23:24
6.32:0	15.9	Ø.EII	9.17	9966. Ø	8.71-271- T.St t		31 16.4 -172-15.2	23:18
2.72:0	Ø. TI	105.6	4.69	£366.0	0.81-071- 0.81 0		1.61-071- 8.81 QE	23:12
7.82:0	18.3	9.66	9.88	Ø366. Ø	1.41-891- 3.21 9		7.01-831- 8.81 es	23: 6
3.0E:0	8.61	7.4e	8.69	8466.Q	1.11-331- 8.3 8	8.41-881- I.I 8S	28 9.5 -166 -7.3	23: Ø
4.2E:0	9.12	þ.06	3.09	1466.Q	1.8- 481- 6.23 8	26 48.4 -164-10.5	8.1- 481- 8.73 82	55:24
9.4E:0	7.ES	8.88	2.73	9866.Q	1.83-131- 0.35 3	26 30.3 -162 -3.0	1.63-161-7.98 32	22:48
Ø.7E:@	1.82	8.88	8.63	Ø£66.0	4.34-631- 0.11 4	24 6.0 -169-61.1	7.85-931- 0.81 AS	22:42
9.68:Q	8.82	7.08	1.03	Ø.9923	2.82-731- 2.84 2		7.91-731- 3.34 22	22:38
4.24:0	8.2E	2.87	2.84	9166.0	0.83-43I- 3.1 I		21 7.1 -164-50.4	22:38
9.34:0	35.6	6.3 <u>7</u>	6. I 4	9066.0	9 13.3 -152-16.9		19.2 - 152 - 8.1	22:24
8.84:0	9.98	8.57	8.78	3689.8	4.71-641- 0.81 T		9.8- 94I- 2.9I YI	22:18
9.53.6	6.44	9. <u>17</u>	1.28	£889. a	7.64-341- 4.83 4.		16 2.8 -145-36.9	22:12
6.83:0	1.13							
2.2 : [ 0.83.0	–	1.07	6.32	788. Q	7.46-141- 8.41 2.		12 21.2 -141-18.3	9:22
00.1	<b>9</b> .69	3.89	6.71	9486.0	1.14-351- 8.34 8	7.4- 8EI- 3.04 8	0.71-351- 7.03 8	22: Ø
3.21:1	2.87	Ø.78	ø.ø	8679.@	0.64-021- 4.02 I	0.43-021- 4.1 I	8.62-021- 8.7£ I	LIMITS
YTIAAJUNNA	WIDTH	Z∀	TJA	OITAЯ	TITUDE LONGITUDE	CATITUDE LONGITUDE LA	LATITUDE LONGITUDE	<b>3MIT</b>
DURATION	HTA9	กักร		RETEMAIG	adiationo i adiatit	1 2011TOHO 1 2011TTA	2017TO10   2017TTA	ONIVERSAL
		,	14113	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	CENTER LINE	SOUTHERN LIMIT	NORTHERN LIMIT	. TOGIATINI
					רבעודכם ו דגוכ	TIMI   MGBUTHO2	TINI   MGBUTGOM	

5

SAROS 137

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# Table 36

TOTAL SOLAR ECLIPSE OF 4 DEC 2002

Ø:22.3	8.82	244.4	ø.ø	6900.1	5.62-241-	3.28-82-	0.16-241-	E.7E-82-	8.12-241 <b>-</b>	2.82-82-	STIMI
0:04:0	<b>4.7</b> 4	255.3	£.81	1.0125	1.23-52.1	-32-21.3	9.31-421-		₽.62-E2I-		9 :6
8.34:0		261.5	4.82	8410.1	9.54-311-	I.SE-8E-	9.2- 811-	1.24-88-	-116-23.4	-38-21.9	ø :6
7.73:0	3.33	3 190	V 30	0710 1	<b>D</b> 07						
	7.70	2.782	32.5	1.0165	3.82-801-	8.81-04-	4.I4-60I-	7.62-04-	Ø.8- 9&1-	7.E- @4-	8:24
8.7 : t	2.13			9710.1	-183-58.3	4.05-14-	1.41-401-	9.94-14-	6.24-801-	1.31-14-	84:8
7.31:1	7.39	272.5	8.78			8.22-24-	8.02-66-	3.68-24-	8.63-86-		8:45
1:23.2	€.69	<b>9.77</b> 2	42.4	0610.1	I.04-46-			7.81-84-	Ø.62-46-	7.68-24-	8:38
ø.ae:r	4.27	8.882	3.84	1.0200	L WV-VO-	6 03 UV	7.04-06-	Z. 04-E4-	8.52-86-	8.0- £4-	Ø£:8
Ø.88:I	6.4T	8.882	4.03	1.0208	7.18-06-	9 00-61-		1.23-54-	2.28-88-	7. &I-E4-	8:24
3.14:1	S.TT	9.462	Ø.43	1.0215	3.86-38-	4 18-84-			5.43-28-	6.01-E4-	81:8
I:46.3	1.67	7.008	8.73	1.0221	6.83-28-	4.28-84-	4.2- 68-	8.63-64-			21:8
9'Ø9:I	8. Ø8	8. T&E	4.09	1.0226	4.62-67-	3.42-64-	1.18-67-	4.84-64-	9. TS-6T-	3.2- 64-	9:8
1:54.2	2.28	314.4	Z. £9	1.0231	8.0I-8Y-	8.8- 64-	6.6- 8Y-	6.08-84-		6.84-24-	
8.73:1	4.68	322.4	7.39	1.0235	I.I- 87-	9.34-24-	1.83-27-	ã.8- £≯-	2.4- ET-	Ø. £2-2≯-	ø :8
6 73.1	, 60	, 000								·	
1:69:8	9.48	8.188	6.78	1.0238	ø. ø9-69-	7.31-24-	8.43-69-	2.86-24-	S.3- @T-	1.63-14-	<b>1:54</b>
		4.148	7.69	1.0240	3.8- T8-	7.68-IA-	2.63-88-	1.2- 24-	8.51-79-	2.71-14-	8 <b>7</b> :7
2: 1.6	<b>92.4</b>	3.238	I.I7	Z+20.1	6.61-48-	8.73-04-	7.01-49-	0.02-I4-	1.62-49-	9.35-04-	24:7
2: 2:9	1.88		6.17	1.0243	7.65-13-	9.01-04-	7.82-19-	4.28-04-	9'09-19-	7.84-eg-	98: <i>T</i>
8.8 :2	8.88	7.4		1.0244 5100 t	ø. 3- 93-		3.23-83-	4.68-68-	4.71-63-	9.83-86-	Ø8:7
7.E :S	ø.78	4.71	1.27		Z.3E-83-			5.14-85-	Ø.64-83-	8.63-78-	42:T
2: 3.3	S. 78	6.62	7.17	1.0244			4.43-53-	£.85-75-	8.42-43-	7.73-88-	81:7
2: 2:2	€.78	9.I4	T.&T	1.0243	9.6- 49-			4.08-88-	4.6- 23-	2.13-36-	7:12
9.Q :S	2.78	1.23	2.69	1.0242	6.74-13-		8.0I-94-	8.71-38-	8.44-64-	9.65-45-	9:7
1:28'2	6.88	2.19	2,78	1.0240	3.72-64-	8.83-46-			2.72-74-	8.52-55-	ø :Z
1:55.8	3.88	ø:69	6.48	7820.1	8.e- TA-	6.14-££ <b>-</b>	6.13-84-	6.63-88-	G LG-LV-	33-03 6	<b>D</b> - <b>L</b>
	8.38	7.37	2.29	1.0234	9.13-44-	9.02-28-	Ø. EE-44-	2.78-28-	2.01-34-	8.2- 26-	8:24
1:52.7			5.63	0820.I	2.88-24-	6.23-08-	0.41-24-	Z.8- IE-	-45-62.3	3.86-0E-	
6.84:I	6.48	4.18	2.83	1.0225	7.21-04-	Z.02-62-	1.83-68-	-29-35.5	Z.28-04-	7.4- 62-	Z≯:9
7.44:1	7.88	<b>4</b> .88		9120.1	2.84-78-	2.14-72-		8.33-72-	0.8- 8£-	7.82-T2-	98:3
0.04:I	1.28	7.0e	8.23		3.71-38-			9.8- 82-	3.78-38-	8.14-32-	ØE:9
7.48:1	Z. Ø8	3.46	1.64	1.0212		1.1- 42-		2.81-42-	8.73-25-	8.84-62-	
1:28.8	8.TT	6.7e	2.3≯	1.0204	<b>≯.</b> 76-26-		9.22-62-	8.7- SS-	8.5- Q5-	6.34-12-	
1:22.3	8.4T	e.øar	8.04	3610.1	4.84-62-	-51-26.9		8.64-61-	1.64-82-	I.0E-6I-	
1:31:1	Ø.IT	a.eat	Ø.8E	4810.I	8.82-82-	8.66-61-			5.1- 52-	4.83-81-	
8.8 : I	ø.99	1.901	3.08	ØΓΙØ.Ι	3.04-22-	4.4- TI-	9.61-22-	2.21-71-	3.41-81-	8.63-61-	
Ø. 73: Ø	2.63	4.80I	8.62	1.0152	9.23-TI-	-13-59.5	2.18-71-	1.3- 11-	3 41-81-	-13-63 8	Ø · 8
0.44:0	9.8 <b>4</b>	9.QII	4.41	1.0125	1.04-01-	6.84-6-	6. A1-Q1-	2.03-6-	2.3- 11-	€. 74-e-	2:24
שיייי ש	9 01	0 011						0:0	Z.65 I	£.64-£-	LIMITS
1.82:0	8.18	2.211	ø.ø	1800.1	£.14 1	9.73-6-	7.84 I	8.6- 4-	0 05 L	S OF S	STIME I
	WIDTH	Z∀	ΤJA	OITAR	TONGILODE	LATITUDE	LONGITUDE	<b>EATITUDE</b>	_ONGITUDE	LATITUDE	TIME
NOITARUO YTIJATOT	HTA9 HTGTW	NOS		DIAMETER						NEW YORK	UNIVERSAL
1101110110	, 1,46 Y W				B LINE	CENTE	N LIMIT	SOUTHER	TTMT_ V	NORTHER	
											SAROS 142
o⊖2 I.T∂	= T et	l a(I					UDINE 20EN				

### ANNULAR SOLAR ECLIPSE OF 31 MAY 2003

8.14:8	2.888	E. &TS	ø.ø	9046.0	158 29.3	0.0 0e	6.42 08	8. Ta Ta	6.42 @8	£.73	LIMITS
3.04:8	7.668	E. &YS	I. QI	4046.0	8.8 831	ø. ø   øe	Ø. ØÞ 83	2.02 IT	8.61 83	9.13.79	Ø8:4
8.04:E	6.000I	3.87	1.6	1046.0	0.72-01-	6.4.38	ø. eε 13	2.7 ET	Ø. YI 33	1.14 78	82:4
4.68:€	3.7211	35.1	I.8	8659.8	7.62 å£	I.91 08	2.62 84	I.9 47	8.81 23	8.82 T8	92:1
6.88∶€	7.062I	I. ØE	ø.Ţ	3659.8	3.13 48	1.11 77	8.41 14	1.84 47	8.61 64	E.EI 78	4:24
8:38:8	Ø. Ø131	4.82	6·3	2659.8	3. 53 35	2.88 47	0.E 8E	5.8 37	2.82 84	1.83 88	4:22
7.78:8	1.8281	8.72	8.4	8659.8	35 58.3	8.62 27	9.1 IE	4.01 87 2 3 37	5.85 EA	8.88 88	4:28
			• ,	2000 2	0 01 10	0 00 02	0 1 16	7 D. 32	6 96 61	0 86 88	DC . A
I.78:E	2314.9	8.72	3.6	9886. Q	8. 4E 3E	I.el at	7.81 82	6.8 37	40 50.2	9.31 99	81:4
4.88:8	3241.6	3.72	2.2	£8£6.@	32 7.9	3.41 89	ZI 63.1	8.74 47	2.8 88	65 52.3	91:1
3:35.7	6.8313	<b>8.7</b> 2	8. Ø	6756. Q	34 26.9	9.81 99	17 63.5	74 23.1	\$5 30.4	8. YZ 38	<b>71:7</b>
3:36.5	7.6894	1.18	2.2	£856.@	3.8 &£	3.5 73	Ø. 61 11	73 61.8	32 56.7	9.0 39	4:12
8.88:8	1.2844	7.55	8.2	4886. @	26 46.3	1.63 99	3.6 II	73 14.5	3.72 ØE	1.25 48	ØI:10
9:38:8	6.6034	7.35	6.2	≯8£6.@	24 1.9	8.88 33	8 24.Ø	2.28 27	Ø.2 82	1.2 48	8:1
8.88:8	4.3894	2.78	7.2	4886. Ø	8. Ø3 IS	P. 09 99	E.1.8	4.34 IT	8.04 82	7. ØE E9	9:17
3:36:5	8.6864	1.88	2.2	2826.8	9.61 &S	8.74 48	9.63 8	7.43 QT	8.82 82	9.73 28	7:7
3:35.7	2182.8	3.75	3.0	87.59. @	8. ES &S	82 53.Ø	7.71 2	Z.0 07	7. QI IS	8.52 28	4: 5
7.88:8	8.8888	6.14	4.2	£856.0	1.78 41	63 58.2	Ø 24.3	1.2 99	þ. Í 91	4.84 13	ø:v
4.78:E	2421.4	1.94	۲.٤	9886. Q	8.44 6	9.88 49	9.11-0	4.0 89	16 55.9	6.11 Ið	3:28
Ø.8£∶£	1,6391	9. ØS	6. Þ	6886.8	I.9 4	8.8 38	I.0- I-	9.43 99	14 64.0	2.48 08	3:28
8.88:8	9.6291	8.33	ø. 9	Z686.8	7.41-2-	6. 88 39	ε· ῖε- i-	6.44.3	12 55.6	3.33 63	3:64
3.98:8	8.6681	4.28	1.7	3656.0	9.21-01-	2.63 39	8.54-I-	5.82 <del>1</del> 8	4.0 II	8.31 63	3:52
8.68:8	1227.5	3.57	2.8	7656.8	2.41-52-	7. EZ 33	8.88-1-	£.4 £8	9.8 6	5.35.83	93:E
8.40.3	I.Ee@I	8.18	2.9	ØØ46.Ø	2.52-25-	T. TA 88	9.52-ø	8.72 I8	9.61 Y	8. 53 73	3:48
9.04:8	1.386	<b>4.</b> 18	Z. ØI	£046.0	2.53-55-	4.II 78	2.64 \( \text{Q} \)	8. 22 ea	3.65 3	8.11 73	3:48
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3.14:8	9.426	8.18	ø.ø	4046.0	0.81-88-	1.72 78	4 32.5	66 46.Ø	4 32.5	6.84 83	LIMITS
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### TOTAL SOLAR ECLIPSE OF 23 NOV 2003

9.8E:I	₽.8@3	0.271	ø.ø	TEEQ. I	1.6- 81-	<b>▶.</b> 61-17-	7.24-12 <b>-</b>	6.3- 68-	<b>4.</b> 13-8-	6.4£-69-	STIMIJ
9 96.1	7 022	2 021									Z3:I0
3.74:I	3.564	122.4	6.8	\$98\$.I	8.74-48-	<b>6.62-77</b> -	1.43-82-	6.61-ET-	9.62-14-	8.8- \\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	23:8
9.64:I	Z.064	7.841	Z. ØI	1.0364	1,14-24-	3.2- 8 <i>T</i> -	9.33-36-	0.23-47-	6.7E-03-	2.02-08-	
1:51.4	8.784	9.141	2.11	8980.I	8.82-03-	7.81-87-	2.42-54.2	<b>▶.</b> 86-37-	6.12 <b>-</b> 63-	9.51-08-	23: 6
8.23:I	8.384	J35. Ø	1.21	alea.1	4.84-73-	7.11-87-	1.68-64-	1.73-37-	I.e- 78-	6.03-67-	23: 🖈
1:54.0	485.6	129.3	8.21	2750.1	5.42-49-	9.13-77-	₽. T3-33-	9.33-37-	8.74-67-	6.31-67-	23: 2
	9.384 9.301	124.4	13.4	4780.1	I.8- &Y-	8.61-77-	8.66-18-	6.86-37-	3.81-67-	6.1E-8T-	23: Ø
1:54.9	A 391	7 701	,	7202 -							
	0:00+	120.4	8.81	97£0.1	3.2- 37-	0.65-87-	8.14-99-	2.01-37-	4.84-68-	E. IÞ-77-	22:58
1:55.7	8.384	S.TII	2.41	7750.1	I.8- 97-	<b>≯.</b> I3-37-	9.2- IT-	5.28-47-	3.82-78-	2.84-8T-	22:58
1:28:3	3.784	7.411	14.5	8750.1	3.18-28-	7.83-47-	1.34-47-	2.74-£7-	6.12-0e-	8.74-37-	22:54
1:56.7	4.684		9.4 <u>ſ</u>	8750.1	9.81-38-	I.S- 47-	0.23-77-	4.83-27-	£.24-26-	8.81-17-	22:52
0.73:I	6.164	112.8	7.41	9750.1	4.48-78-	5.2- ET-	E.72-08-	0.1- 2T-	Ø.48-46-	8.54-57-	22:5Ø
1.73:1	6.464	4.111		9758.1	I.42-68-	I.0- 27-	6.46-28-	8.1- 17-	Ø.2- 8e-	Z.6E-27-	22:48
1.73:1	4.864	4. ØII	7.41		1.13-06-	7.88-07-	8.71-48-	£.63-69-	I.@I-76-	3.55-17-	22:48
Ø.73:1	4.203	8.60I	9.41	8780.1	9.83-19-	£.64-69-	Ø. 65-38-	8.53-89-	▶.I- 86-	8.82-0Y-	22:44
1:56.7	6.903	3.60I	14.5	8780.1	0.64-26-	I.I4-88-	4.04-88-	4.34-78-	1.88-86-	8.81-69-	22:42
1:56.2	8.113	3.60r	14.2	TTEB. I		I.IE-78-	8. EZ-78-	1.46-39-	8.I- 99-	4.6- 89-	22:40
1:22.6	1.713	7.60I	8.51	8780.1	8.62-66-	1 18-79-	8 60-70	1 76 00	0.00	, , ,	
					0:44-06-	ø.er-88-	Z.64-78-	9.61-39-	7.EI-66-	8.83-88-	22:38
1:64.8	7.223	I.QII	£. ££	AYEQ. I	8.44-66-	8.4- 39- 8 91-33-	8.73-78-	2.1- 48-	8. 4 <u>I</u> -99-	8.84-38-	22:38
1:23.8	528.4	7.0II	8.21	2780.1	Ø:19-66-		3.84-T8- 5.73-79-	9.7E-S9-	3.4- 66-	6.28-48-	22:34
1:52.6	1.483	3.111	0.21	QTEQ. I	8.54-56-	8.74-E9-		8.7- I3-	4.84-86-	8.81-58-	22:32
1:13:1	<b>₽.</b> 683	115.5	2.11	7980.1	8.12-56-	4.82-28-	4.61-78-		8.0I-89-	7.73-13-	22:38
4.64:I	7.843	8.511	I. ØI	1.0364	6.24-26-	9.0- IS-	8.6- 88-	6.82-63-		8.48-03-	22:28
E. 74: I	1.848	116.3	8.8	\$358. I	9.24-16-	8.72-63-	6.6- <b>≯</b> 8-	7.62-73-	8.62-76-	8 16-23	80.00
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I.8I:@	£.4I	2.872	₽.8I	Z966'Ø	1.81 Ø8	6.62 8	I.e &8	Z. 9Z 8	2.71 \@8	<b>3.</b> ££ 8	22:12
3.7 : g	8.8	2.472	1.92	£866.8	8.48 38	4.73 T	8.28 38	8.33 Y	7.38 38	6.83 T	52: 6
3.0 :0	Þ.Ö	4.472	1.25	6666. g	7.8 IE	3.6 T	9.8 IE	₽.8 T	8.8 IE	9.6 T	Ø : ZZ
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TT.3 :0	3.4	7. 47S	1.78	1.0012	6.74 46	<b>4.81 8</b>	8.84 46	4.41 8	Ø. TA 48	4.SI 8	51:24
TI.II:0	9.8	4.872	9.14	I.ØØ22	2.23 76	7.11 3	6.83 76	9.61 3	9.03 Te	6'6 9	21:48
TI.8I:0	12.1	2.872	9.34	IEØØ'I	8.18 @at	Ø.8 A	1.48 001	3.8 A	3.62 @@I	3.5	21:42
T3.02:0	1.31	Ø.872	2.64	6800.I	1.83 201	Ø. 73 S	102 E6.Ø	I.a E	102 50.2	5 23.9	21:36
T3.4S:0	7.71	Ø.082	9.23	9400.I	105 Ø.2	I 45.3	102 3.6	6.84 I	104 26.8	8.14 I	21:30
TI.82:@	6.6I	282.5	7.33	1900.1	Ø. 93 801	8.18 Q	106 59.8	Z.38 @	106 52.2	8.72 Q	21:24
TS.18:0	7.12	9.382	9.83	7300.I	108 42.9	6.44-Q	0.74 801	7.04-0	7.88 8@I	I.64-0	21:18
T0.48:0	8.82	3.682	2.18	1900'1	110 22.4	1.6- 2-	6.82 @II	9.83-1-	e. Ti aii	3.Y- S-	21:12
TE.8E:@	24.5	1.462	9.69	1.0064	111 56.1	1.82-8-	6.0 SII	<b>⊅.81-</b> £-	111 61.3	7.72-E-	57: 8
TS.88:@	22.5	8.662	9.39	7900.I	113 25.1	6.44-4-	1.88 E11	I.@4-4-	113 20.1	7.64-4-	21: Ø
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T8.68:0	2,82	1.808	ε. 78	&Υ&&.Ι	114 60.4	3.8- 8-	114 25.8	3.5- 8-	114 45.3	6.61-8-	20:54
Te. 04:0	7.82	8.818	9.89	2700.I	1.81 811	8.88-7-	5.81 311	8.82-7-	8.7 811	7.8E-T-	20:48
TT. IA: 0	6.82	9.128	<b>7</b> .69	£700.1	8. EE 711	6.0- e-	2.68 TII	6.33-8-	117 28.5	6.3- 6-	20:42
TØ. S4:0	Ø.72	7. & E E	9.69	4700.I	118 63.6	6.62-&1-	6.83 811	8.42-01-	1.84 811	6.48-01-	20:36
T0.54:0	6.82	8.688	4.69	4700.I	9.21 \QL	7.0- 21-	2.81 \\ \Delta 18.3	7.33-11-		-12 -5.8	20:30
T3.14:0	9,82	3.848	8.89	4700.I	121 33.8	8.88-81-	8.88 ISI	9.82-21-		8.88-81-	20:24
Te.84:8	1.82	8.838	4.78	ET00.I	122 54.4	9.8- 31-	122 59.6	9.6- 31-	122 49.2	9.61-31-	ZQ:18
T7.68:0	25.4	3.5	8.39	1700.1	124 18.2	6.34-81-	124 23.3	Ø.14-81-	124 13.1	8.03-91-	20:12
TS.88:0	9.42	6.6	8.88	6900.I	126 45.4	7.82-81-	125 50.3	-18-20.9	126 40.6	9.08-81-	20: 6
TE.8E:Q	23.5	12.6	4.18	9900.I	2.71 721	2.8- \Q	8.12 721	8.E- \\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	3.21 721	9.SI-8S-	20: 0
T0.48:0	2.22	9.02	8.83	£900.I	0.33 8SI	8.63-12-	£.63 82I	£.64-12-	128 50.6	-21-68.3	19:61
TE.IE:Q	7. 82	25.1	Ø. 93	6300.I	130 40.5	7.24-82-	130 44.5	4.85-52-	138 86.5	0.74-E2-	87:61
T2.82:0	Ø. 91	2.62	9.23	1.0054	9.88 SEI	5.35-32-	3.95 281	4.15-32-	132 32.4	3.65-32-	79:45
T7.42:0	6.8I	ά. εε 0. ος	3.64	8400.I	134 44.2	7.28-72-	8.74 AEI	8.62-72-		₽.8E-72-	98:61
TT.02:0	14.5	Σ. 9£	6.34	1400.1	2.9 751	1.35-92-	7.11 781		7.8 781	<b>▶.8</b> £-62-	Ø8:6T
TE.81:0	Ţ, ţţ	4.04	6. <u>I</u> ≯	EEØØ.I	139 56.4	8.54-15-		1.14-18-	139 64.6	9.84-18-	19:24
T2.11:0	£.8	2.44	3.75	EZØØ.I	143 14.5	3.0- 48-	1.31 541	<b>4.83-66-</b>	143 13.4	3.2- 46-	81:61
I3.3 :0	2.4	4.84	3.28	ZIØØ.I	9.71 TAI	3.72-88-	4.81 TAI	4.82-86-	4.71 TA1	-36-28.6	21:61
Z.I :@	ø. r	53.3	9.9Z	7666.0	152 34.4	4.e- ee-	152 34.3	7.6- 68-	152 34.5	2.6- 68-	9:61
9.6 : Ø	1.8	8.63	1.91	7766.8		0.71-24-	£.41 091	9.61-24-	8.EI @9I	9.41-24-	Ø :61
Ø.42:0	0.E2	3.87	6. <i>t</i>	7866.@	£.44 TTI	T.23-84-	8.01 871	0.4- TA-	8.02 TT	0.54-84-	18:24
0.07.0											
£.82:@	28.3	3.87	ø.ø	£269.0	6.62-371-	9.93-74-	1.42-24.1	2.3- 84-	8.12-371-	6,64-74-	STIMIL
YTIAAJUNNA	MIDTH	Z∀	T⊐A	OITAR	LONGITUDE	LATITUDE	LONGITUDE	LATITUDE	LONGITUDE	<b>EATITUDE</b>	TIME
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ANNULAR SOLAR ECLIPSE OF 3 OCT 2005

Delta T = 189.4

3.84:8	2.712	8.382	ø.ø	8£46.0	£.82-28 <del>-</del>	6.88-6-	5.44-28-	9.48-01-	2.63-28-	7.35-8-	STIMIL
		7.732	9.II	8946.Q	6.75-17 <b>-</b>	£.64-6-	9.11-07-	9.14-01-	£. 31-57-	6.43-8-	12:18
3:56.2	7.802		3.12	£649.8		6.2- 6-	-62-12.4	2.64-6-	I.7- 48-	9'91-8-	15:15
8.8 :4	202.1	1.692		8039.0		9.1- 8-		7.44-8-	2.34-83-	8. TI-T-	15: 8
6.8 :1∕	1.861	8.692	1.82		0.03-63-	3.43-8-	7.31-53-	8.35-Y-	1.34-43-	Z.EI-8-	75: Ø
Ø.81:4	6.4er	9.692	33.5	Ø236.0	9 99-63-	3 /3-8-	7 31 63	D 36 L	, , .	0 0. 0	
4.31:4	Ø.261	2.692	1.85	Ø836.0	£.84-@3-	7.E4-3-	₽.8- @3-			3.4- 3-	11:24
2.91:4	2.681	3.892	42.3	8£36.0	2.8- 84-	8.0E-4-	8.32-74-	4.T- Z-	1.74-84-	1.63-6-	84:11
7. IS: 4	9.88I	3.782	I.84	9796.0	2.34-34-	-3-12.5	Ø.8- 34-	6.03-E-	6.42-84-	9.66-2-	11:42
7.82:4	9.881	ø. 882	9.64	1996'Ø	4.04-E4-		1.2- 64-	Ø.88-2-	1.91-44-	£.42-I-	11:38
		1.482 232	8.23	7336.8	1.84-14-		9.0I-I4-	6.8I-I-	1.82-24-	8.T- @	##:11
4:25.5	5.181		8.33	1936.8	6.3- 04-			I.9 Ø	I.54-04-	4.01 I	11:24
6.82:4	7.87 <u>f</u>	8.192		9996.0	7.1E-8E-	1.83 1	2.33-78-		4.8- 68-	9.6Z Z	81:11
1.82:4	1.871	268.9	9.83			5.61 5		1.64 S	8.04-TE-		71:15
1.62:4	7.87I	7227	2,13	8996.0			9.3- 3£-		3.71-88-		9:11
6.62:4	4.171	2.132	8.69	<b>0736.0</b>		4 41.4				1.48 8	ø :II
4:30.6	£.691	1.842	7.39	8738.0	4.62-46-	<b>8.4</b> 8	1.84-88-	9.38 3	9.63-46-	1 12 8	D
6.08:4	8.79I	I.042	3.78	4736.0	8.8- 88-	8.82 T	3.88-28-	2.0 T	6.54-55-	8.73 T	10:64
	165.6	2.552	9.89	9739.0	2.83-18-	Ø. 43 8	5.12-16-	7.32 8	2.18-28-	7.22 g	8 <b>7:</b> ØI
2.18:4		2.525	ø. ør	8739.8	3.34-08-	10 20.3	8.0I-0E-	2.23 6	5.02-IE-	7.84 &I	70:45
4.18:4	1.481		9. QT	8739.8	8.35-92-	7.74 II	E.1- 62-	7.61 II	₽.@I-@E-	Ø. 81 SI	10:36
4.18:4	162.8	8.912		8739.8	4.82-82-			12 48.3	6.8- 62-	13 44.6	Ø8:ØI
4.18:4	8.191	8.702	T. &T			1.84 41		Ø.81 41	0.13-72-	16 14.6	10:24
2.18:4	1.191	8.861	E. NT	3736.0				0.64 3I	9.65-82-	Ø. 84 81	81:ØI
6. ØE: 4	9.09I	£.0e1	4.69	4736.0		£.71 81		8.12 71 8 91 31	0.72-32-		zī:øī
3.0E:4	4.09I	182.5	1.89	£739.0	8.23-42-					19 53.8	9 : ØI
Ø. ØE: 4	3.09r	176.4	3.88	1736.Q	2.78-82-		2.8- 82-	Ø 99 81	-24-11.3		Ø :ØI
4.62:4	6.09I	1.931	64.5	8936. à	6.71-22-	2.0 12	1.44-12-	4.08 02	6.13-22-	4.08 IS	ישי ש
1.02.5	3.131	9.691	8.29	9996'Ø	6.83- <u>0</u> 2-	1.85 22	-20-20°5	4.7 SS	7.72-12-	ø.e es	<b>†</b> 9:6
7.82:4		7.831	8.63	Z996.8	6.82-81-	24 18.Ø	<b>▶</b> .03-81-	23 46.4	9.73-61-	24 EØ.Ø	87:6
8.72:4	162.5		1.73	8339. Q	5.84-71-	£.0 82	Z.EI-7I-	8,72 82	9.61-81-	<b>≱.£</b> 6 33.4	Z⊅:6
8.82:4	7.E9I	154.2		£336.8	4.63-31-	2.34 72		1.11.72	2.28-81-	7.61 82	9:38
4:25.6	165.3	1.031	2.43		8.0- 11-	1.55 92	9.82-21-		8.28-11-	1.6 أ	Ø8:6
2.42:4	2.791	146.3	Ø. 13	7436.0	9.84-II-		8.31-11-		0.81-21-	8. S SE	9:24
9.22: <b>₽</b>	3.691	3,241	8. TA	1436.0				7.68 28	2.84-9-	8.63 ££	81:6
8.02:4	272.3	ø.eei	Ø. AA	\$536.0	7.EI-6-	33 19.5	2.44-8-			3.2 88	21:6
9.81:4	175.6	135.2	Ø. 04	9236.@	8.41-8-	32 IB't	8.74-8-	0.78 AE	8.14-8-		9:6
Ø.8I:4	9.671	Z.IEI	8.38	9136.Q	1.04-2-	2.32 TE	7.81-Z-	3.68 88	2.8- 8-	9.11.88	
4:12.9	184.5	1.821	3.08	9096.0	I.TA I	3.88 68	8.4.3	7.84 8E	8.0E I	1.62 @4	ø :6
~.~	01007	0.177	24.5	Ø676. Ø	8.04 T	4.2 24	2.84 T	£.7 I4	7.78 T	42 58.8	8:24
Ø.6 : A	6.061	121.3			7.55 31	9.44 44	8.6 9I	43 41.4	7.8 71	1.03 34	81:8
7.8 :A	5.002	7.EII	9.91	QT46.Q	7 66 91	3 77 77	0, 0 0 1				
3:52.9	0.222	7.86	ø.ø	8249.0	6.82 88	3.6 84	8.33 88	3.11 74	88 24.9	1.21 64	STIMIZ
YTISAJUNNA	WIDTH	ZV	TJA	DITAR OITAR	_ONGITUDE	1 BOUTITAJ	-ONGITUDE	J BOUTITAL	BOUTIONO.	1 BOUTITAL	UNIVERSAL TIME
NOITARUG	HTA9	NUS	NUS	GITINITO	S FINE	CENTER	4 LIMIT	SOUTHER	TIMIT	ИОВТНЕВИ	
oe2 ≯.68	= T st	l e (I				: \		n.,		1	SAROS 134

Table 41

TOTAL SOLAR ECLIPSE OF 29 MAR 2006

### 2.42:2 141.3 2.432 6.3I 9680'I 4.4 -72-48.4 5.83-17- 1.02 03 6.34-67-Z7:II 7.84 13 2:42.5 148.2 7.542 6.6- 18-25.3 1.0420 -61-20.3 49 18.5 1.88 84 E.@4-I8-4.4 QS 98:11 9:99:2 163.2 Ø.982 31.5 8540.I Ø.78-83-0.42 TA 9.86-63-6.88 84 4.68-83-8.6 84 Ø8:II 4.8 :8 167.2 7.622 8.88 1.0452 8.44-74-1.88-74-45 27.3 7.43-74-1.84 44 1.21 84 11:24 3.81:5 7.09I 0.422 8.14 1.0464 E.1- E4-7.05 54 6.81-64-4. TA SA 6.44-24-4. PI PP 8T:II 3:72:8 1.531 7.812 7.97 4740.I 6.4- 68- 6.48 IA 2.72-68-4Ø 62.7 Q. E4-8E-42 17.6 11:15 8:38:8 \$.89I 213.6 I.64 1.8482 8.24-38- 8.04 68 1.6- 86- 2.63 86 -32-16.8 7.12 ØÞ 9:11 3:42.1 6'89I £.80Z 52.5 6840.I 7.84-28- 0.74 TE 1.81-88-0.7 TE -32-17.5 8.72 8E ø:II 0.84:E I.ITI 6.202 9.33 9649° I 7.01-0E-Ø.33 38 1.81 35 Ø.68-62-5.48 38 -30-42.5 10:64 8:53:E 173.2 1.791 58.4 2.42-82-1.05Ø 9.03-T2-5.4 45 4.82 88 7.81-72-34 42.6 87:ØI 3.73:5 176.1 6.0er 6.09 3030.I 8.24-82-8. AI 28 @.81-82-8.78 18 3.7- 32-2.23 28 Z>:0I 8.0 : b Ø. TTI Ø. 48I Ø. £9 1.0588 -23-45.2 3.82 @8 9.12-42-2.03 62 3.8- 62- 6.2 18 38:01 E.E : 1 7.87I 176.5 8,49 1190'1 4.33-12- 1.68 82 -22-32.9 8.71-12- 7.41 es 8.8 82 Ø8:ØI I'9 :> 5.08I £.891 1.99 1.0513 9.11-02- 3.28 82 2.03-02- 8.71 82 4.88-91- 4.72 TS 10:54 £.8 :4 6.18I 3.631 Ø. 78 1.0514 1.88-81- 8.8 32 1.21-91-7.28 42 8.63-71- 0.14 3S 81:ØI 7.8 : 4 183.3 120.4 £.73 319Ø'T 8.73-81- 7.12 82 Z. 78-71- Z.84 ZZ 8.71-81- 8.88 82 ZI:ØI 4.8 :4 7.481 141.3 1.78 319Ø'T 4.42-3I- 2.78 IS 2.4-8I- 2.4 IS 0.44-41- E.0I SS 9 : ØI 6.3:4 182.9 132.6 4.88 1.0514 7.28-41- 3.02 e1 2.23-51- 1.53 91 4.11-81- 7.32 @S Ø :ØI 8.8 : 4 Ø.78I 124.5 2.39 8.86-11- 4.14 81 1.0513 9.91-21- 2.9 8I 8. &- EI- I. 7E TI 79:6 1.1:4 **6.781** E. TII 8,59 1130.1 4.84-QI-16 25.6 8.72-II-16 53.8 Ø'9- ØI-3.73 81 87:6 3:67.9 188.5 I.III 9'19 1.0508 9. ØI-6-14 42.1 ø.23-9-9.01 PT 8.82-8-8:45 9.EI 3I 3:63.9 1.69 6'88I 7.30I 1.0505 0.1E-T-12 58.4 7.21-8-2.72 21 Ø.64-8-3.62 EI 98:6 Z.64:E I.IOI 6.88I 7.99 1.050Ø 2.84-8-3. PI II 2.82-8-3.54 QI 6.6- 3-3.34 II Ø8:6 7.84:8 **≱.88**I 8.79 53.4 3640'I Z. ØE 6 4.43-6-7.8E-4-T.II-E-6.0 QI **≯.**63 8 42:6 ε. 7ε: ε 287.3 I.46 1.03 1.0488 2.53-1-7 45.3 6.35-2-T.AI T Z.QI-I-8.15.8 81:6 0.08:E 182'4 **7.16** 9.94 1840.I I.OZ Ø 9.63 3 Ø.62-@ 1.62 3 9.E I 8.62 8 3:15 3:21.6 182.6 €.68 9.24 1.8472 6.64 5 4 12.6 2.8 2 3 42.4 3 34.1 4 45.6 9:6 3:12:8 8.871 8,78 1.85 1940.I 4.72 8 5.24 8 6.82 Z 3.73 4 0.43 I 2 63.5 Ø :6 3:1:5 173.6 5.38 Ι. εε 8440.I I.7 6 6.28 Ø 8. \QZ 8 4.8 Q 1.43 6 I.S.I 8:24 £.8≯:Z 166.3 9:98 2.72 1.0432 13 23.6 8.12-1-12 34.3 9'Ø9-I-0.41 41 8.53-@ 81:8 0.2E:S 128'1 2.38 7.6I QI+Q'I 7.81 e1 @. £2-E-1.12 81 3.03-5-9.71 **0**2 6.33-2-24:8 4.4 :2 1.881 6'98 ø. 9 8980.I 31 25.8 34 23.8 4.74-8-7.22 62 2.6- 8-7.62-3-8:38 1:63.8 128.8 9.98 ø.ø 6450.I I.4 7E 8.71-8-6.23-8-9. IS 7E I.8 7E 1.44-3-LIMITS YTIJATOT MIDTH ZΥ TJA RATIO LATITUDE LONGITUDE LATITUDE LONGITUDE LATITUDE LONGITUDE TIME **DURATION HTA9** NOS NOS DIAMETER **UNIVERSAL** CENTER LINE SOUTHERN LIMIT NORTHERN LIMIT Delta T = 69.8 Sec SAROS 139

6.82-86- 7.48 18

8.85-86- 0.0 14

£. 0- 66- 6.8 Sa

**STIMITS** 

3:13:1

126.4

9.972

ø.ø

7+50.I

97

6:18:3	3.225	Ø. 172	ø.ø	1226.0	9.44-48-	<b>-63-24.9</b>	Ø.11-88-	0.63-43-	7.72-39 <del>-</del>	9.83-13-	LIMITS
0 10.7	_ 000										13:54
6.53:3	2.862	8.682	6.41	9976'Ø	8.12-24-	-21-36.8	7.34-44-	2.22-23-	4.24-04-	7.73-64-	13:24
3.7:9	2.882	7.662	Ø. E2	8729.@	-31-32.8	7.02-e4-	0.51-25-	2.43-03-	-31-11.2	6.13-74-	13:12
8.71:8	4.872	7.80£	6.82	6826.0	4.78-42-	<b>4.11-74</b> -	0.78-42-	3.88-84-	4.84-42-	4.64-84-	
9.32:9	9.272	312.3	8.55	ØØ86'Ø	9.32-91-	3.Y- 34-	3.3- er-	6.32-84-	4.84-91-	9.13-64-	13: g
	I.882	E. 71E	ά.8ε 0.00	80£6.0	Ø.81-31-	1.8- 64-	1.84-41-	0.12-44-	-12-21.3	2.73-14-	73: Ø
6.28:9	1 890	6 216	£ 00	0200 2							
a	2.492	8.128	8.14	9186.Q	8.53-11-	-41-15.6	2.41-11-	6.02-24-	-12-33.9	0.8- 04-	12:64
Ø.68:3		3.828	6.34	2226. 8	6.0- 6-	4.02-8E-	1.81-8-	8.42-04-	7.34-6-	8.71-86-	12:48
4.44.8	7.192		3.84	8259.8	3.18-9-	5.15-75-	Ø. 54-3-	5.28-86-	7.61-T-	7.1E-8E-	72:42
Ø.64:8	4.632	330.5		ZEE9.8	Z. \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\	8.44-35-	2.62-6-	6.24-88-	6'ØI-9-	0.84-48-	12:36
ø:53.ø	7.732	8.488	4.13		4.62-2-	7.8- 48-	9.08-I-	2.83-46-	8.31-6-	8.8- EE-	12:30
3.83:8	228.4	8.688	1.43	7889.0	I.88-Q	7.81-28-	ğ 16.3	9.21-88-	8.18-1-	-31-56.5	12:24
<b>9</b> .63:9	9.332	1.448	9.83	0156.0		7.85-05-	1 53.4	I.0E-IE-	Z. E. Ø	5.84-62-	12:18
1.2 :7	1.332	1.648	8.83	8489. Q	Ø:89 Ø		8.22 £	I.03-62-	Ø. IE I	3.11-82-	12:12
2.4 : T	1.332	354.6	r. @a	9469. Q	9.82 2	6.8- e2-		6.21-82-	2 52.9	1.86-82-	17: 8
Ø. 9 : 7	222.4	a.a	4.29	8489. Q	2.64 8	3.62-72-	1.84 4	2.35-32- 2.58-35.5	1.01 4	9.1- 32-	77: Ø
£. 7 : 7	1.882	8.8	8.89	6456.Q	۵.۲ a	2.84-32-	4.4 8	-36-2E E	LWLV	0 1 30	2 0.
				~~~~	~·** ^	1.41-42-	0.61 T	4.0- 32-	6.23.6	7.82-22-	11:24
£.8 :T	1.732	9.EI	6.49	Ø386. Ø	0.12 8			8.82-22-	4.48 8	-21-56.6	11:48
ø.e : 7	228.6	8. \\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	8.39	1389.0	7 32.2	2.14-22-	8.0E 8	-21-54.4	I. 54 7	-20-25.3	11:42
£. 6 : 7	₽.09Z	2.82	6.39	2359. Ø	4.14 8	4.6- 12-	8.04 e		8. 63. 8	9.43-81-	11:36
ε. ę : <u>Υ</u>	9,292	35.6	6.39	1369.0	£.64 6	3.86-61-	8.84 QI	-28-23.2		1.32-71-	Ø8:II
ø.e : Ţ	1.392	45.9	4.39	1986.8	6.83 &£	3.8- 81-	11 26.8	9.83-81-	9.73 <b>6</b>		11:24
£.8 :7	Ø.892	7.64	8.48	Ø356. Ø	8.4 SI	£.6E-81-	13 6.1	7.62-71-	6.4 II	Ø:99-91-	81:11
2.7 :7	2.172	1.83	4.89	6456. Q	13 I3.4	6'ØI-9I-	14 14.6	-16-55.4	12 13.0	3.72-41-	
8.3 :7	7.472	8.19	6.18	7456. Q	14 23.9	1.84-81-	12 SE.8	9.72-41-	8.22 EI	3.63-21-	11:15
	4.872 7.672	6.88	Z.09	9756. Ø	9.7E 31	-15-12'8	7.6E 3I	I.I- EI-	14 35.1	9.1E-1 <u>I</u> -	9:11
8.1 :7 0.4 :7	8.282 A.870	4.17	1.83	2459.0	16 53.5	2.64-01-	2.73 TI	6.4E-II-	8. 83 BI	7.4- QI-	ø : I I
81.7	2 000	, ,,	. 02								L0107
1.63:9	<b>4.88</b> 2	2.37	8.33	6556. Q	9. <b>1</b> 1 81	0.52-6-	8.91 91	▶.e- @I-	8. 01 TI	7.7E-8-	10:64
	3.062	8.87	5.53	9889.8	19 41.3	2.73-T-	4.74 QS	3.44-8-	4.88 81	1.11-7-	87:0T
ø.83:8		3.18	3. Q3	1889.8	21 15.3	7.18-9-	8.22 22	I.02-7-	6.8 &S	7.44-3-	70:42
4.23:8	3.462	_	3.74 3.63	9259.8	22 58.3	9.9- 3-	7.7 42	Z:99-9-	21 60.2	4.81-4-	10:36
2.84:8	4.862	6.68		8259.8	7.23 42	8.14-8-	7.4 82	8.28-4-	23 42.5	2.23-2-	10:30
4.84:8	8. SØE	6.38	8.44	8189.8 8050.8	8.2 72 72 10	2.71-2-	7.81 82	8.6- 8-	I.64 32	1.82-1-	10:24
8.78:8	305.3	8.78	7.04		8. IE 62	9-52-9	8.64 QE	E. 74-1-	4.41 82	I.O O	8I:ØI
<b>₽.</b> [E:8	8.80£	ø.68	8.88	9059.0	8.72 SE	8.18 Q	33 52.4	8.32-0	31 6.8	I 26.3	71:01
Ø.42:8	8. &IE	ø. øe	8.28	9626.0		2.88 I	3.04 TE	ø. 83 å	34 32 .6	9.23.2	9 : ØI
1.31:9	312.9	7.0e	2.72	9826.0	8.8 8.8			2 16.3	1.01 95	2.91 4	ø :øī
2.4:8	9.3IE	ø.16	8.82	<b>&amp;</b> 726. <b>&amp;</b>	9.83 @4	7.81 E	Ø.23 S≯	Sarc	1 91 06	0 01 7	2 21
	~1.07.0		<b>L.</b> TT	7426.0	48 53.2	E.14 4	6.22.23	8.88.8	Ø.11 84	2.84 3	<b>†9:</b> 6
5:48.3	0.81E	7.0e	4.11	71.00 B	0 03 01	0 17 7	0 00 0-	• • • •			- · <b>-</b> -
9:18:9	3.228	8'68	ø.ø	Ø226.0	ø.a ea	9.41.8	2.83 63	8.84 €	<b>0.72 63</b>	8.14 8	LIMITS
J 60-3											
				-=	7.40 I TDMO	7 70017177	DOLL TONO	LATITUDE L	TOUGHIODE	LATITUDE L	TIME
YTISAJUNNA	WIDTH	Z∀	TJA	OITAR	ACLITIONO.	LATITUDE L	201 ITTONO	I BOUTTIA I	20 ITTORO	, _0,1_1,	NNIKEBSYL
DURATION	HTA9	NUS	NUS	DIAMETER	7NT7 1	CENTER	ITWT7 P	SOUTHERN	I TWT1	<b>ИО</b> ВТНЕВИ	
					⊒NT   €	ココエルコン	TIME	407UTI 102	A4114 1 1	1001120011	
										+	SAROS 144
⊃⊖2 S.QT	= T st	l a.Œ		oaa.	ור 22 סבר ב	R ECLIPSE C	ומחדאג פחדא	NΑ			
				יששב	. 030 00 3	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	, , 11111				

ANNULAR SOLAR ECLIPSE OF 7 FEB 2008

### CL 3I

2:12:3

8.II:S

8:699

8. Ø33

3.842

Ø.732

ø.ø

8.8

£196'Ø

**\$296.0** 

3:11:5 7.683 228'2 I.II 7£96.8 -65-14.3 148 1Ø.4 141 62.7 8.82-43-9.74 152 47.8 4:18 3:11:5 **258.4** 526'6 I.SI Ø\$96.8 4.7 94I Ø.32-83-143 24.Ø 7.84-33-2.88 531 4.14-83-91:1 4.11:2 2.713 2.192 9.21 Z#96'Ø 8.23 eAI 1.88-73-144 29.6 1.4- 73-164 11.3 0.84-78-4:14 4.11:2 9.909 4.292 T.EI 3.68-83-9.64-83-7796'Ø 3.82 Q3I 146 17.7 7.31-83-164 42.9 4:15 4.11:2 £.864 263.5 14.3 9496.0 9.44-63-146 62.6 9.42-69-15ø 56.2 1.8 331 2.23-63-ØI:+ A. II: S 6.984 4.482 8.41 7496.8 161 16.3 3.84-08-146 15.9 3.15-03-165 28.8 4.43-03-8:4 4.11:5 2.874 265.3 15.2 8496.8 161 29.2 8:19-19-0.7E-18-I.62 84I 166 43.6 1.83-18-9:1 4.II:S 2.074 1.882 9.31 9.43-29-6796'Ø 1.35 131 146 32.8 9.14-29-**JEE 63.0** 9.73-28-7 : 7 2:11:5 1.584 6.892 6.31 6496.8 6.88 131 6.83-88-146 27.Ø -63-4E.1 Ø.73 331 8.83-58-4: 5 3:11:5 426.8 3.732 1.91 Ø996'Ø 4.82 181 9.88-48-146 11.5 Ø.84-48-166 65.2 Ø. Ø 39-Ø : > 8:11:5 4.134 Ø.892 2.81 Ø996'Ø 6.8 ISI 8.0- 88-146 46.7 E. @3-39-4.74 331 E.1- 88-3:28 3.11:5 7.844 5.892 £.8I Ø996'Ø 8.54 Q31 3.2- 78-3.8 341 1.53-88-8.28 331 8.2- 78-3:58 7.11:2 442.8 9.892 16.2 Ø996'Ø 6.8 031 1.4-88-8.81 441 4.83-78-8.01 331 I.A- 88-3:24 8:11:2 8.654 8.892 16.2 6496.0 1.62 641 8.3- 68-6.41 E41 0.43-83-£.04 431 8.3- 68-3:25 8:II:S 437.6 3.882 Ø. 9I 6496.8 4.42 841 0.7- 0T-6.63 £31 T.T- QT-8.48 IAI 0.48-68-3:2Q Ø:21:2 436.3 1.892 8.31 8496.8 8. 01 TAI S.8- IT-8.4I @4I 0.83-0Y-6.7 EBI 7.6- IT-3:48 1.21:2 436.9 4.782 3.31 7486.8 8.88 341 8.6- 27-8.11 881 8.03-17-0.2 251 0.21-27-3:48 2:12:2 4.884 8.882 1.31 9196.0 4.44 E41 I.9- E7-136 40.8 4.84-27-0.65 031 2.41-ET-3:44 2:12.3 @.8E4 8.492 3:42 T. PI 9796'Ø 1.82 141 2.8- 47-3.38 281 4.68-87-0.33 841 4.81-47-2:12.4 7.044 7.292 14.2 £496.0 8.72 881 8.8- 37-3.84 128 48.6 75-18.2 146 44.5 ØÞ: E 3:21:2 9.444 Ø. Ø92 13.5 I+96'Ø 88:5 2.03 481 8.0- 87-7.01 421 4.11-87-I.0 AAI 0.9I-8Y-7.21:2 Ø.034 256.3 8.21 6£96.8 7.61 &EI 7. &3-87-3.18 811 1.34-37-3:38 14Ø 28.4 1.81-77-8:21:2 1.734 521.8 6.II 8.84 421 3.48-77-7£86.0 7.4- 8Y-E. \$1-87-I'Øb III 136 8,3 3:34 8:13.8 466.3 245.5 8. QI ₽£96. Ø 2.03 TII 6.T- 8T-1.32 £01 8.0- 87-8.18 &EI E.3- 67-3:32 2:13.2 4.874 Ø.882 9.6 Ø£96.8 9.62 9&1 2.32-8Y-8.82 88 2.11-37-123 25.Ø I.84-67-9::8 2:13.9 2:899 T. T&S 0.0 6096'Ø 6.48 87 6.23-47-8.73 **0**8 5.84-IT-84 27.5 I.54-EY-STIMIL **YTIAAJUNNA** MIDTH ZΥ TJA RATIO LATITUDE LONGITUDE LATITUDE LONGITUDE LATITUDE LONGITUDE TIME **NOITARUQ HTA9** NOS NNS DIAMETER **ONINERSAL** CENTER LINE SOUTHERN LIMIT NORTHERN LIMIT Delta T = 71.3 Sec SAROS 121

4.41 881 9.44-84-

E.83 841 I.0- 48-

6.78 SEI 7.0- 03-

9'88 68I Ø'Z9-Z9-

8.74-84-

Z. E3 I3I 3.72-43-

**STIMIL** 

ØZ:+

9

LIMITS

11:10

11:15

11:8

11: 4

0:11

10:28

79:0T

87:0T

70:44

04:0I

1Q:36

10:35

1Q:28

78:S4

1Q:50

91:Ø1

IQ:IS

8 :ØI

7 : ØT

Ø : ØI

99:6

3:25

87:6

bb:6

Ø7:6

9:38

35:6

82:6

**₽Z:6** 

LIMITS

TIME

NUIVERSAL

SAROS 128

1.36-411- 0.81 48

3.11-3@1- 8.41 8E

8.0- 001- 8.91 IA

7.18-89- 2.64 EA

6.84-86- 4.8 84

2.7- 48- 8.84 33

Z.&E-28- 1.88 73

8.01-49- E.T AT

8.1.5 -55-32.8

8.44 IQI T.E4 QT

2.31 301 1.84 89

LATITUDE LONGITUDE

NORTHERN LIMIT

T.8

I.8 @3

3.5 23

23 28°I

8.42 63

1.21 IS

2.64 48

4.88 33

3.82 89

8.61 **Ø**7

7.21 27

7.E 8T

7.83 eY

6.43 18

E. 7E E8

7.04 48

6.91 48

7.81 28

7.8E 8T

84

E. 72-19-

I.42-68-

8.18-78-

1.74-38-

5.43-08-

8.71-67-

P.88-77-

7.43-37-

0.4- AT-

4.E- 27-

9.84-69-

Ø. +1-78-

9.42-09-

1.64-84-

5.64-85-

8.88-22-

3 E1.0

Q. IE TE

6.68 49

Q.7 E8

8.81-811- 4.84 SE

1.42-66- 7.33 8£

8.42-3e- 7.08 IA

8.22-29- E.84 EA

6.03-68- 2.13 34

E.85-78- E.64 TA

£.85-38- 8.24 64

8.84-68- Q.88 13

I.1- 28- 7.02 83

9.81-08- 7.8 33

5.85-87- 3.13 83

3.73-87- 3.38 83

8.82-67- 4.2 28

8.78-17- 9.34 EB

4.82-78- S.41 T8

3.8- 38- £.63 88

7.41-28- 4.34 QT

8.63-83- 8.28 27

8.3- 33- 6.61 47

2.33 @@I I.84 78

LATITUDE LONGITUDE

SOUTHERN LIMIT

0.6I 08

7.62 39

9.7 8T

4.43 TT

E. TE 9T

E. QI 18

7. 02 28

8.34 28

0.0 Z8

3.03 67

7.83 37

Ø.31-37-

Z.7E-69-

9.41-03-

4.73-54-

2.72-38-

₽.72-E2-

6.81-8-

16 36.3

9.18 IA

8.21 59

0.02 I8

## Table 44

8.8- EII- Q.EA EE

3.8- 201- 1.04 8E

£.62-78- £.83 64

2.28-88- 3.41 73

8.83-87- T.@ 93

4.14-23- T.A TT

8.6- 84- 8.83 87

4.0 201 2.64 88

LATITUDE LONGITUDE

CENTER LINE

0.88-79-

2.42-46-

9.84-16-

8.08-68-

3.78-38-

2.23-68-

1.11-28-

7.51-77-

7.0E-3T-

9.24-67-

8.84-17-

+·Ø+-69-

£.61-79-

7.7E-48-

£.72-13-

3.35-73-

8.83-88-

-23-10.5

7.8I-Z-

7.62 32

5.08.23

73 12.2

I. \$E 06

E. 72 IA

43 49.2

4.83 34

0.03 TA

0.64 I3

2.68 83

4.72 33

3.84 Q8

2.28 28

2.81 49

8.4 88

6.13 78

I.04 69

3.62 IT

Z. 02 ET

0.21 37

4.34 Q8

7.22 28

1.18 88

3.88 88

4.8I 28

£.82 97

Z. 3I 17

1.0294

T.88.I

I+EQ.I

1.0352

1.836Ø

1980.I

EYEQ. I

TTEQ. I

1.038Z

1.0385

1.8388

0680.I

1.0392

£650.1

1.8394

1.0394

\$680.I

\$680.I

£620'I

1680.1

6880.I

98£0.1

£850.1

EYEB. I

1.0374

1.0368

1980.1

1.0352

1,83.1

IZEØ'I

IQEQ'I

DITAR

DIAMETER

0.0

E.II

Ø.9I

76T

2.22

3.42

4.92

Ø.82

4.62

9.08

31.5

8.28

6.28

8.58

33.5

33.5

4.88

ø.εε

32.5

9.IE

a.re

6.62

9.82

I.72

25.3

I.ES

9. QZ

17.5

13.5

I.T

ø.ø

TJA

NUS

291.3

Ø.482

Ø. Ø82

9.972

£. £72

I. ØYS

6.992

9,592

2.092

6.932

223.4

6.642

2,842

4.242

238.5

4.482

Z. أZ

9.322

8.022

512°4

9.602

3.202

0.46I

182.9

2.731

3,441

116.2

8.38

8.49

9.94

35.3

ZΥ

NNS

Z.IØZ

1.282

242.3

7.742

7.09Z

521'4

221.3

9.092

2.642

9.742

8.345

243.9

Q.242

0.04S

238.2

236.3

234.6

8.8EZ

231.4

576.9

8.822

5.722

1.922

Ø:92Z

8.42S

522.9

7.122

220.3

2.812

213.6

₽.9ØZ

**MIDTH** 

HTA9

1:28.8

1:42.5

1:63.6

9:69:I

3.4:5

7.8 :2

4.21:2

9:31:2

5:18.3

8. QZ: Z

3.22:2

2.42:2

2:22:2

4.82:2

Q. 72: 2

2.72:2

1.72:2

7.82:2

9.32:2

8.42:2

5.52:2

5.13:2

Ø:81:2

2:31:2

6.21:2

1.9:2

3.4.5

1:68.9

6:19:I

2.14:1

8:08:I

YTIJATOT

DURATION

TOTAL SOLAR ECLIPSE OF 1 AUG 2008

Delta T = 71.7 Sec

5.81-821-8.7 3

LIMITS

2 15.7 -124-51.3

Table 45

### ANNULAR SOLAR ECLIPSE OF 26 JAN 2009

87:6 8.81-601- 4.63-0 2:69:9 8.8- SII- 0.SI-I-4.46-311- Q.12-1-7.038 1.132 9.EI 1816.0 4.22-801- 0.22-4-24:6 4.81:8 344.2 521.9 9.22 ZØ26'Ø 8.42-301- 8.43-4-7.85-701- 7.82-8-98:6 2.42:9 1.8- IQI- 2.44-Y-7.33-201- 9.02-8-0.02-66- I.T- T-**≱.8**££ Ø. £32 Ø.62 7126.8 1.82-69- 8.64-01-Ø8:6 Z.@I-86- 7.@E-6-9:88:9 7.34-79- E.QI-QI-8.255 2.432 34.2 8226'Ø 3.16-69- 8.04-II-9.28-39- I.8- EI-72:6 Ø.54:8 1.0- 36- 6.IZ-ZI-A. 72E 6,332 8.88 7829. Ø 0.I4-EI-81:6 Ø'9- 91-8.51-19-7.64:8 1.228 8.732 6.24 9756.8 0.85-29- 4.52-41-Ø'9- \$6--91-53.7 6.8- TI-6.6- 68-7.66-31-3:12 @. 73:8 Ø. TIE 6.632 7.84 1926.8 7.0E-06- 2.71-81-7.81-78- 8.02-71-9:6 8.8 :7 312.2 262.3 £.03 **7926.** Ø 3.46-88- 8.4- 81-E.43-68-7.64-81-Ø :6 1.18-38- 9.1- 91-3.5- 88-E.EE-@Z-E. &I: 7 9. Y&E 1.392 9,59 Z9Z6'Ø 4.84-88- 4.74-61-9.21-22-I.13-68- 0.98-02-9:8 £:31:7 8.892 9.99 9926'0 I.4- 38-9.32-12-6.8I-88-8.EQE 1.31-28-2.21-22-8:48 Ø. Ø3-22-7.88-48-I.84-82-1:22:7 236.3 1.82-88-0.272 9'69 @Y26.@ 8.1- E8- 2.02-32-8:45 7.14-08-0.54-62-4.72:T 7.362 5.972 2.29 £729.8 8.03-18- 6.08-42-9'8- 9Z-98:8 £.71-08- 8.83-32-8.6- 6Y-4.2E:T 292.5 281.3 7.49 9729. Ø 1.82-18-2.64-82-Ø8:8 9:19-6/-E.81-82-8:8E-TT-6.18-82-0.78:T 9.682 2.782 ø. 79 8729. Ø 4.44-87- 4.E2-72-8.7- 87-3.23-72-8:24 8.81-87-8.88-82-I.IA:T **0.782** 1.462 Ø826. Ø 4.11-77- 3.34-82ø:69 4'0I-6Z-81:8 7.04-87-7.63-8£-3.35-47-6.44:T 6.482 302.I 8. ØT 1826.8 4.78-37- 8.4- 08-8:15 7.1- 47- 8.12-1E-0.8- 37- 0.81-28-8.I- EY-9'97-08-I.84:7 1.582 4.IIE 1.27 2826.0 3.52-27- T.35-25-7.22-87- 8.88-88-7.32-17-0.85-IE-8: 8 6.03:T 9,182 8.1ZE Q.EY £826.0 0.68-17- 1.74-48-1.84-68-8.74-28-Ø :8 2.24-07- E.74-EE-1:63:1 **⊅.**082 3.555 4.87 £826.0 1:24 I.A- 88- 6.48-68-2.13-63- 6.73-38-7.49:T 8.672 7.448 73.2 2826.8 8.73-83- 2.83-48-Z.7I-88- 2.93-48-84:7 2826.8 **▶.83-78-**6.3- TE-7.33:7 2.972 322.9 9.27 2.7- TA-E.S- 8E-£.32-49- 3.0- 8£-7:45 Ø.83:7 Ø. 672 4.17 Ø826.Ø 1.21-38- 8.8- 78-Ø. Ø 99-1.11-86-4.8 98:7 8.72-23- 8.83-85-9.33:7 6726.8 6.01-68-7.3- 8E-@.33-58-Z.EI-6E-2.672 12.8 6.69 7.52-09- 7.53-75-Ø8: L 7729. Ø 8.5- 13- 8.5- 98-9.24-13-1.21-04-3.43:7 9.672 2.42 ø.89 £.21-83- 1.34-8E-7:24 7:52.6 4729.8 7.84-83-Ø'99-68-7.12-63-3.7- IA-9.082 T.IE 8.39 2.13-83-6'89-17-8.23-33- T.28-68-81:7 4.88 0.03:Y 281.6 4,89 2728.8 -28-21.9 4.34-04-7:12 6.34-24-0.42-E3- 0.81-04-1.01-48-3.84:7 1.582 9.44 8.09 8926.8 1.74-63- 3.06-14-0.82-E4-8.44-03- 8.43-04-9:7 2.24:7 Ø'98Z 2.03 Ø.83 ₱926.® 1.1-13- 8.01-24-6'91-19-6.53-74- 6.72-14-Ø : L Ø. 78: 7 287.3 9.33 ø.33 Ø926.Ø 3.5-84- 7.34-54-0.01-84-4.4- 44-7.64-44- 2.33-IA-19:9 Q.IE:Y 3.74-44- 8.48-44-Ø:06Z L. Ø9 8:19 9976'Ø 8.64-44- S.41-E4-81:8 Z.08-I4-4.31-24-Z. Y- IA-9.99-44-Ø. 42: 7 293.3 7.39 4.84 6+26.0 I.02-I4--43-36.6 8.3- 75- 8.6- 34--37-52.8 3.72-24-8:45 1.81:7 297.3 T. &T 7.44 2428. @ 2.18-78-I.84-64-9'11-97-8.63-66-7.62-24-98:3 E. 7 : 7 9236. Ø 0.61-EE-E.03-E4-6.88-28-6.10E 7.37 8.04 9.61-24-Ø8:9 6.72-62-4.73:8 8.68-72-5.63-44-3. Y@E 6'Ø8 36.4 9226.8 ₱.78-82-2.98-84-6:24 -24-26.3 6.63-14-31.5 0.82-44-1.94:9 314.3 €.38 9126'Ø ₽.8I-EZ-7. QI-E+-8.83-12-I.A- IA-81:9 2.88:8 8.228 8.32 ZØ26.8 7.81-24-6.3- 31-9.72-EA--18-32.5 1.29 2.83-81-7.83-3-7.55-IA-Z.7- II- 8.85-95-8:15 4.71:8 334.3 6.86 9816'Ø 0.88-01-18.4 4.84-8-6.14 QI 2.6- 88-CIMITS 6.73-38-2.44:3 1.298 112.4 a.a Ø116.0 11 15.4 2.54-45-7.84 ZI LATITUDE LONGITUDE **TIME** MIDTH ZΥ TJA LATITUDE LONGITUDE LATITUDE LONGITUDE **ANNULARITY RATIO** NNIVERSAL DURATION HTA9 NNS NOS DIAMETER NORTHERN LIMIT SOUTHERN LIMIT CENTER LINE SAROS 131 Delta T = 72.1 Sec

0.48-821- 0.88 8

7.04:3

3.848

2,162

0.0

8+16.0

# 7able 46

TOTAL SOLAR ECLIPSE OF 22 JUL 2009

8.8 :8	7.402	7.0es	ø.ø	1.0608	167 42.Ø	-12-55.1	9.4 831 9.34-EI	- 0.31 TST T.8- 21-	LIMITS
			T . C T	0790.I	5.4 4\I	8.22-8-	8.11 371 3.33-3-	4.53 27I 9.I3-4-	ZI:Þ
3:22:1	9.822	9.862	1.61	9690.1	8.84-971-		9.84-87I- 3.02-2-	7.6 671 7.8- 1-	9:4
1.81:4	235.5	6.862	<b>8.72</b>	•			8.15-471- 3.15 Q	£ .82-871- 7.03 f	Ø : Þ
7.8E:₽	241.3	8.882	1.48	AITO.I	2.82-371-	a it i	9 15-471- 3 15 M	£ 80-871 7 83 t	<i>D</i> • <i>V</i>
6.23:4	245.5	8.882	9.68	6270.1	3.63-171-	4.24 &	7.4- 171- 4.0 E	8.33-271- 8.62 4	3:64
8.7:3	7.842	9.262	9.44	ZATO.I	8.1- 691-	8.73 3	E.8- 881- 9.EI 3	9.83-631- 8.04 8	3:48
3.82:3	1.132	7.162	2.64	1.0752	8.42-991-		7 16.2 -165-32.2	4.81-731- 0.34 8	3:42
3.28:3	8.832 1.130	9.062	4.63	1970.1	-164 -2.Ø		4.01-E91- 3.9 9	1.43-481- 2.24 QI	3:36
			4.73	6970.1	8.64-131-		18 66.4 -168-68.9	4.14-281- 1.18 21	Ø8:8
6:43.6	254.5	8.682		8770.I	8.44-631-		7.43-831- 1.88-21	14 13.6 -160-35.4	3:24
6:53.6	222.6	7.782	£.13		8.44-731-	ara et	8.2 -156-56.0	16 50.5 -158-34.6	3:18
7.2 :8	2.632	285.8	ø:39	1870.1			9.8- 331- 2.88 31	17 22.4 -156-37.4	3:15
6. \( \text{1.9} \)	2.732	4.882	8.89	8870.I	7.84-331-			5.74-45I- 7.94 8I	3:6
1.81:9	8.732	4.082	Ø.ST	0670.1	-163-64.8		2.8- 153 -7.2 71	• • • • • • • •	ø : E
4.42:8	1.832	4.872	4.87	£670.1	1.2- 231-	6.71 et	8.81-151-8.22 81	2.84-231- 7.21 02	3.0
9.62:9	<b>⊅.83</b> 2	9.07Z	9.87	9670.1	9.6- Ø31-	28 35.3	7.32-641- 8.8E 91	21 31.6 -160-64.0	5:54
7.88:8	2.832	2.132	9.18	7670.1	1.81-841-		1.48-741- 8.03 02	9.83-841- 4.84 22	84:2
	3.832	4.54S	2.48	997å. <u>r</u>	-146-21.3		1.14-341- 0.93 IS	1.2- 741- 2.73 82	24:2
8.36:8		4.70S	9.38	9978.I	1.42-24.1		8.84-E41- 2.8 E2	7.2- 341- 1.4 32	2:38
7.88:8	2.832			9970.1	8.2-241-		24 3.4 -141-48.1	I.0- E+I- 9.8 32	Ø8:2
3.98:8	2.832	164.5	7.48	8670.1	8.61-041-	7.2 82	7.84-921- 7.93 42	27 5.6 -140-53.3	2:24
1.98:3	9.732	9.041	82.3		2.11-881-		8.14-751- 8.13 32 5.81-951- 5.93 AG	7.14-851- 0.0 82	81:2
4.7E:8	4.732	128.3	£. 67	7670.I				28 49.8 -136-24.5	21:2
4.48:8	T.832	6.02I	2.87	4670.I	£.73-3£1-		2.08-351- 8.68 82.2	8.8- 451- 8.46 92	2: 8
Z.&E:8	8.332	3.311	8.27	1670.1	8.78-88I-		8.EI-EEI- 9.22 72		ø : Z
8.42:8	7.43S	8.111	<b>7</b> .69	8870.1	1.01-161-	6 Z 66	2.03-021- 8.1 82	7.62-181- 8.41 QE	w · o
7.71:8	₽.832	7.701	6.39	£870.1	7.4E-82I-	29 41 6	9.81-821- 4.48 82	8.03-821- T.84 0E	1:24
6.6:8	8.132	4.40I	2.29	8770.1	0.03-321-		8.85-321- T.I eS	3.0- 321- 3.31 18	8 <b>∀:</b> I
	0.052	S.IQI	58.4	2770.1	-122-54.2	a.ae ae	8.74-221- 8.22 92	8.63-521- 3.78 18	1:45
6:69:9		2.86	4.43	4870.1	7.34-911-	8.84 WE	1.44-911- 2.88 92	8.34-611- 4.03 18	1:38
Ø.64:3	0.84S		2.03	9370.1	8.12-811-		8.41.4 -116-25.6	31 54.2 -116-15.9	J:30
9:36:9	245.6	1.36		8470.1 8370 :	3.86-211-		4.84-SII- 8.88 9S	3.82-211- 1.74 18	1:24
8.22:3	242.9	ø.26	8.34	•	8.08-801-		2.74-801- 4.91 92	31 26-4-108-12-9	81:1
₽.7 :3	7.682	8.88	6. Ø4	1.8734				3.04 - 1.83 - 22.9	ZI:I
1.63:4	Ø.882	85.5	35.5	0270.I	8.64-EQI-		2.61-401- 1.64-82	29 44.5 -97-41.3	9:1
4.38.4	4.162	8.18	8.62	EQTQ.I	3.71-86-		0.03-86- 0.03 T2		Ø:ī
8.8 :4	2.325	8. <i>TT</i>	8.1S	0890.1	0.51-19-	1.7 72	4.83-19- 3.3I 8S	7.22-09- 2.73 72	<i>b</i> · ι
1.18:8	Ø.ÞIS	8.17	6.8	6880.I	8.31-67-	23 28.1	22 56.4 -8Ø-45.6	4.82-77- 0.23 ES	\$9:Ø
		• . –						010 01 0101 17	STIMIL
<b>4.</b> 6 :€	2,305	4.89	ø.ø	Ø190.1	₱.8E-@T-	20 22.4	7.63-07- 8.08 el	3.8- \( \text{0.5} \)	2TTUT !
11774101	HTGIW	Z∀	TJA	OITAR	TOMETIONE	<b>EATITUDE</b>	ATITUDE LONGITUDE	LATITUDE LONGITUDE L	TIME
YTIJATOT		NOS		DIVMETER	_ 4 1220110 1	'			ONIVERSAL
NOITARUG	HTA9	INI 12	14113	11114	R LINE	СЕИТЕ	SOUTHERN LIMIT	NORTHERN LIMIT	
72.5 Sec	= T stl	eq			700 77 10	70 17707 ***	7700 77101		SAR05 136
				6007	0E 00 'IIII	AR ECLIPSE	INS IATOT		

ANNULAR SOLAR ECLIPSE OF 15 JAN 2010

Table 47

1.51:7 7.17E Q. 243.Ø 0.0 3.62-221- 6.31 38 3.83-02I- 9.85 8E SITWIT 6906'0 8.83-021- 0.0E 8E 8.62:7 6,188 8.882 6.T 1706.0 38 52.1 - 112-37.9 36 20.5 -116-12.6 **79:8** 8.88-8II- 9.II 88 2.0:8 I. 71-801- 0.08 62 8+:8 348.1 232.4 Z.9I 8.62-E&I- 8.24 TS 26 2.6 -1Ø3-51.4 4016.0 8:02:8 0.31-76- 0.33 32 8:45 8. Q+E 6.822 Ø.82 Ø216.0 3.81-86- 7.02 AS £.23-89- 7.03 22 7.13-66- 6.7 ES £.8E:8 7.388 2.922 4.IE Z£16.0 6.08-46-Z. Q4 IZ 9'71-96-7.31 02 8:38 1.43:8 9.IEE 7.522 0.8I-2e-8.2 81 I.84-06-8.84 QZ 8:30 Ø. 9E I+16.0 1.18-19-Z. EZ eI 8:8:6 6.8ZE 6.41-88-6.24 8I 42:8 E.IZZ 0.04 6716'Ø I.Q- 68- I.SS TI 7.84-68-7.E 3I 9:22:6 7.828 6.812 £.8E-78-E.S- 88-8.13 81 81:8 7.54 9916'0 7.84-88- 9.28 3I 14 16.2 9:38:6 325.Ø P.9IZ 3.4- 48- 8.01 3I 8:15 Ø. TA 2916.0 3.13-48- 0.53 EI 7.65-38- 3.75 SI Ø.84:9 9.525 8.71-28- 8.7E EI 9:8 7.512 1.03 8916.0 Z.3- 88- 9.02 ZI 4.83-83- Z.8 II 8.68-88- 3.11 SI 7:63:6 3.525 8.0IZ Ø :8 6.23 2719. Ø 10 65.4 -81-26.8 8.4I-Z8- I.IA 6 8.11-08- 4.12 8 1:64 T. &I: &I 9.52E 9.702 9.33 9719. Q 7.43-67- 8.38 6 4.7- 67- 3.13 QI 0.12:01 3.838 6.E@S 6.73 6716. ® 4.72-8Y-6. \Q 8 6.41-6Y-7.8 T 4.84-TT- 6.88 6 84:7 9.08:0I 8.525 6'66I 8.03-TT-2.71-87- 2.72 8 7:42 ø. ø9 7.E- TT-6.01 T 3.83 3 Z816.0 4.68:@I 7.428 195.3 8.83-47- 0.22 T 98:7 6.Ia 9816'Ø -76-42.9 6.3 8 5.62-87-4.03 A Z. 74: QI 8.88-87- @.12 8 Ø8:7 9.92E Z.06I 63.5 7816.8 9.52-47-7.5 3 7.6- 37-3.8≯ € 1.43:01 9.72E 7.4a 7.12-27- 0.42 3 7:24 184.5 8816. Ø E.8- ET-6'9 7 E.13-ET-8.64 S 8.8- IT- 8.88 A 81:7 Ø.09:01 £.62£ 4.87I 7.39 6816.0 4.64-17-6.II E 3.55-27-7.43 I T.A :II 331.3 6'I/I 2.99 7.31-17-Z.E I 7.64-69-8. IA 8 7:12 Ø616'Ø -78-32.5 4.IS S 9:1 1.8 :11 8.888 4.89 7.73-69-Z.3I Ø 3.55-83-4.33 S 165.2 Ø616'Ø £.3I-69-4.48 I 11:10.2 332.4 128'2 2.89 Ø616'Ø 2.73-78- 0.13 0 1.85-89-4.62-8 4.8I-78-I. 5I Z Ø : L 49:9 e.ar:tr **₽.7**EE 1.231 9.39 E. 7I-78-8.01-1-1.84-38 -65-58.1 Ø616'Ø 8.7E-88- @.II @ 0.01:II 6.75-48- 1.68 @ 84:8 8.688 9.49 9.43-39-Z.84-I-1.841 6816'Ø 2.81-38- 4.82-@ 8:45 8.7 :II 9. I48 T. QPI 5.59 7819. @ 8-58.2 -63-52.3 I.62-48-E.22-2-4.31-68- 8.72 @ 8.E : II 342.4 7,19 8.64-18- I.Q- Q 85:3 136.9 -62-25.3 2.72-1-7.0- E8-7.23-2-3816. Ø 7.02-09- 6.52-0 Ø8:9 6:73:0I 3.545 T.IEI 8.63 9.82-19-1.91-5-£816.@ 7.43-09-E.S3-I-7Z:9 9.03:01 344.4 2.74-83-9.54-0 Ø.8ZI 9.73 1816.8 7.61-63-E.EI-Z-6'19-69-4.14-8-T. IA: QI 346.0 156.Ø 2.33 7716. Q ₱.6E-73-8.62-2-6.6- 83-2.63-6-₱.8- T3-9.83-Q 81:9 Z.IE:QI 346.4 9.12-99-2.21-4-8.82-33- 9.8- I-21:9 122.4 9.23 4719. @ 8.23-33-**4.14-2-**1.91:01 6.61-4-9.0E-E3-8.51-1-9:9 345.6 120.2 7.64 7.74-2-8.32-43-6916'Ø 8.83-53-Z.8Z-I3- 8.ZI-I-Ø :9 10: 6.4 345.7 **4.8II** 9.02-23-8.12-4-9.34 **≯916'**Ø Ø:39-19-0.84-2-0.41-64- E.A- I-19:9 2.03:6 342.9 Ø. TII 43.2 8916'Ø 8.65-64- 2.14-2-Ø. 4- Ø3-E.8I-4-3.55:6 346.3 115.8 39.68 1916'Ø 8.6- TA- I.82-2-8.28-74-6.2- 4-4.44-84-4.74-Q 87:9 5:31:6 27:9 1.748 5.24-44-2.68-8-2.43-54.2 7.9I-8 8.411 35.4 £416.8 3.91-44- 3.0- 2-Ø:33:8 348.4 Q. PII 8. أ \$216.0 Z.I- IA- 0.IZ-I--41-54.5 Z.Z- E-8.48-04- 7.22 Q 98:3 8:32.5 8.82-86- 0.72 I Ø8:3 35ø.8 25.3 6.42-78-6.3- Z-113.4 2216.0 3.83-85- 0.12-0 8:5:8 3.44-0E- 7.21 E 2:24 355.Ø 8.211 £.8I 9Ø16'Ø 3.16-16- 8.31 f 8.8- 28- 2.88-@ E.II:7 a.are P'III ø.ø £9Ø6'Ø 4.22-81- 8.24 8 6.41-31- 8.12 3 8.8- 81- 0.78 8 STIMIL **YTISAJUNNA MIDTH** ZΥ TJA LATITUDE LONGITUDE LATITUDE LONGITUDE LATITUDE LONGITUDE TIME RATIO NIVERSAL DURATION HTA9 NOS NNS DIAMETER SOUTHERN LIMIT NORTHERN LIMIT SAROS 141 Delta T = 72.9 Sec

TOTAL SOLAR ECLIPSE OF 11 JUL 2010

8.84:2	183.4	8.808	ø.ø	1.0452	71 41.4	6.0E-03-	0.88 IT	6.86-13-	8.81 <b>0</b> 7	Ø.6- Ø3-	STIMIJ
1.9 :8	2.191	3.418	<b>7</b> .6	6740.1	9.88 I8	1.12-24-	₱.8 eT	4.03-74-	83 12.6	8.02-E4-	20:48
	2.861	3.026	4.91	1050.1	7.24 88	8. T- IA-	3.83 T8	1.34-24-	8.31 68	1.76-66-	50:44
4.62:8			2.12	9190.1	£.4 £6	1.81-86-	85 45.2	0.84-98-	6.71 E6	2.73-88-	84:82
3.44.8	203.5	3.428	Ø. 32	1.0526	Z.EZ 86	à. €- 8€-	9.91 96	8.12-78-	9.92 96	2.74-48-	98:0Z
3:56.3	7.80S	8.728		1.0535	2.7 66	8.8- 4£-	6.7 66	7.82-38-	Ø. 4 66	-35-22.8	Z8:9Z
Ø. T : 4	212.3	7.0EE	2.82			-32-28-3	4.48 IQI	0.14-EE-	8.02 IQI		8Z:ØZ
7.81:4	2.812	333.5	6.0E	1.0543			1.64 £01	7.6- 28-	9.22 £&1	8.64-62-	20:24
4:25.5	8.822	2.888	4.88	6430.I	• • • • • • • • • • • • • • • • • • • •	8.83-06-	1.05 40.1	4.74-0E-	0.41 301		ØZ:ØZ
4:33.5	7.822	6.888	35.6	1.0555		7.78-62-		4.28-82- A 7A-86-	7.83 801		20:16
8.04:4	4.722	3,148	3.78	1.0560	107 12.4	9.52-82-	a. 72 Tai		9.28 801 7 93 901		ZQ:12
4.74:4	6.0EZ	8.448	8,68	1.0564		4.21-72-	9.8 ear	-28-23.5			8 : ØZ
4:53.5	4.462	1.748	6. 04	1.0568		-26-12.5	110 40.3	1.02-72-	8.8 QII		7 9: 4
6.83:4	8.782	6.648	2.24	1730.1		1.41-32-		-26-21.4	9.0E III		Ø : ØZ
7.8 :3	1.142	8.238	43.5	1.0573	7.41 EII	6.9 <u>1</u> -≱2-	8.48 811	0.72-32-	112 54.1	0.41-62-	Ø . ØC
ø.8 :3	244.3	3.83.7	9.44	9730.I	114 36.3	3.62-82-	114 67.3	4.86-42-	0.31 411		18:28
9.11:3	5.742	7.835	46.4	1730.1	112 22'8	T.SA-SS-	8.71 811	-23-48.6	8.88 311		79:67
5:14.6	2.032	8.1	I.84	6730.1	T.EI TII	2.63-12-	1.88 TII	0.8- ES-	116 51.2		87:61
0.71:3	262.9	8.4	9.94	1.058Ø	3.0E 8II	8.81-12-	118 53.4	-22-25.6	4.7 8II		19:44
7.81:3	255.4	ø.8	6.84	1.058Ø	119 46.5	-20-41.5	12Ø 9.9	4.84-12-	1.52 911		ØÞ:61
8.91:3	3.732	ĭ·ĭı	1.74	1.058Ø		I.7- 02-	121 26.1	-SI-14°1	120 38.4		98:61
2.02:3	2.692	2.41	2. <u>7</u> 4	0830.1	122 18.Ø	7.36-91-	122 42.2	8. <b>2</b> 4-@2-	121 63.9		19:32
8.82:3 5.82:3	7.032	8.71	Ø. 74	7.058Ø		0.7- e1-	123 58.8	£.41-@2-	8.8 521		19:28
1.91:3	7.132 7.832	4.02 6.51	7.84	6730.1		E.14-81-	125 16.1	8.84-61-	124 26.4		19:24
3.71:3	1.282	23.4	2.84	8730.1	Z'6 9ZI	5.81-81-	126 34.6	8.32-61-	125 44.3		19:20
8.31:3 3 71:3	0.282	4.82	9.64	9730.1	8.82 721	E.83-71-	127 54.6	Ø.8- 91-	8.E 721		91:61
5:12.3	4. I 3 S	2.62	8.44	4730.1	9'09 821	5.14-71-	9.91 621	1.84-81-	128 25.Ø	2.46-31-	ZI:6I
	1.092	8.2E	8.64	1730.1		4.72-71-	130 41.2	<b>▶.3</b> 6-81-	7.84 est	1.0S-31-	8:61
9.8 :3	258.3	7.48	9.24	1.0568		7.81-71-	132 8.8	9.42-81-	131 15.3	£.6- 81-	7 : 6T
£.4:3	255.8	2.78	£.14	1.0565	133 12.3	3.6- TI-	133 4Ø.2	6.71-81-	132 45.5	6.1- 81-	ø :61
2.63:4	8 336	0 L6	2 17	1010 -	•					7:00-07	<b>78:2</b> 9
4:53.3	8.232	7.68	8.68	1.0561		1.8- 71-	135 16.1	8.41-81-	6.61 461		18:52
8.34:4	2.642	Ø. 24	1.88	1.0557	7.72 aei	7.8- TI-	136 67.5	3.31-81-	738 89.4		18:48
4.98:4	245.0	6.44	2.98	1.0552		<b>6.11-71-</b>	138 45.7	1.12-81-	1.34 751		\$7.8I
£.1£:4	240.3	4.84	1.48	1.0546		5.22-71-	140 45.4	0.28-81-	9.88 681		
4:22.3	8.35.g	48.5	8.18	1.ø539	7.41 241	6.86-TI-	145 49.9	1.64-81-	7.14 141		78:40
4.12.4	2.922	9.03	1.62	1.0532		9.S- 8I-	7.11 341	1.41-91-	£.73 EP.1		18:36
5.1 :4	8.222	9.23	1.92	1.0523	7.9 TAI	₽.8E-8I-	147 53.2	2,64-61-	8.62 841	17-25.1	18:32
3.84:8	7.312	7.43	22.5	1.0512	160 12.9	Z.EZ-61-	161 4.1	-20-38.5	4.82 641		18:28
2.48:8	3. <u>7</u> 82	9.83	2.81	6640'I	7.63 E31	4.0E-0Z-	1.8 831	ø.13-12-	163 1.4		18:24
3:15.5	£.791	9.63	12.2	0840.I	4.8I eai	8.81-22-	6.8 191	-23-55.6	0.13 Tal	1.03-02-	18:2Ø
				055017	LIGT OUT	7.16-07-	0.84 0TI	1.24-72-	9.8 171	<b>4.4-</b> 82-	LIMITS
0.44:S	1.081	7.48	ø.a	1.0443	A OF NT!	2.78-82-	א אין אין אין	r GV-ZO-	<i>3</i> 0 121	. , , 50	O,12112 1
YTIJATOT	МІВТН	z∀	ΤJA	OITAR	-ONGITUDE	LATITUDE	AUTIONO.	1 30UTITAJ	DUGITUDE	LATITUDE L	TIME
VOITARUQ	HTA9	์ กักร	ÑŃŚ	DIAMETER			ITWT7 A	SOUTHERN	ITWTT	ИОВТНЕВИ	UNIVERSAL
					3 FINE	コエルヨン	TIMIII	AGDUTI INS	TIMI		
73.4 Sec	= T st	le(I								•	SAROS 146

Ø.22:4

322.3

Z94'I

0.0

**₽186.**Ø

ANNULAR SOLAR ECLIPSE OF 20 MAY 2012 Table 49

2.14:4 Ø'86Z 2.282 p.TI 1.71 811 4.EI 04 38: T 9986. Ø 6.7E 9II 7.83 68 122 29.6 7.1E 6E 9.03:4 7.882 6.372 124 29.1 43 8.5 1:24 4.42 2759.8 126 54.3 4. IE S4 1.3 621 41 21.6 4:83:4 8.772 I.QYS 7.62 0.85 ØET 7.8 34 81:I **≯8£6.**Ø 8.78 SEI 7.22 44 134 26.6 43 35.3 5:3:3 A. QYS 264.5 138 84.2 7.04 84 1:15 34.2 \$686. Ø 137 35.2 1.64 84 E.8 9EI Ø. 73 AA 8:11:8 48 58.3 1.492 6.832 1.85 2016.0 142 4.6 143 25.Ø 8.2 84 3.75 @AI 8.83 74 9:1 5:17:3 7.832 2.532 9.Ib 46 56.1 147 24.3 8'69 PFI 48 52.4 ø : t 6016.0 9.4I 84I I.43 74 5:22.4 254.1 4.742 \$9:Ø 7.44 9146'Ø £.11 031 7.88 84 7.01 Id1 8.88 TA 2.7 941 2.98 94 8.72:3 1.092 5.I4S 9.74 0.74 431 E.21 84 1.8 881 9.81 08 87:Ø Ø246.0 1.73 631 8.51 64 5:31.2 7.842 Ø.382 8.64 831 8.84 88 2.03 4246.0 157 34.2 E. 04 64 Z.3I 83I 7.7E 8A 27:0 6:34.9 243.9 4.822 9.29 8246.0 1.4 191 Ø'69 67 161 36.4 48 65.7 6.82 031 2.8 18 98:Ø Ø.88:3 9.I4Z **₽.** I22 8.48 1848.8 164 27.6 7.8 64 51 15.3 164 1.3 08:0 9'ØI Ø9 164 51.6 7.04:3 7.682 2.412 4.83 7.72 Tar 4.02 Ia \$2:Ø 8549. @ 167 45.3 4.31 Q3 p.I 89T 4. II 94 6:45.9 238.3 9.902 81:Ø 6.73 9849.8 8.78 **0**71 6.EI @3 2.8 ILI 6.6 64 4.84 QTI 9.81 I3 3.44:3 237.3 9.8er 1.63 7549. @ 174 6.4 9.9 03 4.8 714 7.2 64 0.4 471 E.11 13 ZI:Ø 7.34:3 7.882 7.06I ø. ø9 771 6.64 84 8. P.I TTI T. T3 03 9 : Ø 8846.8 3.8 771 8.83 94 5.2 5:46.3 8.882 182.Ø 9. Ø9 2.43 971 9.18 84 3.65-671- 3.85 @3 ø :ø 6546.Q 6.23-671- 7.48 64 4.84:3 8.882 173.5 6.09 6849. Ø 2.83-871- 8.01 64 7.71-771- 7.8 84 0.8E-87I- 8.EI @3 53:24 0.84:3 4. YES Ø:99I 8.84-ETI- 8.84 64 8.09 6546.Q 4. T- 4TI- 8. I4 84 9.28-471- 8.04 TA 23:48 5:45.1 4.09 238.4 156.7 8£46.0 9.91-171- 8.7 84 E.13-171- 8.7 74 6.84-071- 8.8 64 23:42 7.54:3 23:38 8.682 3.8 L 9.69 7549. Q 4.35-831- 6.82 TA £.21-631- 8.62 84 3.83-781- 8.82 84 6:17:9 9.142 6.04I 9.89 9849. Ø 46 45.2 -165-53.3 8.35-881- 8.74 34 9.8- 331- 8.84 TA 23:3® 9.68:3 8.542 3.551 1.73 3.0- 481- I.0 34 4.62-231- 8.63 84 23:24 ££46.@ 45 56.6 -163-13.2 8:36:8 4.842 126.8 9.39 £.65-631- 6.83 34 23:18 1546.0 2.45-031- 2.8 34.2 44 8.8 -161-26.5 7.88:3 248.6 23:12 120.5 9.83 7.33-831- 6.83 AA 8246.8 8.83-T3I- 8.4 77 43 11.1 -158-52.6 E:30:1 \$23.8 3.411 51.3 4248. Ø 2.81-331- 1.1 43 Ø.81-831- I.9 SA 43 63.6 -164-11.3 23: 6 1:92:9 Ø. 732 Ø.egI 6'87 Ø246.0 41 62.Ø -152-34.8 4.14-631- 8.1 IA 8.42-131- 7.24 SA 23: Ø 8:12:9 9.192 6.EQI 1.94 9176'Ø 7.64-641- 8.85 Q4 4.1- Id1- 8.84 98 41 25.6 -148-34.4 55:24 Ø:11:9 8,882 1.66 1.54 Ø146.0 8.83-841- 0.31 98 8.81-841- 3.82 88 7.75-341- 3.1 @4 22:48 6:11:3 2.272 9.46 2.16-241- 3.62 88 22:42 8.68 £016.0 37 1.3 -145-22:1 37 45.4 -143-58.9 5: 6.3 4.872 6.6- 6EI- 8.74 8E 22:38 **7.06** 1.88 9656. Ø 7.34-041- 3.8 35 25.1 -142-16.2 2. Ø : 3 282.3 5.38 6.IE 7856. à 2.21-781- 7.31 A8 2.23-861- 8.78 88 34 62.8 -135-25.8 22:38 4:53:4 Ø. £62 82.3 Ø. TS 8789. ® 8.8- 881- 1.8 SE 31 35.2 -134-59.6 8.E- IEI- 4.9E SE 22:24 9:97:7 7. IØE 2.87 7.72-321- 8.83 92 22:18 Ø.IS 1986'Ø 2.0- 821- 4.88 e2 2.71-081- 0.9 es 8.33-311- 1.38 3S 2.38:4 312.6 4.87 22.3 Ø486.0 £. £5-021- 8.88 32 0.34-521- 9.33 32 22:12 £.23:4 8,828 8,89 ø.ø IIE6.0 7.82-801- 7.22 IS 7.04-60I- 0.33 6I 2. 22.3 L1Ø1- 8.22 SS STIMIL **YTISAJUNNA** MIDTH ZΥ TJA RATIO LATITUDE LONGITUDE LATITUDE LONGITUDE LATITUDE LONGITUDE TIME DURATION HTA9 NOS NNS DIAMETER UNIVERSAL SOUTHERN LIMIT NORTHERN LIMIT CENTER LINE **SAROS 128** 

1.13 IQI E.QI EE

7. \[ \text{0.1 } \text{20.1 } \text{0.1 }

7.5

94 S.2 100

STIMIL

#### TOTAL SOLAR ECLIPSE OF 13 NOV 2012

											•
1:42:1	8.721	8.842	ø.ø	1.0331	8.7 <b>0</b> 8	<b>₽.</b> 86-62-	4.38 eT	8.2- 0£-	3.81 \\ \psi \	₽.S- 6S-	LIMITS
0:31:Z	7.84I	7.632	9.7 <u>1</u>	9850.I	ø.82 86	7.08-38-	7.01 7e	7.64-38-	8.04 66	6:6- 98-	24:62
		2.882	9.52	1140.1	1,83 801	8.13-76-	3.73 301 5 %; 50		9.03 TOI		23:36
7.28:2	154.2				113 20.4		5.28 211	7.73-68-	2.8 411		23:38
8.84:2	1.631	9.172	32.1	1.0428							
2:58.9	8.291	4.772	ε. γε	1.0442	2.84 811	8.82-@ <del>1</del> -	118 5.4	8.8- 14-	119 24.9	9.03-68-	23:24
8.e :£	165.8	8.282	8.14	1.0453	123 35.5	0.81-14-	1.1 821		124 8.1	1.35-04-	23:18
3:19.2	2.891	4.882	6.3 <del>1</del>	1.0463	3.63 721	6.64-14-	0.18 TS1	1.26-24-	128 26.4	£.8- I4-	23:12
7.72:E	Z. ØTI	2.462	7.64	1740.1	132 4.4	-45-11.5	131 41.5		132 26.Ø		23: 8
3:35.2	9.171	2.008	1.63	8740.1	132 64.4	1.42-24-1	136 36.8	6.6- 64-	8.01 361	2.88-14-	23: Ø
8.14:8	£.57I	7.8&£	2.83	1.0483	0.28 eei	£.82-24-	9.61 <b>6</b> 81	1.31-84-	139 43.5	9.14-14-	55:2 <del>4</del>
3.74:8	8.47 <u>I</u>	7.8IE	ø. 63	8840.I	142 69.2	-42-25.2	142 61.8	9.21-64-	143 6.9	8.75-14-	22:48
3.52.2	7.871	5.125	3.13	Z640. I	4.71 841		9.41 841	1.8- 64-	3.61 841		22:42
3:56.1	9.971	3.628	9. 59	3640.1	8.72 e41			1.74-24-	149 25.5		22:38
		7.8EE	4.38	8640.I	5.15 231	2.78-14-	7.78 231	0.32-24-	162 24.8		22:38
Ø.63:E	4.771				155 28.8	8.6- IA-		4.73-14-	166 18.3		22:24
Ø.1 : 4	Ø.871	3.848	8.88	6640.I							22:18
4: 2.Ø	9.87I	1.638	9.79	1.0500		E. 7E-04-		-41-24.3	128 6.8		
2.2 :₽	Ø. 671	ø.ør	<b>6.</b> 78	1.0500	9.8 191		161 26.6	2.84-@4-	6.03 09I		22:12
3.1:4	£.671	6.02	T. T.	0090'I		8.71-68-		2.E- @4-	163 31.5		22: 6
6.63:£	3.671	4.18	6.88	6640.1	2.88 331	7.0E-8E-	166 57.6	6.31-96 <del>-</del>	E. 9 33I	Q.84-7ε-	8 : 22
3:57.4	3.671	2.14	9.39	7640.1	7.11 ear	1.68-78-	0.68 691	T.SS-8E-	0.34 831	3.33-86-	51:24
8:54.Ø	4.67I	Ø. Ø3	6.59	3640.I	6.84 ITI	0.64-86-	8.81 271	₽.3Z-TE-	9.61 171	3.0- 86-	21:48
9.64:8	1.971	<u>6.73</u>	8.13	1640.1	174 25.6	-36-42.2	0.83 ATI	2.62-86-	173 64.Ø	0.1- 3E-	21:42
8.44.8	7.871	6.49	5.63	7840.1	1.8 771			-36-16.2	£.62 971		21:38
8.98:E	Ø.871	1.17	8.83	7840.I		8.32-25-		6.8- 48-	8.8 971		21:30
		3.87	3.53	7740.1		- 3.6- 26-		1.84-26-	9.11-871-		21:24
3:32.4	Ø. TTI			0740.I		- 8.74-88-		1.22-18-	7.42-371-		21:18
3:24:9	175.7	4.18	1.03					1.13-62-	9.82-271-		21:12
3.31:8	Ø. 47I	8.38	7.84	1.0462		- 2.81-62-					
ε.Υ :ε	7.171	8.68	42.4	1.0452		- 6.04-72-		7.11-82-	7.02-691-		9:12
2.57.1	9.89I	93.5	6.7£	I + 40. I	£.8- 391-	- 8.63-32-	2.12-491-	6.12-92-	-165-54.3	7.42-32-	21: Ø
2:42:2	164.5	6.96	8.28	7240.I	1.11-191-	- 7.23-62-	8.02-091-	1.81-42-	E.&- S81-	8.82-62-	50:64
2:32:1	128.8	I.00I	7.8S	ØIÞØ'I	-126-26.3	- 7.1E-12-	7.0E-381-	-21-53.2	-167-2Ø.3	E. 6- IS-	8≯:ØZ
7.31:2	150.2	1.881.4	6.81	7850.1	1.4- 031-	- 18-33'2	-148-26.3	1.84-81-	Ø'6- 191-	▶.71-81-	ZØ: 4Z
2 31.0	0 221	, 02.	• • •								
1.14:1	126.2	108.5	ø.ø	7280.1	3.81-661-	- 6.0- SI-	3.64-281-	4.72-21-	9.42-881-	8.82-11-	LIMITS
YTIJATOT	WIDTH	Z∀	TJA	OITAR	TOMOT LODE	LATITUDE	FONGTIODE	LATITUDE	LONGITUDE	PATITUDE	TIME
VII IATOT	HTA9 HTGTW	NOS		DIAMETER	_0.122010	, WI I		and all laborates to 1	_014401101		NNINEBOY
MOTTAGIIA	UTAG	14112	IALIO (	771117	3 FINE	רבעובו	ITWT7 N	SOUTHER	N LIMIT	מטע ו חבע	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
					DIAT I C	ココエルコン	TTMT ! N	פחו ודגובם	TINT I N	asutanii	
		100									SAROS 133
Sec 4.3√	= T st	leQ				וע ברדדגפב ו	/700 7VIC:			1	ser 20042
				7 T (X 7	, VIN 2.1 74		with Millian				

ANNULAR SOLAR ECLIPSE OF 10 MAY 2013

Delta T = 75.8 Sec

SEI 208A2

7.41:4	2.55.5	T.782	ø.ø	9656. Q	4.61 T21 T.SS-8-	0.61 721 2.72-8-	-4-28.3 126 48.5	LIMITS
4.88:4	≯.80Z	7.882	9.7 <u>t</u>	1446.Q	8.38.2 142 3.86-0	8.72 241 8.8E-I-	7.24 142 4.22 @	5:15
2,84:4	201.5	Ø.682	25.3	Ø946.Ø	0.04 841 8.E I	I.88 84I 9.3 0	7.24 841 7.0 S	9:2
4:58.Ø	7.9er	8.682	2.18	£746.0	8.8 831 7.9 2	1 14.0 153 Ø.1	1.8 £31 8.4 £	Ø : 2
6: 9: 9	6.291	7.68Z	2.88	3846.0	8.35 331 7.33 2	2 2.5 156 32.9	3 50.4 156 38.0	1:24
0:31:9	6.68I	2.062	7.04	\$6\$6.0	8.78 931 I.18 8	0.48 931 1.88 2	1.04 931 7.52 A	1:48
5:22.5	£.78I	6.8es	7.44	ZØ96'Ø	1.71 281 1.88 8	1.51 231 1.4 E	7.02 231 8.74 A	1:45
6:29.5	186.2	6.162	4.84	6036.0	0.14 431 7.81 A	2.88 481 8.22 8	2 4'8 184 42'E	1:38
8:35:3	183.4	Ø.862	6.13	9196.0	4 25,2 166 52,5	8.84.8 16.9 8.48	6.13 381 8.31 3	øe: I
9:17:9	8.181	3.462	1.99	Ø236.Ø	4 31,4 168 54,3	8.74 881 8,14 8	8.0 631 T.02 3	1:24
8.84:2	3.081	4.862	2.83	9236.0	2.84 NTI 8.28 A	8.04 071 8.84 E	4.33 \NT 8.12 3	81:1
6:11:3	2.971	8.862	1.18	8.9529 8.9529	8.38.1 172 35.6	8.72 271 7.14 E	8.84 271 8.81 3	1:15
5.55.2	1.871	8.108	8.59	££36.0	8.71 471 8.82 A	3.8 471 7.38 8	7.82 471 1.11 3	9:1
3.83:3	1.771	3.808	8.89	8836. à	4 13.5 175 55.2	3 26.1 175 45.2	2.8 871 8.0 8	ø∶τ
ø:I:9	2.971	3.018	3.89	8£36.0	I.62 771 0.0 4	2.81 771 2.81 E	1.04 771 3.84 4	\$9:Ø
6. Z : 9	175.3	Ø.918	ē. ģŢ	Ø+36.0	0.0 eti 4.54 e	2 67.1 178 48.3	8.11 971 E.92 A	84:Q
Ø. 4 : 8	174.6	8.52E	2.27	Z+96.0	3.18-971- 7.82 8	0.44-671- 6.78 S	8.81-671- 1.6 A	Z≯:Ø
4.4:8	8.E71	4.IEE	4.87	8,9643	9.4-871- 0.1 E	2.81-871- 8.31 2	4.13-771- 0.84 £	98:Ø
2.4:8	I.SYI	8. I 4E	2.47	4436.0	7.65-371- 4.38 Z	1 50.5 -178-53.8	3.32-371- 0.02 £	øe:ø
8.8:3	172.5	3.135	74.3	4436.0	4.81-871- 9.8 S	2.08-371- 4.22 I	3.0- 371- 1.13 S	\$:5 <b>₹</b>
7.1 : 9	1.271	9°I	Ø. 47	4436.0	3.13-671- 8.36 1	I.T- 471- 3.13 @	9.36-67I- 4.9I S	81:Ø
9:69:9	7.171	Ø.II	Ø.EY	4436.0	7.72-271- A.1 I	9.54-271- 8.71 Q	4.11-271- <b>9.44</b> 1	8:15
8.83:3	3.171	£.61	8.17	8,96.8	8 24.3 -171 -3.3	I.02-171- 8.61-0	4.84-QTI- 3.T I	9 :Ø
6:53.6	3.171	26.3	8.69	1436.8	8.78-681- 8.31-0	8-59-2 -169-55.3	4.02-631- 2.72 @	ø :ø
6.64:3	7.171	32.1	8.73	Ø+36.0	8.01-891- 1.63-0	-1-45.3 -168-28.8	8.23-731- 2.81-8	<b>53:64</b>
7.34:3	172.0	6.98	4.39	7839. Ø	3.14-831- 3.34-1-	0.03-331- T.82-2-	9.52-331- 8.2- 1-	23:48
1.14:3	172.6	8.04	8.29	9836.0	2.6- 381- 4.38-2-	1.82-381- 8.81-6-	2.03-43I- T.23-I-	23:42
1.86:3	4.871	1.44	1.09	\$ 823 B	1.88-881- 0.62-8-	4.23-531- 2.21-4-	9.21-631- 2.84-2-	23:38
8.08:3	3.471	6.94	1.73	8236. <b>0</b>	4-26.6 -161-52.Ø	7.11-281- 0.01-8-	1.26-161- 8.64-6-	23:3Ø
5:25:2	176.9	6.64	Ø. 43	Ø'823	7.4- 031- 8.82-3-	7.42-031- E.SI-8-	9.44-631- <b>6.34-4</b> -	23:24
6:19.3	9.771	4.13	7. Q3	8136.Q	9.6- 831- 8.38-8-	7:62-831- T.61-Y-	1.64-731- 6.13-3-	23:18
1.51:3	9.671	2.63	1.74	8.9512	2.4- 831- 8.84-7-	3.42-831- 0.66-8-	8.64-331- <b>0.4</b> - 7-	23:12
8.8 :3	1.281	6.43	43.3	9096.0	8.34-831- 6.7- 6-	6.3- 431- 4.83-6-	-8-22.8 -153-25.Ø	23: 8
7.63:4	185.1	9.83	1.68	7649. Q	2.9- 131- 9.38-01-	-11-22.6 -161-29.2	7.84-031- 8.64-6-	23: Ø
4:52.5	7.881	2.83	3.48	8846.0	8.7- 841- 9.41-21-	0.72-841- 9.2- E1-	8.74-741- 8.72-11-	22:54
8.44:4	1.591	ø. øə	2.62	9749.0	8.72-441- 4.6- 41-	7.34-441- 4.63-41-	0.6- AAI- 0.02-EI-	84:22
4:35.8	Ø:66I	1.28	8.22	1946.0	7.14-8EI- 8.8Z-8I-	2.83-981- 2.22-71-	9.35-26.6 -139-25.8	22:42
7.42:4	e. Tas	2.39	7.81	9849. Q	4.71-281- 2.44-91-	4.91-281- 9.44-02-	7.11-281- 8.34-81-	86:22
6.01:4	2.222	E.&T	ø.8	3046.0	2.88-eII- 0.82-42-	8.46-911- 4.72-32-	8.73-811- 8.18-62-	STIMIL
DURATION YTIRAJUNNA	HTA9 HTGIW	Z¥ N∩S	NUS TJA	DIAMETER RATIO	LATITUDE LONGITUDE	LATITUDE LONGITUDE	LATITUDE LONGITUDE	UNIVERSAL TIME
MOTTAGIN	UTAG	CHIN	14112	GITINATO	CENTER LINE	SOUTHERN LIMIT	NORTHERN LIMIT	.,002/12/11/

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#### Table 52

Delta T = 76.2 Sec

ANN/TOT SOLAR ECLIPSE OF 3 NOV 2013

T.0 :0	T. Ø	7.432	ø.ø	7.0002	2.21-74-	9.18 8	7.21-7 <b>4-</b>	6.1E 8	7.21-74-	3.15 8	LIMITS
T7.73:0 T0.64:0 T5.14:0 T2.15:0 T2.81:0	4.0.4 3.1.5 2.5.2 15.8	2.68.1 262.0 262.7 263.4 263.4	4.04 7.35 3.08 7.52 1.4.4	2110.1 1010.1 8800.1 0700.1 4400.1	1.84-81- 7.01-71- 3.81-12- 8.12-82- 8.1- 48-	0.410 0.3 0 2.75 0 2.05 1 3.8 5	9.84-81- 13.41-71- 2.42-13-4.5 3.4-4.5	8.2- \( \) 2.31 \( \) 2.34 \( \) 7.76 I 7.51 \( \)	4.84-71- 2.8-71- 2.11-12- 2.61-8.4- 2.93-58-	8.32-0 2.82 0 8.22 1 8.52 5	14: 8 14: 12 14:18 14:24
T7.78:1 T7.88:1 T7.88:1 T6.92:1 T1.82:1 T7.12:1 T7.12:1 T9.81:1 T9.81:1	8.58 6.99 6.98 6.98 6.98 6.98 6.98 6.98 6.9	2.05.0 2.05.0 2.05.0 2.05.0 2.05.0 2.05.0 2.05.0 2.05.0 2.05.0 2.05.0 2.05.0 2.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.05.0 3.	8.83 63.83 63.83 63.83 63.84 7.44 7.44	7310.1 7310.1 7310.1 7410.1 7410.1 7410.1 7510.1 7510.1	2. 74-01- 8.8- 8.8-8- 2. 74-8- 2. 74-81- 2. 74-81-	9. £2-0 8. £2-0 6. £2-0 8. £1-0 6. Ø 6. Ø	7.25.1 6.85.2 7.36.1 6.85.6 7.25.1 6.82.1 7.44.3 7.44.3 7.44.3 7.44.3	7.88.1 7.88.1 1.82.1 8.4.3 8.4.3 8.4.3 8.4.1 8.11.0	2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43 2.43	20.92 8.08 8.08 1.08 1.08 1.08 1.08 1.08 1.08	75:25 13:54 13:51 13:51 13:51 13:51 13:51 13:51
17.82:1 17.62:1 17.62:1 17.06:1 11.06:1 11.06:1 17.06:1 17.06:1 10.06:1	6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 6.48 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7.21 11 7.21 11 7.21 11	2.81 Ø1 0.81 6 0.81	7.63 \$2.5 3.5 3.5 3.5 3.5 12.9 26.7 12.62.9 14.23.2 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 11.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 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12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12.26.7 12	7.305 9.325 9.325 9.45 9.45 9.45 9.45 9.45 9.45 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.55 9.5	9.85 1.45 1.45 1.45 1.45 1.45 1.45 1.45 1.4	8.89 %I F. 19 7 7 8 8 8 1 8 1 8 1 8 1 8 1 8 1 8 1 8 1	0 : 21 12 : 12 12 : 36 12 : 36 12 : 36 12 : 36 13 : 36 14 : 31 15 : 31 16 : 31 17 : 31 18 : 31 18 : 31 19 :
19.8:0 14.02:0 11.18:0 12.04:0 11.84:0 14.33:0 10.2:1 11.8:1 13.8:1	4.8 8.81 2.42 8.42 8.75 8.75 8.74 8.74 8.84 8.84	6.711 6.711 6.131 6.431 7.181 7.181 6.481 8.481	6.08 8.08 8.08 8.08 8.08 8.08 8.08 8.08	6000.1 8400.1 6300.1 3800.1 7600.1 7110.1 3210.1	6.3 68 4.4 6.3 4.4 6.4 6.9 8.4 8.62 76 8.62 7.5 8.62 92 8.63 14 8.63 1	28 15.9 28 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	6. 56. 54 6. 56. 54 6. 52. 54 6. 52. 75 6. 52. 95 75. 61 75. 62. 95 75. 95	2. 71 82 2. 63. 9 2. 63. 9 2. 63. 15 3. 61. 7 2. 64. 4 2. 64. 4 3. 64. 4 3. 64. 4	63 64.1 63 65.5 64.8 6.8 34.9 7.20 46.9 7.20 46.9 7.21 72.7	8.6 43.8 6.2 43.8 1.8 52.4 1.5 1.5 1.5 23.8 1.5 23.8 1.5 32.0 1.1 16.3	8 : II 9 : II 98 : II 98 : II 98 : II 98 : II 99 : II
DURATION ANNULARITY 1.4.1	HTA9 HTGIW 0.4	NUS ZA 6.701	NUS 9	DIAMETER RATIO ©.9989	R LINE LONGITUDE 71 12.2	CENTE LATITUDE 30 26.5	N LIMIT LONGITUDE 3.81 IT		N LIMIT LONGITUDE 7.1 12.9		UNIVERSAL TIME STIMIJ

# ORIGINAL PAGE IS OF POOR QUALITY

Delta T = T stied

## Table 53

2019	ЯAМ	ØZ	40	ECLIPSE	SOLAR	<b>JATOT</b>

2.9 :2	9.604	196.2	ø.ø	1.0395	0.71-24-	8.83 78	2.48-111-	8.8£ T8	63 32.6	3.68 88	LIMITS
2:24:1	413.2	4.07I	8.8	4140.1	9:38-81-	Z.13 Ø8	ø. 01-22-	5.35 TT	2.2- E-	2.83 38	7Q:14
1.82:2	415.3	3.891	9. Q.T	1.042Ø	4.81-81-	6.23 87	6.83-81-	1.8 37	6.64-8-	2.88 28	78:15
2:31.4	7.714	2.631	1.21	1.0425	5.75-21-	6.21 77	0.71-81-	74 4Ø.3	6.13-3-	7.81 @8	øī:øī
2.48:2	4.024	£.091	£.81	1.0429	0.52-01-	4.44 37	7.83-51-	4.42 ET	1.15-4-	2.82 87	8 : ØT
2:36:5	8.824 A 80A	5.73I	5.41	1.8432	2.42-8-	74 24.3	9.33-11-	0.41 27	4.3- 6-	9. 03 97	9 : õt
8.88:2	4.824	1.881	1.31	1.0435	2.85-8-	3.01 EY	8.6- \( \text{0.1-} \)	9.7 IT	Z.@4-I-	7.82 87	7 : Øī
4.04:2	8.624	1.521	6.31	7.840.1	2.83-4-	3.1 27	6.61-8-	3.3 QT	8.81-0	9.7 AT	z : ői
2:41.9	8.884 8.004	150.5	3.81	1.6439 7210 1	2.22-E-	9.83 &Y	8.24-8-	2.8 69	8.4 I	9.33 27	ø :øt
0 11.0	433 3	3 631	3 81	1 8430	2 22-8-	0 83 87	8 61-8-	6 9 09	<i>0</i>	0 33 02	
2.64:2	6.984	148.3	Ø.TI	1440.1	7.23-1-	9.33 69	8.01-3-	3.6 89	2 24.3	4.84 IT	89:6
2:44.3	7.044	1,841	3.71	1.0442	8.82-@	Ø.73 88	8.24-6-	2.31 78	3.42.5	8.44 &T	99:6
2:45.2	7.444	Ø. 44I	6.71	1.0443	8.83 Q	I.I 88	6.71-S-	6.22 99	7.63 A	8. pp 69	<b>79:6</b>
2:42.9	7.844	6,141	1.81	PPPØ'I	2.17.5	4.7 Ta	8.33-Q	₱.SE 33	2.81 8	8.84 88	3:62
4.84:2	462.8	6.681	£.81	1.0445	2.7E E	9'91 99	6.42 @	8.84 43.6	4.28 T	67 61.3	Ø9:6
8.84:2	6.834	6.78I	3.81	1.0445	Ø.88 A	9.32 39	0.44 I	2.83 58	7.84 8	1.83 88	87:6
6.84:2	Ø.194	132.9	3.81	8440.I	2.41.8	1.78 48	8.2.8	63 10.2	10 6.4	7.8 88	97:6
6.84:2	Ø.394	6.EEI	3.81	9440.I	7 32.5	Ø. Ø3 E9	0.02 A	6. 25.5	11 23.Ø	Ø.71 33	<b>77:6</b>
7.84:2	Ø. 694	6.1EI	18.4	1.0445	2.13 8	£.4 £8	7.78 3	8.14 18	8.I4 <u>2</u> I	6.82 48	2≯:6
2:46.4	7.274	129.9	£.81	1.0445	T. OI OI	8.61 29	7.33 8	£.63 @9	14 2.4	1.24 68	ØÞ:6
8.34:2	£.874	6.72I	1.81	1.0444	3.18 11	£.8E I8	4.41 8	7.71 Ø8	16 25.2	6.88 58	88:6
2:46.1	3.674	152.9	8.71	1.0443	12 64.1	6.83 @a	£,4£ 9	Ø.78 93	8.03 SI	1.21 28	9:38
2.44.2	482.3	6.621	Þ.TI	1.0442	Ø. 61 11	9°21 Ø9	6'99 ØT	2.73 83	18 20.Ø	8.82 18	9:34
2:43.8	484.5	8.121	6.91	I++0.I	0.74 ar	6.18 63	9.61 21	58 18.2	7.83 er	4.84 Q8	9:35
7.14:2	Ø. 984	7.611	£.8I	6840.I	8.81 71	58 52.1	1.84 &1	0.04 Ta	Ø.88 IS	Ø.3 Ø8	Ø8:6
1.04:2	8.384	8,711	15.7	7540.I	18 25.5	2.81 83	Ø. 91 31	57 2.5	8.91 ES	€. 42 63	87:6
2:38:3	4.884	118.4	6.41	1.0435	Z.88 0Z	Ø.35 73	16 60.3	7.32 83	SP 12.6	2.44.8	97:6
2.36.2	8.484	2.811	Ø. 41	1.0432	22 28.9	3.73 83	I. 05 8I	9.64 33	4.42 TS	- 2.5 83	42:6
7.88:2	7.184	8.011	6.21	6240.I	24 30.0	7.02 83	6.8I &S	1.41 33	9.13 62	1.72 73	32:6
6.8E:S	9.874	£.801	7.11	1.0425	26 45.5	9.44.8	8.21 22	2.68 43	9. TA SE	4.64 83	øZ:6
	• •			20/2			- ,				
4.72:2	Ø.694	3.301	I.QI	1.042Ø	8.22 62	ø.e 33	24 21.1	Ø.3 43	3. QÞ 98	56 12.3	81:6
2.53.2	8.734	£.201	2.8	4140.I	3. 45. 28	2.48 43	7.84 82	₽.1E E3	8.8I 44	7.38 33	91:6
			• •								
7.8 :S	7.814	ø. £6	ø.ø	£6£0.1	Ø.1 64	7.88 83	42 12.1	5.13 13	2.44 84	6.28 33	STIMIL
YTIJATOT	MIDTH	Z∀	TJA	OITAЯ	LONGITUDE	LATITUDE	LONGITUDE	<b>JOUTITAJ</b>	-ONGITUDE	LATITUDE	TIME
DURATION	HTA9	NUS	NNS	<b>NIAMETER</b>							UNIVERSAL
					K LINE	CENTE	YIMIJ N	RAHTUOS	4 LIMIT	NORTHERI	

#### Table 54

Delta T = 78.3 Sec

#### TOTAL SOLAR ECLIPSE OF 9 MAR 2016

1.88:1	6.86	ø.392	ø.ø	8720.1	1.38 441 3.88 18	9.08 441 9.7 28	7.08 AAI 2.0 EE	LIMITS
7:16.3 1:50.0	8.711 1.801	252.8 259.3	8.12 2.6	aaso.i Tasa.i	8.71 781 8.71 92 8.83 481 1.82 18	8.82 731 4.84 82 8.18 331 8.43 &8	2,01 10,12 10,2 3,2 15,1 15,1 19,3	88:8 86:8
2:32:3	124.3	8. TAS	8.82	1°0362	8.8 ATI 9.AE TS	6.8 ≯\! 0.0 \\	7.8 ATI 1.01 82	3:24
2:48.5	4.6SI	0.44S	8.48	1880.1	0.21 971 4.2 82	2.8 eTr @.T2 a2	1.71 971 0.88 82	3:18
2:58.9	133.5	8.042	8.68	1.0394	24 36.8 -176-42.3	2.13-871- 8.0 A2	25 12.Ø -176-34.Ø	3:12
8.9 : 8	8.8EI	8.782	44.5	1.0404	9. EI - ETI - 0. AI ES	22 38.Ø -173-25.2	1.6- 671- 1.83 62	8 : 8
8.61:8	6.681	7.482	7.8 <b>≯</b>	£140.1	7.11-071- 8.33 12	6.42-071- 2.el 12	0.63-691- 8.18 SS	3: Ø
8.82:8	142.4	9.182	9.23	1.0421	8, 82-781- 4.88 &S	7.84-781- 2.8 \@S	21 15.8 -167-14.6	5:54
6.88:8	7.441	2.822	5.83	1.0428	19 25.8 -165 -1.Ø	1.71-331- 3.64 81	28 2.3 -164-45.3	2:48
0.44:E	3.841	224.4	9.69	1.0433	7.44-281- 8.41 81	8.1- 881- 0.88 TI	18 50.8 -162-27.8	2:42
8.68:8	148.4	220.1	8.29	8640.1	3.75-031- 3.4 71	16 28.2 -160-55.6	8.91-081- I.IA TI	2:38 5:38
3:55.6	6.64I	215.1	7.39	I + + Ø · I	3.76-831- 3.88 31	16 20.1 -168-56.4	8.81-831- 0.88 81	
2.0 : A	161.2	1.602	4.89	1.0445	8.84-831- 9.94 AI	13.5 -157 -2.9	15 26.4 -156-23.9	2:18 5:24
8.8 :4	152.4	Z. IQZ	T. ØT	7440.I	9:63-431- 7:44 61	13 8.2 -165-13.6	14 21.2 -154-33.6	21:2
9.9:4	123.4	8.291	8.27	6440.I	12 40.7 - 153 - 15.2	7.72-631- 8.4 SI	5.2- 151- 5.41 21 7.84-51- 2.71 51	2: 6
4.8 :4	154.2	1.281	Ø. 47	0340.I	1.82-131- 0.88 11	7.1- 031- 1.0 01 0.44-131- 3.1 11	3.61-941- 0.51 11 5.2-131- 3.41 9.5	ø : Z
£.9 :4	154.8	Ø. ØTI	8.47	1.0450	9.04-641- 3.88 QI	2 1- 031- 1 0 01	3 01-041- N ST 11	<b>9</b> · C
4:6 :4	122.3	167.2	8.4T	1.045Ø	7.83-741- 1.88 e	8 59.7 -148-20.0	4.78-741- 3.SI QI	1:24
9.8 :4	122.5	145.Ø	Ø. AT	6440.I	8.31-841-8.88	1.86-841- 4.0 8	9 13.2 -145-55.1	1:48
7.8 :4	122.5	134.2	9.27	TAAQ.I	8.88-44 <u>1</u> - 8.88 7	7 2.2 -144-55.1	0.11-441- 9.41 8	1:45
0.4:4	122.4	125.2	T. &T	1.0445	7.84-241- 4.14 8	2.01-641- 1.3 8	I.72-24I- 7.7I 7	1:38
4. Ø : A	6.431	Ø.SII	4.89	1.0445	5 45.4 -141 -1.2	5.22-141-1.6 3	8.98-041- 8.12 8	1:30
8.33:6	1.431	212.3	7.39	1.0438	4 20.4 -139 -9.9	2.16-981- 8.41 4	5 26.5 -138-48.4	1:24
3:50.4	1.631	8.T&I	8.28	1:0434	7.61-761- 7.88 E	8.46-761- 7.02 E	4 32.6 -136-52.4	81:I
8.44:E	121.6	104.2	7.63	6240.I	4.11-351- 2.4 E	2 28.3 -135-32.3	2.03-421- 6.68 E	1:15
8.88:8	8.641	₽.ſØľ	5.33	1.0423	2.1- 661- 0.61 2	9.12-881- 4.78 I	2 48.5 -132-40.3	9 : 1
3:28.4	4.741	2.66	8.23	9140.I	2.14-081- 2.82 1	8.1- 181- 8.74 Q	1 58.5 -130-20.4	ø:t
1.91:8	9.441	<b>≯</b> .76	7.8⊁	1.0408	8.8- 821- 2.38 @	8.82-821- 2.0 Q	8.74-721- 0.01 I	\$9:0
8.8 :8	2,141	ø. 96	3.44	86£0.1	8.91-321- 9.01-Q	8-45.4 -125-39.2	0.83-4-124-58.9	84: Ø
A. 73: 2	I.TEI	ø.36	6.68	7850.1	0.8- 122 -8.0	7.72-221- 3.82-1-	7.74-121- 8.02-0	8:42
7.44:2	1.281	8.49	8.48	4780.1	-1-35.1 -118-25.2	9.2 -118-45.Ø	7.4- 8II- I.S- I-	98:0
2.88:2	9.321	8.86	8.82	1.0357	7.63-EII- @.II-S-	2.41-411- 2.54-2-	7-39.0 -113-32.5	Ø8:Ø
2:12.8	8.711	7.86	4.12	1.0335	0.63-701- 1.98-S-	7.31-801- 0.01-E-	8.62-T&L- 4.8- 2-	Ø:24
4.74:1	2.401	ø. 46	4.6	8620.I	4.91-79- 6.44-S-	8.73-76- 6.41-6-	1.76-86- 3.71-2-	81:Ø
£.8E:I	8.86	4.49	ø.ø	6920.I	4.82-88- 4.81-2-	4.81-88- E.14-2-	-1-5ø.3 -88-22.2	LIMITS
YTIJATOT	MIDTH	Z∀	TJA	OITAЯ	AUTITUDE LONGITUDE	LATITUDE LONGITUDE	LATITUDE LONGITUDE	TIME
DURATION	HTA9	NUS	NUS	DIAMETER	7NT7 V71V70	LIMITA ANIANI COC	1 TWT - 100011 1000	ONIVERSAL
					CENTER LINE	SOUTHERN LIMIT	NORTHERN LIMIT	

### ANNULAR SOLAR ECLIPSE OF 1 SEP 2016 Delta T = 78.7 Sec

	DURATION ANNULARITY 2.14:3 2.49.1 2.49.1 2.13:2 2.53:3 5.53:4 5.53:4 5.53:4	PATH WIDTH 152.2 136.2 126.4 121.7 118.6 116.9	XA XA 6.18 6.18 8.67 7.77 8.87	NUS TJA 0.0 0.0 1.45 3.08 6.04 0.04	DIAMETER RATIO Ø.9539 Ø.9659 Ø.9654 Ø.9674 Ø.9685 Ø.9685	CENTER LINE  -2.3 19 4.5 28.9 4 13.0 28.9 4 13.0 28.9 4 13.0 28.9 4 13.0 28.9 4 23.7 20.8 -18-62.9 22.0 -16-36.1	E- 7.02 eI  19 20.7 -3  1- 4.84 4  1- 7.0. 2-  1- 7.0. 2-  1- 7.6. 3-  1- 13.36.21-  1- 3.36.21-	SOUTHER LATITUDE -3-46.5 -2-8.6 -1-61.2 -1-64.1 -2-7.2 -2-7.2	2 39.7 19 21.4 3 39.7 -2-48.0 -11 -3.4 -14 -9.4 -14 -9.4		UNIVERSAL TIME 7:36 7:36 7:42 7:42 7:48 7:48
	ANNULARITY 2:41.3 2:46.2 2:49.1 2:53.5 2:53.5 2:53.5	HTDIW 2.231 1.781 2.081 4.321 7.121 7.121	2.4 6.18 6.18 8.67 8.87 7.77	ALT 0.0 4.31 3.4.5 3.05 3.08 3.36 3.04	01TAR 0.9596 0.9639 0.9659 0.9659 0.9686	3.4 91 E.2- 0.51 4 8.82 7.42-2- 3.31 7.6-7- 8.82 8.34-81- 3.38 8.34-81- 3.38	E- 7.02 61 -1- 4.84 4 -1- 7.0- 21- 7.64-31- 8.72-011- 8.72-011- 2.38-21-	-3-46.5 -3-46.5 -3-46.1 -3-46.1 -3-46.8	A. IS 91 7.98 8 8.84-2- 6.82-7- 4.8- 11- 4.9- 41-	0.52-2- 0.94-0 0.94-0 0.04-0 0.7.74-0 1.4-1-	TIME CIMITS 42:7 5:36 7:36 7:48
	2.84:2 2.49.1 2.53.5 2.53.5 4.63:2	1.781 2.081 2.081 1.081 7.121 6.811	1.18 3.08 8.97 8.87	16.4 24.5 38.5 35.6 40.0	6596.0 6396.0 4736.0 3836.0 4636.0	0.81 4 9.82 7.42-2- 8.82 7.6- 7- 8.02 8.34-01- 3.03 9.53-61- 3.03	-1-	8.8- 2- -1-51.2 -1-54.1 -1-54.1 -1-54.8	7.88 8 8.84-2- 8.82-7- 4.8- 11- 4.8- 41-	9.94-0 8.04-0 7.74-0 1.4-1-	42:7 88:7 84:7 84:7
	2:49.1 2:53.5 2:55.4 2:55.4	138.2 125.4 7.121 118.6	8.87 8.87 7.77	24.5 30.5 35.6 40.0	6396.0 4796.0 3896.0 4696.0	7.4.2-2-3.31 7.8-7-8.02 36.8-10-18-8 8.34-01-3.93 8.34-61-3.83	-1- 7.0- 2- -1- 7.84-8- -1- 8.72-01- -1- 2.38-21-	2.13-1- 1.43-1- 2.7- 2- 8.82-2-	0.84-2- -23.3 -11- -3.4 -12- 41-	8.04-0 7.74-0 1.4-1- 4.32-1-	42:7 88:7 84:7 84:7
	2:49.1 2:53.5 2:55.4 2:55.4	138.2 125.4 7.121 118.6	8.87 8.87 7.77	24.5 30.5 35.6 40.0	6396.0 4796.0 3896.0 4696.0	7.4.2-2-3.31 7.8-7-8.02 36.8-10-18-8 8.34-01-3.93 8.34-61-3.83	-1- 7.0- 2- -1- 7.84-8- -1- 8.72-01- -1- 2.38-21-	2.13-1- 1.43-1- 2.7- 2- 8.82-2-	0.84-2- -23.3 -11- -3.4 -12- 41-	8.04-0 7.74-0 1.4-1- 4.32-1-	86: T 86: T 24: T 84: T
	2:61.6 2:63.6 2:66.4	125.4 7.121 8.811	8.87 7.77	36.5 35.6 40.0	4799.0 3899.0 4699.0	7.8- 7- 8.02 8.34-01- 3.38 9.53-81- 3.83	-1- 7.84-8- -1- 8.72-01- -1- 2.86-21-	1.43-1- 2.7- 2- 8.82-2-	8.82-7- 4.8- II- 4.9- 4I-	7.74-0 1.4- 1- 4.82-1-	88:7 24:7 84:7
	2:63.5 2:55.4	7.121	8.87 7.77	35.6 40.0	3896.0 4696.0	3.54-61- 3.36 3.6.5 -13-52.9	-I- 8.72-01- -I- 2.86-51-	2.7- 2- 8.82-2-	4.6- II- 4.6- 4I-	1.4-I- 4.82-I-	24:7 84:7
	2:22.4	8.811	T. TT	0.04	\$696.0	6.53-51- 3.83	-1- 2.86-21-	8.82-2-	4.6- AI-	<b>▶.82-1-</b>	8 <b>7</b> :7
							• • • • • •				
					701010	T:00-0T- 0:77	-7- C'07-QT-	Z*TQ-Z-	6.14-81-	0.53-I-	7:64
	2:58.5	113.5	8.4T	T. 74	<b>6079.0</b>	8.1- 61- 1.13	-0- 3 810r_	, 01 0	~ ~-		
	8:69:2	4.111	3.27	1.13	4179.Q		* * * * * * * * * * * * * * * * * * *	4.9I-E-	8.71-91-	8.52-2-	ø :8
	0.1 :E	3.601	I.QT	54.3	6176.0	8.11-12- 1.82 8.73-8.73		8.03-E-	-21-28.8		9:8
	3: 2.Ø	8. Tar	2.78	2.73	£279.8		<u> </u>	3.42-4-	I.08-82-	£.18-8-	8:15
	3: 2.9	£.8&I	7.89	6.69	7270.0	<b>-</b>	• • • • • • •	8.0- 3-	2.52-23-	6.8- 4-	81:8
	7.8 :E	6.40I	3.63	4.28	Ø£79.8	5.36-82- 7.81 5.36-82- 8.43	<del>-</del>	5.65-3-	4.6- TS-	4.84-4-	8:24
0,0		9. EQI	3,43	8,48	2879. Q	8.21-06- 6.76		7.61-8-	Z. 03-82-	8.62-3-	Ø8:8
8 6	8.4 :8	102.5	8.84	9,88	4879.0	8.34-18- T.IS		8.2- T-	7.82-8E-	8.21-8-	8:38
$\Xi$		9. IØI	8.14	2.89	3879. Q	1.81-88- 7.7-		0.84-T-	8.63-15-	3.73-8-	8:45
77 2	3: 5.4	8.00I	34.1	<b>≯</b> .69	8879.Q	4.44-46- 8.33		7.15-8-	8.62-66-	8.54-7-	84:8
ZS	)						-8- 7.0E-4E-	1.61-6-	1.83-48-	8.18-8-	8:24
ORIGINAL OF POOR	3:5:5	100.2	9.32	S.&Y	8879.Q	4.11-86- 3.44	-9- 8.73-36-	יומ באו	M 30.96	2 10 0	<b>D</b> -0
ച	4 4 • 5	8.66	9.9I	3.87	8£79.0	7.78-78- 2.38		I.8- QI-	0.32-88-	0.12-e-	ø :6
<u>Р</u>	3.5.5	3.66	8,7	E. &T	8£79.@	0.4- 65- 8.72		8.83-01-	S.13-75-	8.11-01-	9:6
A C	3: 5.3	4.66	328.9	9.69	3879.Q	8.02-04- 8.12		2.13-11-	4.71-6E-	2.4- II-	21:6
S 7	3: 5.1	8.66	321°0	3.89	££79.@	17.2 -41-58.9		2.84-21-	2.44-Q4-	1.83-11-	81:6
PAGE IS	7.4 :€	6.66	9.648	Ø.78	1879. Q	14.6 -43-28.9		0.14-81- 8.85-11-	2.21-24-	9.63-51-	77:6
	8.4 :E	100.5	8.788	1.39	6276.0	8.1- 34- 8.51	<del>-</del> - · -	8.86-41-	2.24-E4-	8.03-51-	Ø8:6
Z 22	8.8 :8	E. IQI	1.288	6.29	8279.0	0.88-84- 9.4I		1.86-31-	8.41-34-	7.64-41-	98:6
	E.E :E	E.S&I	8.728	3.09	227e.0	9.81-84- 2.81		8.65-81- 8.64-71-	0.13-84-	4.03-31-	24:6
	3: 2.6	9.5QI	1.626	6.73	8179. Ø	8.3- 03- 8.52		6.64-81-	7.15-84-	2.63-81-	87:6
								0105 07	Z.8I-03-	1.83-71-	<b>†</b> 9:6
	8: I : 8	102.2	8.918	ø.33	EITE. 0	31.6 -51-59.5	-61- 2.74-13-	0.83-e1-	7.11-23-	h 3- or-	ישי ש
	3: 1.1	Ø. TØ£	9.315	6.13	8076.0	42.4 -64 -2.4		9.6- 12-		-19 -5.4 -19 -5.4	9 :01 70: 0
	3. ø . ɛ	2.6&I	7.218	48.5	2076.0	6.81-88- 8.88		-22-24.5	1.82-58-1	-20-15.3 -21-28.3	10:18 10:6
	2.63:2	8.111	9,60£	6.44	9696.Q	9.34-83- 9.8I		-23-43.3	£.83-83-	8.44-22-	10:15
	2:58.1	6. <b>⊅</b> II	9.90£	Ø. I4	9896.Q	8.48-18- 1.88		9.8- 32-	3.61-13-	3.8- 42-	81:01
	8.83:2	8.811	9.50£	3.88	TT36.0	0.64-48- 8.E-		4.86-82-	4.88-48-		10:24
	2:56.4	123.Ø	E. QQE	7.IE	9996'Ø	8.14-88- 1.9E		-28-13.9	£.84-88-	3.15-32-	10:38
	7.53:2	7.82I	7.8eS	6.32	1996.0	4.36-67- 4.35.4		2.8- 08-	8.48-87-	8.4- 72-	10:36
	2:51.6	136.5	Ø.262	18'2	Z£96.@	3.72-08- 4.18		5.41-26-		0.84-82-	10:42
								01 LT 70-	E.3I-08-	4.64-08-	8 <b>+</b> :ØI
	7.84:2	9.731	6.672	ø.ø	£836.0	1.61-001- 2.8E	-36- 7.16-001-	4.12-98-	£.86-@@I-	7.33-46-	LIMITS

#### 7able 56

#### ANNULAR SOLAR ECLIPSE OF 26 FEB 2017

8.71:1	1.06	4.192	ø.ø	£876.0	3.73-82-	2.83-\r	I.02-72-	7.61-11-	0.1- 72-	6.28-&1-	STIMIJ
8.43:0 2.0 :1 3.5 :1 3.5 :1 6.7 :1 6.4:5	9.74 9.13 9.33 4.53 8.83	277.Ø 273.9 273.1 268.6 265.9 3.582.6	6.04 6.05 8.15 8.9 8.9 8.8 8.9	7889.0 8789.0 7889.0 4889.0 3889.0	8.83 8 7.03 8 9.81 0 7.84-9- 7.84-9- 2.71-12-	8.61-I2- 2.63-61- 8.12-81- 6.84-41- 2.84-41-	8.85 8 8.85 8 9.02-4- 9.02-4- 8.91-62-	7.28.12- 6.2.02- 7.6-31.0 1.6-81.2 1.6-61.2	3.3 7 8.85 8 8.85-8- 8.81-9- 3.84-91-	1.11-12- 9.64-91- 2.11-81- 2.06-31- 3.46-41- 8.13-11-	9:91 16:12 16:18 16:24 16:38
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8.71:I	1.08	9.68	7.91	1.0205	150 53.2	43 23.2	2.8 Ø	7.ø 15	43	161 40.2	8.88 84	18:24
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9.64:2	9.131	3.608	7.81	1.0384	6.88 3 <i>T</i>	3.72-72-	6.2 ar	T.62-82-	6.8 AY	1.72-82-	20:38
3:2:5	4.731	312.2	1.62	7680.1	Ø.32 e7	-25-41.8	7.1 eT	6.04-82-	8.34 67	9.44-42-	Z8:9Z
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7.28:8	۵.۲۲۲	3.918	32.5	1.0425	8.22 T8	-22-13.2	0.21 T8	£.8- £2-	₽.SE 78	8.81-12-	82:82
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7.8⊁:ε	£.871	7.525	2,78	1.0434	9.12 19	2.14-02-	£.≱I I€	7.36-12-	ø.82 16	2.74-61-	ZQ:15
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8.71:A	7.261	8.888	46.3	1.0462	7.6I 66	1.02-81-	8.81 ee	9.41-91-	9.22 66	6.32-71-	19:52
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Ø.32:₽	9.961	9.148	4.74	1.0456	102 6.4	5.64-71-	102 2.8		T.T S@I	Ø.33-91-	77:6I
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6.62:4	£.661	8.84E	8.84	1.0458	9.84 40.	4.0E-TI-	104 41.5	-18-25.1	104 45.5	1.86-81-	18:38
4:31.5	I.002	321.1	2.64	1.0469	6.0 aar	2.32-71-	Ø:69 9ØI		106 2.6	6.&E-8I-	19:35
4.28:4	2.002	354.3	3.64	1.0429	4.TI TQI	T.22-TI-	T. 31 TØI		0.el 701	4.82-81-	18:28
7.28:4	9.002	3.738	7.6A	69 <b>†</b> ذI	3.88 30.5	<b>6.22-71-</b>	108 32.0	3.71-81-	9.38 8@I	9.82-81-	19:24
4.32.4	2.002	T.Q	9.64	1°0426	4.64 eqi	8.32-71-	1.84 eq1		8.03 eq1	3.16-31-	78:5®
4:31.5	7.661	<b>6.</b> 8	4.64	1.0458	111 5.6	8.18-71-	4.4 111		6.8 III	1.78-81-	91:61
Ø. ØE: 4	9.8er	1.7	1.64	1.0457	112 22.3	3.68-71-	2112 211.3		112 23.4	4.34-81-	19:15
8.72:4	ε. 761	10.2	8.84	1.0456	8.68 811	₱:09-7I-	0.68 EII	7.44-81-	8.04 811	18-56.4	8 :61
4:25.1	9.361	E.EI	6.74	1.0454	114 58.5	2.4-81-	114 58.Ø	<b>4.83-81-</b>	114 69.3	8. QI-71-	₱ :6T
7.12:4	7.861	£.8I	Ø. Y₽	1.0452	8.81 311	8.02-81-	9.81 911	6.4I-6I-	E. 61 811	1.72-71-	Ø :61
8.71:4	<b>7.191</b>	2.91	Ø.84	1.0450	0.14 TII	9.04-81-	8.14 TII	3.48-61-	8.14 TII	0.74-71-	18:56
4:13.3	6.88I	ø.ss	8.44	TAAO. I	8.8 911	9.8- 61-	3.8 911		9.3 ell	1.01-81-	18:25
2.8 :4	2.881	7.42	43.5	1.0443	7.88 8SI	Ø.0E-e1-	12Ø 34.9	7.62-02-	120 33.0	8.88-81-	18:48
4: 2.5	2.881	4.72	Ø. 24	0440.I	122 6.3	Z.0- 02-	122 7.2	8.63-62-	122 4.Ø	6.8- 91-	18:44
3:56.3	1.081	6.62	£.04	1.0435	123 41.4	4.48-82-	123 44.3	1.82-12-	123 39.4	E.14-91-	ØÞ:81
3.64:8	7.971	32.4	4.88	1640.1	125 23.2	-21-13.3	125 27.1	0.T- SS-	125 20.2	-20-20.2	18:36
3:42.1	173.2	7.48	36.4	1.0425	127 12.Ø	2.73-12-	2.71 721	-22-61.2	7.7 721	-21 -4.3	18:32
8.48:E	₽.69I	1.78	1.48	6140.1	129 9.5	7.74-22-	3.81 621	9.14-62-	7.8 621	-21-54.4	18:28
3:25.3	165.4	4.68	31.5	1.0412	131 18'2	-23-45.3	7.72 181	-24-39.5	9. QI ISI	-22-51.7	18:24
3:15.8	1.191	8.14	8.82	7040°I	133 42.6	9.23-42-	133 64.9	-25-46.9	6.18 EEI	6.73-62-	78:20
3: 6.4	126.4	2.44	4.82	4680.I	136 28.1	-26-10.9	136 44.9	0. T- T2-	136 13.3	7.51-52-	91:81
2:53.6	151.2	8.84	21.5	£850.1	I.84 98I	2.74-72-	1.01 041	7.34-82-	139 25.Ø	-26-50.1	18:15
8.68:2	6.441	6.64	7.81	6980.I	9.1 441	-29-62.8	8.68 441	3.83-8£-	143 28.4	-28-51.3	8 :81
0.12:2	2.881	64.3	3.6	1.0346	15ø 43.4	7.8- ££-	9.31 231	9.36-46-	149 32.4	9.13-16-	18: 4
4.0 :S	126.2	6.63	ø. ø	8150.1	ŭ.33 631	1.72-78-	£.8 &a1	▶.SI-8E-	7.8E 081	1.7- 78-	LIMITS
YTIJATOT	HIDIW	Z∀	ΤÄΑ	OITAЯ	LONGITUDE	<b>EATITUDE</b>	BOUTIONO.	1 BOUTITAL	LONGITUDE	I BULITAL	JMIT
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# ORIGINAL PAGE IS OF POOR QUALITY

Table 59

ANNULAR SOLAR ECLIPSE OF 26 DEC 2019

7.4 :8	8.891	245.2	ø.ø	Ø996'Ø	1.82-931-	18 42.3	8.1- 731-	7.6 81	-166-30.5	6.8E e1	LIMITS
									T.07 747	7'0 CT	<b>79:9</b>
4.11:5	161.2	6.0A2	7.9I	9696'Ø	8.7- S41-		3.73-141-		-142-20.1		
3:15.4	7.841	6.882	9.42	9196.0	6.1- 8£1-	8.72 6	7.63-381-	2.44.8	6.4- 8EI-		84:9
3:18.8	138.5	8.782	3.08	1886.0	5.24-151-	1.28 7	9.24-121-	6 62.1	4.24-181-		24:8
		8.352	35.4	548.0	-128-13.5	a. p. a	-128-14.8	8.32.3	-128-12.5	7.E4 8	98:3
3:21.9	134.5				-126-16.5	3,00	1.71-821-		-125-14.Ø	9.18 3	ØE:9
7.42:8	4.ISI	2.482	7.68	£396.0	3 31-301-	8 62 8			7.85-221-		8:24
8.72:8	8,821	4.282	43.5	1996.Q	-122-38.3	3 56.0	-122-39.9		8.41-021-		81:9
7.62:8	1.821	£.&£Z	Ø. TA	6996'Ø	1.81-021-	₽.8 £	8.71-021-				6:15
8.18:8	J25.Ø	Ø.822	2.03	9796.Q	4.3- SII-	£.62 Z	3.8- 811-	1 54.6	E.4- 811-		
8.88:8	123.6	225.3	2.83	Ø896'Ø	4.E- BII-	3.73 I	2.4- 811-	£. EZ I	7.2- 811-		9 : 8
3:35:5	122.4	2.222	8.33	3896. Q	4.8- AII-		7.8- AII-	3.83 Q	2.8- AII-	I.8 S	ø :9
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8.88:8	<b>₽.</b> [2[	218.5	2.83	6896.Q	Ø.81-211-	O'ZT T	8.81-211-	8.98 Q	-112-19.2	I.84 I	<b>2:24</b>
					9.88-011-		Z. EE-QII-		7.48-011-	3.18 I	2:48
1.88:5	120.5	214.4	£. 09	2696. Ø			1.13-801-		-108-63.6		27:9
6.88:5	8.611	9,602	1.29	9696. Ø	-108-52.3	6 67 10			8.31-701-		2:38
3:88:8	2,911	1.402	8.88	8696.Q	3.51-701-		T. II-TaI-				Ø8:3
7.68:8	7.8II	Z.86I	9.49	6696'Ø	7.85-301-		-10E-34.3		1.65-301-		
7.68:8	2.811	7.161	65.3	IQ76.0	5.1- 401-	9.64 Q	-103-58.4	8.71 \@	2.4- 40I-		2:54
5.68:8	8.711	6.48I	9.29	IQT9.0	8.82-201-	1.83 @	-102-23.3	I.72 &	£.&£-2&1-	8.0E I	2:18
	4.7II	1.871	4.39	2079.0	9.23-001-	T'ZT T	8.84-00I-		9.93-001-	9.84 I	21:3
8.88:8					2.81-66-	6.62 I	8.51-99-		7.22-66-		9:9
7.78:E	2.711	3.171	8.48	IQ76.Q			8.78-79-	8.02 I		7. ES 2	ø:s
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9.46:6	Ø.TII	9.631	4.28	6696.0	2.8- 86-			1.61 2	4.88-49-	1.22 E	87:7
3.58:5	S.TII	124.5	9. Ø 9	7696.@	4.72-46-	2.68.5	5.12-46-			3 58.8	24:4
8.18:8	3.711	6.64I	8.83	9696.0	7.34-26-	8.72 E	2.68-26-	2 25.6			98:4
3:29.1	Ø.8II	Ø.34I	5.33	Z696'Ø	Z.@- 16-	6.8 <b>≯</b>	£.£3-\e	E. TE E	1.7- 19-	6.04 A	
3:26.9	8.811	142.5	9.53	8896.0	8.6- 68-	9.83 4	8.2- 68-	7.42 A		8.82 3	4:30
3:24.5	6.611	4.98I	8.03	£836.8	2.81-78-	7.03 3	9.3- 78-	₽.8I 3	8. \S-\\	8. 23.3	42:4
	5.121		8. Y.A	8789. 8	8- 8- 38-	ø. 23 . ø	9.0- 38-	2.61 8	Ø.81-38-	2.32 T	81:4
3:22.0		7.981					0.84-28-	£.82 T	8.0- 58-	8 35.6	4:12
4.91:5	1.821	8.48I	2.44	2786.Q	-82-52.9	8.1 8		2.74 8 5.99 5	8.8E-88-	<b>7.83 6</b>	9:4
7.8I:E	126.4	132.1	<b>4.04</b>	4996.Q	2.62-08-	9.12.6	-80-15.4		9.04-77-	5.05 II	ø:Þ
8.41:E	£.82I	1.081	2.88	9996.Q	8.88-77-	10 64.2	<b>▶.8</b> 2-77-	9.81 QI	O MA-TT-	5 pc 11	D · 7
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1.11:8	0.281	1.821	4.18	9796.0	3.31-47-	0.44 SI	1.6- 47-	12 6.5			3:48
1.8 : 8	6.981	172.9	7.32	1696.Q	0.01-07-	14 69.4	6.3- 07-	2.91 þí	4.81-07-	16 40.3	
₹.4 :€	9.541	123.3	£.8I	Z196.0	6.08-48-	18 2.3	4.88-48-	8.81 TI	6.82-48-	2.64 SI	3:42
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ANNULAR SOLAR ECLIPSE OF 21 JUN 2020

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8:53:8 8:58:8 1: 5:4 1: 1: 5:4	3.75 0.14 6.34 6.03 8.73 8.69	8.772 4.082 6.682 7.382 7.882 8.292	43.6 39.1 34.8 2.82 2.83 2.83	9689.0 7889.0 9789.0 2689.0 4489.0 \$189.0	7.84-III- 2.41-3II- 3.82-82I- 8.82-82I- 8.82-92I- 4.81-95I-	7.28 32 8.8 42 0.01 22 1.78 91	2.24-111- 4.36-6.4 118-56.9 129-10.5 129-39.9	25 23.6 22 63.6 22 Ø.4 19 27.8	1.33-111- 2.2.2.311- 1.19-15.8 4.46.45.1- 5.46.48.1- 1.39-651-	25 41.8 2.1 2.5 7.91 22 4.34 91	%:8 %:8 %:8 %:8 %:8 %:8
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#### Table 61

TOTAL SOLAR ECLIPSE OF 14 DEC 2020

Ø:25.2	E. QE	244.3	ø.ø	8700.1	6.8- II-	1.68-82-	1.21-11-	9.44-62-	8.1- 11-	6.8E-ES-	STIMIL
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3.64:0	9'19	2.832	9.81	1.0135	0.54 8	7.12-18-		2.82-46-	7.05 PI	3.8- 46-	24:71
1: 1.5	7.63	8.832	7, 82	8910.I	0.01 AI	9.81-46-	6.84 EI	0.45-85-	20 16.Ø	9.8- 85-	98:71
8.11:1	<b>62.4</b>	8.682	8.28	3710.1	6.33 er	4.12-86-	4.88 eI		25 10.0	3.68-78-	ØE:71
8.91:1	8.69	2.892	ã.8£	6810.I	24 62.4	37-54.5	24 34.5	4.6- 88-		2.03-85-	42:7I
4.72:I	<b>4.</b> εΥ	1.872	7.24	1.0200	8.81 62	I.7- 98-	8.2 62	8.62-68-	8.48		81:71
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9.04:I	Ø.67	2.882	7. Q3	1.0218	3.31 78	7.74-04-	8.S 7E	4.7- IA-	8.72 78	6.72-04-	
7:48.2	1.18	8.882	5.43	1.0225	4.43 B4.4	4.02-14-	8.64 Q4	2.14-14-	7.4 14	9.69-01-	9 : 71
1:51.2	<b>0.</b> ε8	4.462	8.73	1.0231	7.82 AA	8.84-14-	44 15.2	1.3- 24-	8.18 44	4.12-14-	Ø :71
1:55.6	9.48	8.00£	7. Ø 9	7.520° I	8.44 74	£.73-14-	8.88 TA	8.61-24-	8.03 TA	7.48-14-	10:24
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7:2:2	1.78	315.8	1.88			7.23-14-	I.6 73	42-16.5	8.7 73	6.82-14-	16:36
2: 5:3	1.88	7.428	€.89	1.0248	3.8 T3		0.8 03	Z.I- 24-	8.2 <u>88</u>	5.51-14-	ØE:9T
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7.8 :2	3.68	8.848	9.17	1.0252	1.73 28	4.3I-IA-	8.13 88 63 2.0	I.II-I4-	8. YE 38	7.62-04-	81:91
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2: 1.6	4.68	3.39	1.39	7420.I	4.42 18	<b>4.</b> 63-38-	8.01 18	7.61-86-	8.88 88	1.28-48-	12:38
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#### ANNULAR SOLAR ECLIPSE OF 10 JUN 2021

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2.84:8 0.74:8 7.34:8 0.44:8	0.033 7.233 1.973 4.003	2.028 3.718 7.718 3.918	0.91 3.71 5.31 1.51	0.9425 0.9427 0.9411	1,44-341-	- 8.03 +8 - 8.25 28 - 8.34 97 - 8.04 87	-135 -3.4 -135-48.5 -135-48.9	83 58.8 8.28 18	4.84-781- -161-22.8 -168-28.3 -168-17.3	6,44,67 6,88,87	8:11 91:11 8:11 8:11
8.64:8 1.64:8	633.2 54ø.3	1.41 5.155	21.3 20.3	1849.0 8249.0	4,81 181. 8,81-481.	- 3.73 88	8.71 E E.21-e\[ \]		1.34 731 3.74 971	8.58 38 8.71 48	Ø : II
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7.44:8 3.84:8	7.988 8.818	8.78 7.07	9.81 8.81	0149.0 8149.0	9.98 47 8.42 27	68 58.4 63 25.8	7.78 78 2.38 38	7.84 18 8.3 48	8.84 88 2.18 \text{\text{0}}8	58 49.2 62 4.1	10: 4 10: 8
1.88:8	9.169	6.43	ø.ø	1866.0	8.28 88	7.14 13	3.73 38	ε.6 8₽	<b>4.38 89</b>	3.61 23	STIMIJ
DURATION YTIRAJUNNA	HTA9 HTGIW	Z¥ N∩S	SUN	DIAMETER OITAЯ	ONGITUDE	CENTER	LONGITUDE		LONGITUDE		UNIVERSAL IIME I
59.1.88	= T & J	l e (I									TAI SOAAS

#### TOTAL SOLAR ECLIPSE OF 4 DEC 2021

5e2 3.88	= T st	le(I								;	SAROS 152
DURATION	HTA9	NOS	NUS	DIAMETER	B LINE	CENTE	A LIMIT	SOUTHER!	7 LIMIT	иовтневи	IA 2G3VTUIL
YTIJATOT	HTGIW	ZV	ΤΊΑ	OITAЯ	LONGITUDE	LATITUDE	LONGITUDE	LATITUDE	LONGITUDE	I BOUTITAJ	UNIVERSAL TIME
1:29.9	424.0	5.721	ø.ø	7180.1	8.31 64	0.7- 43-	0.84 £3	1.42-43-	2.73 84	0.43-13-	LIMITS
0.9E:1	450.6	9.0SI	3.7	TEEQ.1	€.88.3	3.83-83-	6.21 13	-66-53.1	0.0 TE	0.32-09-	9 :7
6.14:I	422.8	6.811	9.6	£460.1	4.83 @4	8.13-03-	8.EI 74	1.1- 63-	3.64 36	6.0- 29-	8 :7
2.44:1	452.2	2.711	6.0I	1.0348	8.84 68	@.18-28-	45 26.6	9.4- IS-	8.44.48	9.62-69-	ØI:7
1.46.1	1.034	8.311	12.1	1.0352	3.83 88	8.1- 48-	44 22.5	8.84-28-	3.0 48	2.53-49-	21:7
8.74:1	8.744	9.411	13.1	1.0366	9.82 88	8.82-38-	8.44 64	1.22-48-	33 28.1	1.51-99-	7:14
1:49.2	Ø. 444	9.811	Ø. Þ.Ľ	7350.1	3.9 88	7.74-88-	0.72 EA	8.84-39-	3.8 6.5	I.0E-78-	91:7
1:50.3	9.0pp	8.211	7.41	1.836ø	3.8 8.2	£.3- 89-	4.82 64	▶.@I-T8-	32 55.3	6.44-89-	81:7
1:51.3	S. 784	2.211	15.3	1.0362	9.EI 8E	Z. \\ \\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	6.14 EA	1 00-09-	30 64 6	2 23 08	20°2
1:52.2	8.884	8.111	15.8	£980.1	9:98 88	8.28-07-	9.17 44	I.82-88-	3.43 26	7.73-68-	82:7
1:52.9	7.0E4	3.111	2.81	1.0364	39 12.8	3.54-17-	45 2.2	2,24-68- 1,43-07-	33 4.5	0.6- 17-	22:7
1:53.4	7.724	9.111	9.91	1.0365	£.3 @4	4.23-27-	<b>7</b> .6 97	0.5- 27-	33 26.5	8.81-27-	42:7
1:53.8	425.0	<b>6.111</b>	8.81	9980.I	8.81 IA	<b>▶</b> .63-£7-	E. 7E 7A	2.6- 57-	34 2.8 34 53.1	3.72-87- 0.38-47-	82:7 82:7
1:54.1	422.5	9.211	۵.71	7980.1	3.64 24	8.4- 87-	6.82 64	7.21-47-	7.2 8E	E.14-37-	82:7 82:7
1:64.3	£.\\\\	7.811	۵.71	7980.1	2.84 44	8. T- 8T-	1.84 13	2.51-37-	6.48 TE	E.84-87-	98:7 7:32
1:64.3	4.814	115.3	۵.71	7980.1	I.8I 74	8.8- TT-	1.68 43	Z.@I-97-	2.38 98	8.64-77-	≯8: <i>1</i>
1:64.2	8,814	3.711	۵.71	7980.1	6.32 <b>0</b> 3	8.3- 87-	4.7 83	8.2- TT-	6.01 24	9.13-87-	98:Y
1:53.9	412.5	150.5	8.81	3980.1	9.61 43	3.63-87-	1.81 29	2.03-77-	8.18 34	9.03-67-	86:7
1:53.5	414.6	124.4	8.81	1.ø366	ø.8 63	1.84-67-	1 91 78	A 16-97-	, 53 0	0 07 20	W 7 * L
1:53.Ø	8.514	129,3	5.91	3980.1	9.63 49	8.62-88-	I.8I 78 7.8 87	8.18-87-	4.03 94	2.84-88-	Ø4:7
1:52.4	413.4	138.4	6.31	£850.1	4.63 17	-81 -2.4	8.88 <b>6</b> 7	8.8- 97- 2.32-97-	5.22.28 62.23.4	8.85-18-	24:7 AA:7
1:51.6	4.814	142.6	15.4	1.0362	9.8 \@8	-81-23.2	6:13 98	4.48-67-		Z. 02-28-	44:7
1:50.6	8.814	120.6	8.41	Ø98Ø.1	<b>4.33 88</b>	-81-29.5	9.92 46	9.82-67-	8.4 IT 9.91 I8	8.21-68-	84:7 84:7
3.64:1	9.414	128.8	1.41	1.0358	I.4 86	Ø. 61-18-	102 Ø.Ø	1.8- 67-	7.88 26	9.41-68-	Ø9:1
1.84:1	416.6	8.881	13.3	1.0355	106 52.4	2.03-08-	4.6 60I	9.42-8Y-	103 45.2	9.93-28-	Z3:7
1:48.5	6.814	8.571	12.3	1.0352	3.84 AII	₽.2- @8-	7.38 3II	1.62-77-	113 63.Ø	9:81-28-	<b>≯</b> 9∶∠
3.44:1	7.814	8.671	1.11	1.0348	121 33.9	0.33-87-	8.8 121	8.83-37-	122 21.ø	2.12-18-	7:56
1:45.3	7.02A	184.4	9.6	1.0344	9.I 72I	0.82-TT-	125 34.9	6.33-67-	129 1.4	7.3- Ø8-	7:58
1 .30 E	0 667	8 781	8 L	1 0338	9 61 181	7E 00 3	0 77 001	0 00 02			
3.98:1	6.224	8.781	8.T	8880.1	131 12.6	-75-29.3	Z.44 82I	0.0E-07-	9.2 4EI	2.18-87-	ø :8
6.62:I	451.2	I.0eI	ø.ø	8150.1	134 33.6	Ø.⊅3-83-	128 56.3	1.88-78-	2.88 881	3.6- 78-	STIMIL

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2 62.3 178 45.1

#### Table 64

#### ANN/TOT SOLAR ECLIPSE OF 20 APR 2023

										,	
TI.1 :0	ø°T	8.082	4.11	1,0003	9.62-071-	8.68 ₽	Z.6Z-07I-	9.65 A	0.08-071-	Ø.6£ ₽	<b>₽9:9</b>
	a.sr	8.882	9.12	Z800.I	7.44-181-		8.14-131-	Z 9T 9	9.74-ISI-	7.6 3	2:48
T0.41:0			2.82	0300.I	6.61-931-		Ø.81-831-		-166-23.9		2+:9
T4.82:0	19.3	288.3			9.11-231-		2.7- 231-		9.91-291-		98:3
TE.IE:@	6.42	7.082	8.88	1.0065					0.63-841-		Ø8:3
TS.88:0	8.62	4.182	<b>≯.</b> 8£	8700.I	8.74-841-		-148-42.3				2:24
T4.44:0	8.88	282.5	8,24	9800.I	-146-52.7		7,84-34 <u>1</u> -		9.83-341-		
T0.03:0	a. TE	Ø.482	4.84	3600.1	8.81-6+1-	8.22 2	6.21-641-		-143-25.3		2:18
IQ.33:0	6.68	Ø.882	8.64	Z@IØ.I	0.1- I+I-	1.72 1	0.43-041-	1 32°6	0.8- I4I-	₽.8I I	21:3
14.63:0	8.24	4.882	6.23	8øīø:ī	-138-22'8	T.TS &	4.84-8EI-	8.8£ @	2.E- 9EI-	9.81 Q	9:9
TE.E : I	5.44	4.162	8.33	AIIQ.I	8.8- TEI-	8.48-0	8.23-981-	6.32-0	₽.8- \EI-	8.44-Q	ø : 9
TC C . r	6 77	, 100	0 23	,,,,,							
1010 17	6.34	6.462	4.83	8110.1	9.61-361-	4.14-1-	-132 -2.5	8.18-1-	7.12-351-	6.03-1-	<b>4:64</b>
T8.8 : I			7.03	SZIØ.I	2.88-881-		8.42-221-		9.14-221-		87:7
T3.9 : I	1.74	2.662			1.83-181-		4.64-151-		7.8- SEI-		74:4
T8.11:1	1.84	3.408	8.28	1.0125					1.85-051-		4:36
T3.81:1	7.8 <del>4</del>	a.aie	8.49	8210.I	E.72-021-		4.81-0£1-				4:30
10.31:1	1.94	3.818	3.39	aeta.t	7.63-821-		8.03-821-		7.8- 621-		
16.31:1	Z.6₽	7.828	8.39	ieio.i	7.48-721-		9.32-721-		T.84-T2I-		4:24
12.81:1	1.64	8.IEE	7.88	7.Ø132	2.11-821-		0.2- 821-	£.3− e−	-126-20.3		81:4
12.81:1	6.84	Ø.688	8.88	7:132	-124-48.5	6.68-01-	6.68-421-	1.08-01-	9.73-421-	8.64-01-	4:15
19.31:1	4.84	7.848	ø. 99	ZEIØ.I	-123-25.7		7.81-521-	7.73-11-	8.46-621-	1.71-21-	9:4
18.41:1	7.74	8.838	6.48	ieio.i	-122 -2.2		2.53-121-		-122-11.1	E. 74-EI-	ø:Þ
Ta Ar.r	2 20	0 636	0 , 0		• • • • • • • • • • • • • • • • • • • •		• • •				
1710717	6.84	9.Q	9.69	ØEIØ.I	8.8E-@ZI-	T'TT-GT-	0.82-021-	9'T- 9T-	9.34-021-	9.02-31-	3:24
TS.81:1		7.8 a.n	9.19	8210.I	7.8- ell-		0.0 eli-		8.71-911-		3:48
TE.II:I	6.34				8.8E-7II-		2.82-711-		9.44-7II-		37:8
Te.8 :1	7.44	12.2	3.63	1.0125			1.13-311-		2.Y- 8II-		3:38
Tf.8 :f	6.54	2.71	ø. Ta	1.0122	-116-59.2						3:30
18.2 :I	7.14	9.IS	5.43	7110.1	8.41-411-		1.7- 411-		-114-22.4		3:24
TI.63:@	8.68	7.32	51.3	ZIIØ.I	-112-21.3		1.41-211-		-112-28.4		
16.43:Q	9.YE	9.62	Ø.84	T@I@.I	8.31-011-		2.6- WII-		5.22-@11-		3:18
II.03:0	1.36	2.EE	44.4	øøīø.ī	3.43-701-	2.63-72-	8.84-701-	0.13-72-	5.0- 801-		3:12
18.44:Q	3.28	6.88	40.5	I600'I	7.11-301-	7.81-08-	7.8- 301-	6.3- &£-	7.81-301-	-30-21.5	3:6
T7.88:0	7.82	8.04	1.88	1800.1	7.83-101-	1.68-28-	9.43-101-	8.18-28-	9.2- 2@I-	4.84-28-	ø : e
17 96.0	2 00	0 2,									
10.10.4	24.5	7.44	ø.18	6900°T	ø. ø 86-	2.91-38-	£.73-79-	-36-12.5	7.2- 88-	8.32-36-	5:24
T8.15:0			Ø. 52	1.0054	7.44-29-	8. IZ-8E-	8.54-26-	0.81-88-		E.72-8E-	2:48
T7.82:0	1.61	3.64		Z E Ø Ø . I	I.84-48-	8.8- S4-	0.74-48-	7.2- 24-	2.84-48-		24:2
TE.EI:@	3.11	2.83	6.91	1 0030	1 91-10-	8 8- CV-	W ZV-VO-	Z 0 0V	0 37 70	. 3 21 07	0, 0
			~ . ~	000010	0:05.00	0.02-0-	0:74-00-	1.62-84-	8.04-58-	1.02-0#-	STIMIL
2.8 :Q	2.8	4.27	ø.ø	£866.8	6.64-69-	8 80-81-	8.11-68-	1 00-81-	8 01-68-	Z 30-01	STIUT I
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							,		3.60 ( TD) :03	74017197	TWTI
YTIAAJUNNA	MIDTH	Z∀	TJA	OITAЯ	LONGITUDE	<b>EATITUDE</b>	LONGITUDE	AGUTITAJ	LONGITUDE	aditttA I	
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281'2

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6966'Ø

1.84 871 8.33 2

SAR05 134

ANNULAR SOLAR ECLIPSE OF 14 OCT 2023

#### 7able 66

#### TOTAL SOLAR ECLIPSE OF 8 APR 2024

2: 4.5	142.1	<b>≯.</b> 182	ø.ø	68£0.1	3.5 Q	2.68 74	8.1 \QS	I.0 74	19 26.4	4.81 84	LIMITS
I.44:S	7.831	<b>⊅.</b> 632	£.61	6440.I	4.12 T	7 1'69 8 <del>7</del>	48 11.2	8.51 84	46 25.Ø	2.44 e4	8 <b>†</b> :61
1.2.5	6.49I	8.03Z	I.YS	8740.I	3.24 75		1.4 83	3.71 74	8.71 73	2.43 84 2 AA QA	74:9I
3:31:5	3.691	242.6	33.2	0640.I	2.11.2		7.91 39	8.I 84	6.8 3.5	0.04 TA	98:61
7.82:8	£. £7.1	£.862	8.88	1.0503	7.8 17		I.0 I7	3.85 44	8.6 17	8.41 84 8 84 74	98:6I
£.6£:£	3.971	230.5	8.24	1.0515	2.83 57	43 63.8	4.44 27	43 5.8			
3.84:5	£.97I	225.1	6.8 <sub>4</sub>	1.0525	E.8 Q8		8.84 eT	43 E 0	Ø.11 87	44 42.2	19:24
3:56.7	8.181	8.912	7.03	1.8533	1.14 68			7.18 IA	8, 25 \@8	£.8 EA	81:61
7.8 : 4	1.481	2.412	2.43	1.0540	8.64 88		1.81 88	4.33 es	7.3 48	9.72 IA	19:15
8.6 :4	2.881	6.80Z	8.73	3450.I	9.75 98		6.02 88	8.71 88	3.81 78	9. 74 9E	9 :61
8 6 . 1	0 981	0 800	£ 73	8730 L	0 28 08	8 6.22 78	6.3 68	1.68 88	6.6 <b>0</b> 6	<b>ω.</b> Υ 8ε	Ø :61
Ø.3I:4	1.881	6.S&S	2.09	1.0551	<b>4.</b> 6 26		6.48 IE	8.63 48	1.44 26	36 25.3	<b>78∶2</b> ₹
2.91:4	6.68I	₽.861	8.29	1.0222	3.72 46	34 1.5	6.03 66	33 2Ø.Ø	8.4.3	34 43.3	18:48
4:22.6	9.191	1.681	1.39	1.0659	8.48 86	32 20.2	3°99 96	8.68 18	1.81 79	6.0 EE	18:42
4:25.2	1.591	ø.181	Ø. 73	1990'1	7.28 86	7.88 &E	9. E3 Te	2,63 62	7.21 ee	8.81 IE	18:38
Ø.72:4	9.46I	a.str	3.89	1.0563	8.82 00	Z8 26.8 1	6.24 66	28 18.4	6.4 IQI	3.38.62	Ø8:8I
6.72: <i>₽</i>	Ø:96I	162.2	<b>7.69</b>	1.0565	1.6 26	1 8. PI 72	E. 72 IQI		102 61.2	2.23 72	18:24
4:28.2	£.791	6.131	8.69	1.0565	2.03 56		8.7 EQT	24 55.6	1.88 401	2.6 92	81:81
8.72:4	3.861	141.5	9,69	1.0565	1.82 30		184 44.8	23 13.6	7.11 801	24 25.6	18:12
4:26.3	9.66I	9. IEI	6.89	3990.I	I.4 76			1.18 12		8. I 4 SS	18: 6
4:24.3	9.002	122.6	8.78	1.0563	£.68 80		0.33 TOI	9.74 eI	0.42 90I	I.73 02	ø :81
						_					
4:21.5	201.5	7.411	8.39	1.0561	8.41 QI		0.08 eqi	0.4 8I	11Ø 69.9	19 12.Ø	17:64
Ø.8I:4	ZøZ.I	e. Tar	8.69	6990.I	8.13 11		8.8 III		8.78 SII	1.82 71	84:71
7.81:4	8. S&S	102.2	2.18	1.0555	9.18 EI		0.84 SII	3.68 ≱1	3.71 411	£. 65 31	24:71
7.8 :4	7.202	4.79	4.83	1330.1	12 1E.E			15 48'E	8.1 911	13 61.3	98:71
e.s : 4	4.202	4.86	5.33	1.0545	3,3 71		116 19.2	Ø.83 ØI	117 62.2	8.1 21	Ø8:71
3:56.3	201.5	I.0e	6.13	1.0539	4.E 9I		7.81 811	9.7 e	9'09 6II	9'ØI ØI	17:24
3:48.8	I.002	8.78	€.84	1.0532	2.21 12.2	I 5.84 7	120 24.9	1.31 7	121 69.9	2.71 8	81:71
8.04:8	8.791	82.1	8.44	1.0523	23 35.4	2 20.6 1	122 47.5	8.61 3	124 24.0	6.82 a	21:71
9.0E:E	9.4eI	8.88	8.68	1.0513	7.81 82	3 61.1 1		3 21.0	127 8.3	Ø.12 4	9:71
7.91:E	Ø'Ø6T	ø.28	Ø.38	1.0500	9. ØE 62	I 46.8 I		Þ.YI I	13Ø 22.Ø	ğ. 91 Z	ø :Zī
6.8 :E	7.88I	Ø.18	29.3	1.0485		1 9.42-0	132 33.5	Z.83-0	134 51.5	3.5 Q	18:24
2:13:2	8.47I	9. <b>0</b> 8	2.22	1940.I	1.64 86		5.64 TEI	-3-15.2	8.44 981	6.12-2-	76:48
8.82:2	1.091	Ø.18	8.11	1.0432	Ø.38 7₽	1 6.24-3-	1.8 841	8.4- 8-	7.01 eal	9.22-3-	16:42
8.8 :2	144.3	82.3	ø.ø	96£0.1	3.71 83	I E.84-7-	1.71 831	3.72-8-	1.04 831	6.11-T-	STIMIJ
LITTVIO		70	1714	OTIM	740 : 77:						
NOITARUQ YTIJATOT	HTA9 HTGIW	Z¥ N∩S	SUN	DIAMETER OITAR	AGITTION	LATITUDE LO	LONGITUDE	LATITUDE	LONGITUDE	<b>BOUTITAL</b>	
MOTTAGLIA	пт∧а	NI IS	(A) 12	GETEN	コハエコ	CENTER	I TWITT A	VIZ.LL 000	1 714177	VITU 1 VIOL	UNIVERSAL
					DIAT I	ロコエルヨン	N LIMIT	93HTI IO2	N LIMIT	AHTANN	
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6:33.9	332.2	2.482	ø.ø	1616.0	à.e4 7£	1.88-94-	3.82 88	-5ø-58.2	4.18 TE	1.2- 84-	STIMIJ
6.8 :8	9.40E	Ž84.3	3.7 <u>1</u>	8.9233	4.IE S3	8.41-64-	Z.88 @9	1.64-03-	7.33 89	4.84-74-	\$8:38
9.22:8	Ø. 462	1.882	9.42	1329.8	8.8 27	5.23-74-	3.62 17	6.22-64-	Ø. 38. ST	-48-25.1	50:24
8.88:8	8.882	7.662	9. å£	4926.0	78 62.3	9.0Z-97-	6.84 87	5.34-74-	78 62.2	1.83-44-	81:0Z
6:42.1	Ø.182	5.305 7.000	35.4	4729.8	8.8 48	-44-45.3	4.91 48	1.3- 84-	83 48.2	3.72-84-	ZQ:15
7.64:8	8.872	3.015	9.68	2829.8	6.9I 88	7.8- 54-	8.84 88	6.52-44-	9.13 78	1.33-14-	9 : ØZ
£.83:8 7 01.8	8.872	3.418	43.5	0826.8	9. 63. 6	7.18-14-	1.62 26	6.24-24-	2.71 19	0.22-04-	2Ø: Ø
6.I :7	1.072	2.918	Ø. 74	9676.0	9.83 46	6.43-68-	<b>4.85</b> 39	£.2- <u>1</u> 4-	9.41 46	8.84-85-	18:61
8.8 :7	7. 732	3.828	£. <u>8</u> 3	1089.0	9.35.79	9.81-86-	4.22 8e	9.22-68-	9.64 96	9.31-78-	8 <b>&gt;</b> :6I
Ø.11:7	8.532	9.728	5.53	9059.0	9.93 66	8.24-86-	1.84 001	6.54-75-	I.7 66	7.24-3E-	79:45
8. AI: 7	4.482	332.5	1.93	Ø159.8	102 2.2	8.7- 3£-	1.43 S&1	Ø.8- 86-	E. QI IQI	I.@I-48-	19:38
8. TI: T	5.532	5.755	7.83	4159.8	183 55.6	1.55-55-	104 50.0	1.62-48-	7.1 EQI	0.88-28-	Ø8:61
0.02:7	5.282	342.5	1.18	7159.8	9.88 3&r	5.63-15-	8.45 80I	2.83-28-	104 43.6		19:24
8.22:7 8.82:7	2.282	348.1	2.89	8289.8 7150.8	8.81 T&1	1.82-85-	0.11 801	0.81-18-	E. TI BOI		81:61
				2226.8 8020 R	0.24 801	4.83-82-	I.04 90I	7.84-62-	3.44 TOI		71:61
3.52:7	2.292	£.43E	7.88 1.88			E.12-72-	3.5 111	1.01-82-	Z.8 <u>eat</u>		9:61
9.42:7	2.292	2.1		6266.0		8.64-32-	2.22 211	2.75-82-	110 23.5		Ø :61
2.32:7	2.632	8.8	6.79	8.9325	111 22.5	A 61-30-		0 20 00			
7:22:6	264.3	6.8I	8.83	9286.0	9.88 211	-24-18.3	E. TE EII	8.4- 32-	E. TE III		78:2 <del>4</del>
4.25:7	7.392	25.4	€.69	9226. Ø	113 48.6	4.74-22-	3.64 411	0.88-82-	112 48.5		18:48
6.42:7	4.78S	3.4.2	€.69	9326. Ø	114 68.4	8.81-12-	116 69.9	7.1- 22-	8.73 EII		18:42
I.42:7	3.692	7.24	9.89	9226. Ø	6.8 SII	£.84-61-	Ø.6 711	7.0E-02-	9.3 311		18:38
Ø.82:7	9.17S	8. Q3	1.88	9326 Ø.9325	0.31 TII	Ø. 81-81-	7.71 811	Ø.03-81-	1.61 311	0.66-71-	Ø8:8I
3.12:7	7.472	1.83	6.88	\$289.0	118 23.3	8.34-31-	9.82 911	9.62-71-	7.02 TII	0.6- 81-	18:24
7.91:7	8.772	7.48	6.39	2259.8	3.28 911	9.31-31-	9.88 QZI	2.63-31-	2.62 811	9.28-41-	81:81
3.71:7	1.182	4.07	63.5	8289.8	120 43.5	2.34-61-	121 48.4	-14-28.9	4.98 eli	-13 -2.5	18:15
9. AI: 7	8.482	8.87	4.13	7189.8	1.73 121	9.41-21-	123 2.9	-15-28'2	128 62.1	8.16-11-	9 :81
Ø.21:7	8.882	3.67	ø. 63	3159.8	123 14.1	8.64-01-	124 21.1	0.82-11-	2.8 521	8.0- QI-	Ø :81
7.8 :T	9.262	1.88	3.83	1159.Q	124 35.8	9-12-6-	125 44.Ø	2.73-6-	7.82 821	8.82-8-	17:54
6.4 :Y	7.862	2.88	7.83	7889.8	126 3.4	7.04-7-	8.EI 721	ø.82-8-	124 64.9	<b>7.83-8-</b>	84:71
Ţ. Ø : Ţ	8.008	7.88	7.03	2089.0	3.88 721	I.8- 8-	8.64 821	6.43-8-	126 28.3	1.62-3-	24:71
6:22:9	9.40£	6.8e	3.74	7629.8	8.82 est	7.48-4-	130 36.5	8.12-3-	Ø.11 821	8.84-6-	98:7I
8.03:8	8.888	9.26	Ø. 44	1626.8	8.61 151	2.0- E-	132 36.Ø	4.84-6-	£:9 ØET	1.51-2-	Ø8:71
3.44:8	312.4	Ø. 46	2.04	₽826.0	7.28 881	1.42-1-	134 52.2	7.51-2-	132 15.Ø	8.3E-Q	17:24
7.75:8	315.7	1.36	8. 9£	8729.8	2.7 881	8.EI Q	3.18 781	2.78-Q	134 46.4	9.E I	81:71
7.62:8	8.818	8.36	E. 1E	3926.8	0.51 9EI	1 64.5	2.44 &41	8. I I	0.34 TEI	8.34 2	17:12
E. \\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	3.128	2.86	7.32	8.9263 3869.8	7.7 541	1.65 8	144 61.Ø	7.44 2	9.62 141		9:71
E.8 : 3	3.4.4		9.81	7829.8 5300.8	148 35.3	ø.18 3	Ø. 74 Ø31	1.35 4	146 35.3		Ø : ZI
8 8 .8	P PGE	1.86	9 81	7500 B	140 25 3	2 1 2	D 27 D31	. 20 /	V 20 0/.	0 20 0	
7.65:3	8.155	I.4e	ø. ø	Z616.0	164 56.8	<b>4.</b> 61 8	165 52.8	7.23 8	165 5.3	6.64 6	CIMITS
	5										
YTIRAJUNNA	HTGIW	Z∀	TJA	OITAR	LONGITUDE	LATITUDE	<b>TONGITUDE</b>	<b>AUTITAL</b>	BOUTIONS	L ATITUDE L	NNIVERSAL TIME
DURATION	HTA9	NUS	NUS	DIAMETER	B LINE	CENTE	N LIMIT	SOUTHER	LIMIT	иовтневи	HOGSKINI

#### ANNULAR SOLAR ECLIPSE OF 17 FEB 2026

8.61:2	<b>₽.</b> 287	264.5	ø.ø	9096.0	6.84-46-	-51-26.1	£.81-201-	63-32.ø	9.62-96-	3.0£-74-	STIMIL
4.91:2	7.557	6.192	ø.e	ZZ96.0	6.63-78-	6.4- 88-	9.82-86-	6.13-43-	I.7- 28-	Z.0Z-83-	12:28
4.9I:S	716.5	1.592	9.9	\$296.8	8.8- 78-	8.11-73-	2.84-36-	8.62-83-	3.25-18-	8.22-73-	12:28
2:19.4	2.669	2.482	3.01	9296.8	3.16-88-	6.81-83-	2.72-46-	4.04-73-	6.3- I8-	7.42-83-	12:24
4.91:2	8.288	265.1	I'II	7299.8	9.8- 88-	7.02-69-	0.04-59-	2.13-83-	8.84-88-	0.82-93-	12:22
2:19.5	ø.788	ø.882	3.11	8296.8	1.88-88-	7.82-09-	3.31-86-	7.83-63-	8.48-88-	1.72-08-	12:28
2:19.6	8.238	9.882	8.11	6296.0	3.63-38-	2.82-19-	ø.e- se-	Ø.4- 18-	6.82-08-	1.82-19-	12:18
8.91:2	2.048	2.782	12.1	Ø£96. Ø	T.Q- 88-	2.82-28-	8.81-66-	8.7- 28-	9.0E-08-	@.ez-29-	15:16
2:19.6	1.629	9.792	2.21	Ø£96.@	1.81-88-	6,62-69-	9.44-66-	4.0I-E8-	9.68-08-	1.08-89-	12:14
7.91:2	8.619	8.782	12.3	Ø£96. Ø	4.84-88-	4.18-48-	9.82-46-	8.11-48-	9.83-08-	2.18-48-	15:15
7.91:2	1.218	6.782	2.21	Ø£96.@	7.82-78 <b>-</b>	-62-35.8	9.82-36-	-65-12.Ø	-81-22.3	9.28-39-	15:10
8.91:2	2.909	8.732	12.1	6296.Q	T.@2-88-	6.88-88-	Ø.74-86-	Ø.11-88-	1.83-18-	8.48-38-	17: 8
2:19.9	S.209	₽.Y82	6.II	8296.Q	3.0E-68-	8.4E-78-	2.16-86-	2.8- Ta-	7.34-28-	2.86-78-	15: 6
Ø.02:2	2,009	7.882	9.11	7236.@	Ø:69-Ø6-	-68-35.1	7.44-00I-	6.2- 88-	8.34-68-	£.8E-89-	15: 4
1.02:2	2.009	9.392	1.11	9296.0	I.03-29-1	7.4E-68-	9.35-501-	6.63-89-	9.2- 38-	3.04-69-	15: 5
2.82:2	7.20a	1,482	9.0I	4296.Q	£.6- 36-	9.SE-&T-	3.41-701-	6.88-69-	8.86-88-	8.24-0T-	12: Ø
8.02:2	6.T0a	Ø.292	6.6	2296.0	7.E- 86-	8.82-17-	6.3- 211-	8.21-07-	<b>4.</b> 68-88-	8.44-17-	11:28
4.02:2	616.5	2.632	1.6	0296.0	3.61-43.5	1.12-27-	3.41-611-	7.01-07-	8.01-16-	8.34-27-	11:28
8.02:2	<b>4.117</b>	8.862	ø.ø	£096.0	8.31-721-	8.08-87-	£.e- 821-	T.3- 69-	0.14-441-	0.33-ET-	LIMITS
DURATION YTIAAJUNNA	HTA9 HTGIW	Z¥ N∩S	SUN T⊒A	DIAMETER RATIO	LONGITUDE	BOUTITAL	LONGITUDE	<b>EQUTITAL</b>	LONGITUDE	LATITUDE	TIME
HULLIGHU	112.40	1413	14113	G313/1410	S LINE	CENTE	N LIMIT	SOUTHER	N LIMIT	язнтяои	UNIVERSAL
97.5 Sec	= T st	Вe		07/7	מו זג וכם	70 17727 NV	ANG NINTONIN			1	SAROS 121

TOTAL SOLAR ECLIPSE OF 12 AUG 2026

2.48:1	2,392	8.882	ø.ø	60E0.1	4.71-4-	6.73	38	8.48-4-	6.8E 7E	-8-22.5	6.68 68	STIMIL
2: 8: 2 2: 1: 8 2: 1: 8 1: 49: 8	3.718 3.918 3.818 3.818 3.838	267.5 278.6 273.6 273.1 281.8	0.12 2.91 1.01 1.4.1	1760.1 6360.1 6360.1 7860.1	6.9 71 1.1 61 1.1 63.4 5.63.6 4.63 6	13.2 18.8	46 68 48 58 48	0.81 6 0.84 71 0.92 31 0.81 9	2.77 68 2.77 64 69.8 7.8 49.2	1.4 32.1 12 33.1 10 6.0 11 61.1 1 41.0	52 22.0 50 15.6 48 2.7 45 37.4 42 41.0	18:15 18:26 18:26 18:28
4.31:2 2:13.6 2:11:3	3.708 8.118 8.418	268.8 261.6 264.5	24.5 23.6 22.4	2850.1 9750.1 8750.1	9.92 I2 8.21 82 9.44.9	2.7 8.01 8.21	99	23 69.6 22 38.8 21 10.3	7.74 73 2.83 33 2.83 83	8.23 81 9.78 71 8.21 81	58 24.4 56 25.Ø 54 24.5	18: Ø 18: 4 18: 8
6.13: 6.33: 7.2. 7.2. 7.2. 7.2. 7.2. 7.2. 7.2. 7.2. 7.2. 7.2. 7.2. 7.2. 7.2. 7.2. 7.2. 7.2. 7.2. 7.2. 7.2. 7.2. 7.2. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3. 7.3.	273.9 277.5 277.5 277.5 277.5 289.1 289.1 289.1 289.1 289.1 289.1 289.1 289.1 289.1 289.1 289.1 289.1 289.1 289.1 289.1 289.1	6.1.2.2.2.3.3.4.1.3.4.2.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3		446 1.03564 1.0376 1.0379 1.0379 1.0386 1.0386 1.0386 1.0386 1.0386 1.0386	2. 25. 25. 25. 25. 25. 25. 25. 25. 25. 2	2.6.0 1.01 1.9 1.9 23.6 28.9 22.5 11.5	78 88 77 77 77 27	0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 - 0.5 -	7.7 88 7.7 88 8.81 48 8.81 48 7.84 87 7.84 87 7.84 87 7.84 87 7.84 87 7.85 80 8.75 80 8.75 80 8.75 10	2.83 – 101 – 8.84 2.83 – 101 – 8.87 2.82 – 8.97 2.13 – 8.97 2.14 – 8.97 2.15 – 8.97 2.16 – 8.97 2.17 – 8.97 2.18 – 8.97 2.19 – 8.97 2.10 –	2. 184 2. 184 2. 184 3. 186 3.	21:28 17:58 17:46 17:36 17:36 17:36 17:36 17:28 17:16 17:17 17:17 17:17
1:35.9	<b>₽.</b> 692	6.T	ø. ø	\$160.1	2.8- 111-	8.1	97	2.61-811-	5.43 AT	8.73-801-		STIMIL
NOTTARUQ YTIJATOT	HTA9 HTGIW	Z¥ N∩S	NUS TJA	DIAMETER OITAR	LONGITUDE		TAJ	LONGITUDE		LONGITUDE		UNIVERSAL TIME
5e2 <b>0.88</b>	= T st	l e d		070	. 504 77 10	<b></b>		/700 <b>7</b> 1/101			:	2 <b>4</b> R05 126

#### Table 70

Delta T = 88.5 Sec

#### ANNULAR SOLAR ECLIPSE OF 6 FEB 2027

7.44:3	8.73£	7.492	ø.ø	7410.0	2.61-6-	3.5 8	4.28-4-	4.24 ¢	8.8- 8-	8.98 T	STIMIJ
0.7.0	1.035	223.6	9. <b>≯</b> I	2816.0	4.8 6	3.58 I	8.23 3	1 11.6	11.45.1	r:r z	84:71
6.4:8		9.532	1.62	8029.0	6.18 31	9.84-1-	13 23.5	<u> 7. 12-2-</u>	7.18 71	8.8- I-	24:71
9.81:8	7.448				1.84 91	0.42-4-	2.73 TI	8.6- 3-	21 29.9	4.44-8-	38:71
ø.62:9	8.688	7.452	4.62	7126.0			0.82 I2	3.42-7-	8. 85 42	9.2- 9-	Ø8:71
6.78; a	8.488	8.332	34.5	8226.0	23 1.3	4.84-8-			8. 01 T2	E.9- 8-	17:24
6.45.9	9.628	1.732	ø.6ε	7829.0	25 42.2	Ø.13-8-	24 10.6	1.88-9-		• •	81:71
8:53.2	9.428	8.832	1.54	4426.0	4.0 82 i	-10-50.3	7,88 32	0.55-II-	8.42 62	1.8- QI-	
Ø. Ø3: 8	9.0ZE	7.09Z	6.94	1926.0	7.2 ØE	-12-43.3	7.6£ 82	9.82-21-	31 23.5	3.0- 2I-	21:71
£.8 :7	312.2	Ø. E92	£. Ø3	9326.0	31 23°4	8.18-Þ1-	4.88 &8	1.31-31-	4.II EE	0.84-81-	8 : 71
2.21:7	9. Ø18	265.6	9.63	1926.0	33 36.5	1.31-91-	8. TI SE	3.63-81-	8.13 48	2.16-31-	Ø : 7.£
	2.808	7.832	9.93	9926.0	3.11 38	+:99-71-	7.33 EE	9.04-81-	98 25.Ø	6. QT-71-	18:54
7.71:7			4.63	6926.8	3.24 88	7.25-21-	35 28.6	9.81-02-	37 54.3	4.74-81-	3 <b>⊁</b> ∶9T
7:22.9	302.1	8.272		2729.8 0320.8	9.9 88	2.7- I2-	9.73 88	21-53.9	4.02 gg	1.12-02-	16:42
T. TS: T	4.862	3.872	1.29				38 24.9	9.82-E2-	3.44 04	-21-62.3	16:36
2.28:7	6.462	281.3	9.49	3729.0	4.38 ee	5.98-22-			4.7 S4	1.12-52-	ØE:9T
£.8E:7	8.162	1.782	T.88	TT20.0	7.63 @4	2.6- 42-	9.03 68	8.73-42-			16:24
Ø. Ø4 : T	1.682	8.862	T.88	9729.Q	7.82 SA	Q. 78-32-	Ø. 81 IA	7.82-82-	Ø. ØE E4	7.74-42-	16:18
5.54:7	7.88S	9.10E	E. &T	Ø826.Ø	1.84 64	8.S <del>-</del> 7S-	6.14 SA	8.63-72-	44 63.1	2.21-82-	
£.84:7	7.482	9. ØIE	3.17	1826.0	42 13.9	7.82-82-	1.9 44	1.91-92-	3.71 84	8.48-72-	16:12
7.84:T	Ø. £82	3.028	£.27	1826.0	7.14 84	7.84-62-	45 38.4	8.54-0E-	8.64 TA	-28-55.3	9 :91
7.03:7	7.182	3.188	9.27	1829.8	48 12.3	8.8- IE-	T. QI TA	3.4- 26-	8.21 64	6.81-88-	ø :9ī
7:52.2	7.082	9.24E	4.27	1826.0	9.84 eA	8.72-2E-	7.84 84	9.42-88-	1.34 03	3.08-18-	12:24
2.83:7	I.082	3.238	7.17	Ø826. Ø	61 25.Ø	8.54-55-	Z. 72 \ \textit{0}3	6.24-42-9	62 21.6	-32-42.2	12:48
		8.2 3.036	9. QT	9729.8	7.8 53	2.83-46-	5. 13.3	5.63-35-	8.8 A3	7.73-66-	72:4S
3.53:7	7.972	2.II 5.0		7729.8	4.88 43	8.01-86-	8.8 4.8	8.51-75-	1.03 33	Ø.8- 36-	12:38
7:53:7	8.672		ø.69		6.88.88	7.02-75-	8.8 88	1.82-85-	6. £4 <u>73</u>	0.81-8E-	7E:30
7:52.3	1.082	1.61	1.78	3729.0				6.35-65-	£.34 63	4. IS-78-	16:24
T.03:T	8.082	2.92	Ø:99	£729.0	E.0 63	5.82-88-	5.41 83		6.36.18	0.42-8E-	12:18
4.84:7	8.182	7.28	8,58	0729.0	7.41 I3	2.88-98-	E.EE @9	1.84-04-	8.81 48	3.52-95-	12:15
7:45.2	2.882	8.88	ø. øə	8926. Q	8.68 89	6.48-04-	8.8 88	2.74-14-			12:0
8.I4:7	6.482	1,44	1.73	£926.0	4. TI 88	1.88-14-	£. 7. 38	8.74-24-	8.74 88	4.61-04-	Ø :31
8.88:7	1.782	€.64	5.43	8326.Q	£.6 69	2.72-24-	3.84 88	2.44-64-	7.SE 69	2.11-14-	6 .31
Ø.18:7	7.682	4.43	ø:19	£326.0	6.71 27	4.81-64-	8.8 27	9.35-44-	2.88 ST	-41-28.3	14:24
	2.262	4.63	3. <u>7</u> 4	7429.8	0.84 37	8.63-64-	76 42.4	0.12-34-	8.13 37	7.68-24-	14:48
4.42:7			9.54	Ø+29.8	3.78 97	0.85-44-	3.84 67	6.83-34-	8.15 eT	5.41-54-	74:42
Ø. TI: T	9.962	3.48		2629. à	8.73 £8	2.8- 34-	9.12 48	8.72-84-	Ø.88 88	E. 04-E4-	14:38
4.8 :T	S. I ØE	7.69	6.68			8.81-34-	7.75 68	1.54-84-	2.71 88	43-55.4	14:30
7.83:8	7.8QE	75.1	32'4	Ø.9223	0.43 88				8. 84 £6	7.33-64-	14:24
8.74:8	3.818	Ø.18	4.0E	Ø.9212	9.68 46	-46-18.2	6.84 36	6.14-84-		I.48-84-	81:41
8.48:8	$\epsilon.sse$	3.78	24.5	6616.Q	e.ee igi	2.83-44-	103 26.9	9.11-84-	8.6 ØØI		14:12
Ø.81:8	3.488	9.36	7.81	0816.0	p.p III	8.14-64-	0.6 AII	4.44-44-	7.38 8@I	<b>9.</b> ££-2≱-	21.11
Ø.84:3	9.09£	7.eat	ø.a	9519. à	1.64 QE1	3.41-66-	8.81 SEI	0.28-01-	E. SI QEI	6.8E-TE-	STIMIL
YTIAAJUNNA	MIDTH	Z∀	TJA .	OITAR	ONGITUDE	I BOUTITAL	EQUTIONO.	I BOUTITAL	ONGITUDE.	LATITUDE L	UNIVERSAL TIME
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TOTAL SOLAR ECLIPSE OF 2 AUG 2027

8.3 :6	<b>≯.3</b> 02	1.882	ø.ø	1.0602	<b>4.4</b> 2-06-	-12-28.4	8.8- @e-	2.12-21-	1.43-06-	<b>▶.</b> 68-11-	LIMITS
3:52.1	<b>≯.</b> 622	6.0es	9.61	399ø°I	2.08-87-	-6-21.3	0.81-27-	-6-52.2	6.74-47-	T170 4	
4:13.9	<b>≯.8</b> 82	2.162	8.72	8698.I	8.88-78-	9.23-1-	8.32-33- 8.31-07-	6.72-2~	8.78-88-	1.23-4-	11:42
4.18:4	244.4	6.062	2.48	8070.I	6.51-59-	I.83 Q	7.21-28-	4.02 Q		4.8I-I-	11:36
9.84:4	7.842	Z.8e2	7.68	8270.I	6.84-63-	3.82.5	7.64-83-	I.94 S	7.81-48-	1 35.0	## : 11
1.0 :3	8.132	2.682	5.44	3870.1 5070 I	0.33-33-				4.64-08-	2.7 4	11:24
ē: īš: š	254.1	Ø.882	I.94			4.34 B	2.73-33-	3.4 3	0.43-73-	7.32 8	81:11
5:23.5	8.332			3470.1	6.12-43-	3.23 T	-63-26.1	E. QI T	7.61-33-	1.48 8	11:15
9.88:3	0.732 9.330	2.982	53.3	1.0754	4.8- 28-	6.13 6	3.7- 13-	4.8 6	E.0- E3-	8.48 QI	9:11
8 66.3	Ø 730	9.482	2.73	1970.1	6.33-64-	9.44 II	2.0- e4-	2.0 11	-5ø-51.4	12 29.2	ø:II
7.24:3	8.732	2,282	Ø.13	897@.I	8.43-74-	13 32.6	3.0- TA-	7.84 SI	I.03-84-	1.81 14	10:64
Ø:19:9	258.3	8,672	9.49	ETT0.1	7.63-34-	12 12.6	1.8- 84-	14 28.4	1.48-84-1	16 2.4	87:0I
5:83:3	9.832	7.372	6.78	8770.I	2.8- 44-	16 64.4	-43-12.6	ø. 8 e. ø	7.1- 34-	3,24 TI	79:42
8.4:8	8.832	Ø.172	2.17	1.0782	6.81-24-	₽.62 8I	2.72-14-	7.68 TI	-43-11.5	6.81 er	98:91
8. NI: 3	8.832	7.482	2.47	3870.1	7.0E-04-	8.0 QZ	0.04-ee-	8.6 er	-41-22.2	9.13 QZ	ØE:ØI
6.11:8	9.832	\$28.8	Ø.TT	7870.1	4.24-88-	8.82 12	0.83-78-	4.88 \QZ	9.28-98-	1.12 22	10:24
8:18.5	228.4	8,642	4.67	6870.I	-36-53.1	22 53.6	Ø.3- 88-	8.63 12	9.14-78-	E. 74 ES	81:01
1.12:8	Z28°I	7.322	Ø.18	0670.I	6.I- 36-	24 15.2	-34-16.4	83 28.8	1.64-35-	25 18.3	71:01
7.22:8	7.732	8.202	9. IS	0670.1	8.7- 55-	8. EE 32	1.52-25-	8.78 42	2.83-88-	2. 85 32	9:01
8:23:8	1.732	7.671	6.08	0670.I	I. ŠI-IE-	7.84 82	£.72-8£-	8.63 32	-31-53.3	8.84 YZ	9 : ØI
							_	0 23 30	6 63 16-	8 8V 70	10.01
7.22:8	2.832	4.131	1.67	6870.I	T.T- 62-	3.0 8S	£.72-82-	2.1 T2	9.84-62-	6'69 8Z	<b>†9:6</b>
8:21.Ø	8.332	148.3	9.87	<b>7870.1</b>	7.63-82-	8.8 62	0.22-82-	2.8 82	8.78-72-	9.6 ØE	87:6
1.81:8	224.9	8.881	8.57	3870.I	-24-42.2	3.EI &E	4.01-42-	9.11 es	-26-20.2	31 15.5	24:6
1.41:8	8.632	9.181	T. &T	2870.I	1.62-22-	3.41 16	7.13-12-	I.II QE	9.43-22-	4.71 SE	9:38
8.8:8	8.232	125.8	4.78	8770.I	1.23-61-	32 10.5	-19-24.6	3.8 18	9.6I-02-	6. ÞI EE	Ø8:6
2.2 :8	2.132	120.8	Ø. 49	ETTO.I	8. QI-7I-	33 2.2	3.74-81-	2. 73 ££	9.88-71-	4.7 48	₽Z:6
5:54.4	9.642	8.911	4.09	8970.I	7.71-41-	33 48.4	1.63-81-	7.24 SE	7.35-41-	34 64.4	81:6
5:45.3	8.742	112.1	9.93	1970. I	7.01-11-	34 28.6	4.73-01-	33 22.4	9.82-11-	0.35 35	
6.48:3	7.345	1.801	7.23	£370.1	E. 74-7-	35 1.6	6.65-7-	33 55.4	£. £3-7-	36 8.1 1.3	9:12
Ø.52:3	243.3	1.401	3.84	3470.1	I.A- A-	35 26.3	4,8- 4-	8. \( \omega \). \( \omega \)	I.E- 4-		9:6
					. , ,	2 90 30		34 28 3	1 E- A-	3.28 88	ø :6
9.6 :9	8.012	1,001	6.5≯	AETÒ.I	4.8 @	7.04 3E	ε.ε- α	34 36.4	4.SI Q	36 46.Ø	8:24
4:54.6	4.782	6.36	Ø.68	1.Ø725	4 45.6	35 42.Ø	2.72 A	3.88 48	9.0 3	36 45.8	8+:8
3.78:A	8.882	<b>⊅</b> .16	4.88	T@T@.I	ø:9 øt	35 25.6	7.68 6	34 24.2	6.88 QI	8.82 88	24:8
3.71:4	8.822	3.88	8.82	889Ø.I	16 35.2	34 42.8	3.83 BI	33 45.4	2.81 TI	3.68 38	8:36
3:52.5	1,222	3. Ø8	2.81	Z990.I	1.91 32	33 10.2	24 18.8	92 Z8.9	26 26.9	3.73 88	Ø8:8
									0 00 00	7 77 66	DC.0
ã.8 ∶£	8.305	0.07	ø.ø	£090.1	44 18.3	1.83 72	43 56.5	0.8 TS	7.13 AA	7.84 8S	LIMITS
YTIJATOT	MIDTH	Z∀	TJA	OITAR	LONGITUDE	PAULTING	LONGITUDE	PAULING	7/01/701/07	7001711	====
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Table 72

#### ANNULAR SOLAR ECLIPSE OF 26 JAN 2028

τ.ι :۲	3.65.5	8.442	ø.ø	9706.0	1.61-1-	8.41 04	1.13-2-	1.63 88	₽.SS-I-	0.8 SA	LIMITS
1 1 · L		• • • •							£.82	₽. 9E TE	16:54
<b>≯</b> .82:7	320.4	Z. 7. E. Z.	9,11	ZØ16.Ø	8.61 NI	8° 18° 8	9.88 QI	8.02 88		8.82 28	16:48
2.64:7	8.855	4.182	1.12	9716'Ø	18 4E.2	3.64 QE	8.71 8I	6.8 62	6.9 61	2.85 82	ZÞ: 9I
	9.25E	7.722	27.5	Ø+16.8	8. E4 E2	3.62 T2	7.2 ES	2.4 82	24 19.9		16:36
8.8 :8		7.422	32.56	1316.0	8.22 T2	3.64 42.5	Ø.88 82	8.62 £2	ø. 8 8 S	26 12.1	
8:11:8	8.72E		I.75	Ø916.Ø	3.71 ØE	6.62 22	29 28.3	0. pr 12	3I E.3	2.84 62	J6:38
8:32.4	3,828	Ø.222	[,[4	8919.0	32 45.0	20 24.4	31 E4.0	E. II 91	0.38 EE	7.68 IS	16:24
8.74:8	3.026	4.912			34 63.1	7.62 8I	9. I 48	17 18.6	35 44.3	8.24 er	81:91
3.63:8	<b>6.716</b>	8.812	7.44	3719.0		4.84 81 7 00 01	3.43 35	7.88 31	8.68 TE	17 54.9	16:12
4.01:6	1.915	1.412	Ø.84	1816.0	6.84 88	2.4 3I	I.78 78	13 55.6	3.22 98	3. 41. 8I	9 : 9 T
8.82:e	314.8	2.112	Ø.13	9816.0	1.08 88		8.21 9g	12 23.2	6.73 84	1.04 41	ø :9I
3.0E:6	314.Ø	I.8@2	8.63	Ø616.0	40 5.2	1.18 81	30 10 0	2 60 01	0 23 27		
							0105 05	10 ee.8	9.82 St	13 12.4	12:2 <del>4</del>
7.68:6	313.6	7.402	4.83	\$616.B	6.88 I₽	12 3.3	8.04 04		4.03 64	I.64 II	12:48
2.84:9	7.818	8.002	8.83	8616.Q	8.73 24	10 40.2	6.4 24	8.28 6	4.01 34	10 30 4	72:4Z
2.83:9	314.1	9.961	6. Ø 9	ØØZ6.Ø	0.81 AA	8.12 e	43 25.3	9.81 8		8.31 9	12:38
10:3.4	9.418	7.191	7.29	£026.0	45 35.4	<b>4.</b> 8 8	0.84 44	7.83 à	3.72 84		72:30
	1.915	186.3	5.48	9026.0	6 09 97	2.33 8	42 28.9	I.74 3	8.24 74	ø.3 8	16:24
Ø.01:01		4.08I	3.39	9026.0	1.3 84	3.74 B	8.EI TA	7.8£ 4	4.83 84	Ø.83 8	
10:15.8	9.716		4.39	7029.0	7.81 64	1.84 4	8.72 84	8.EE E	9.6 Ø3	P. 43 3	12:18
1.02:01	319.4	6,87 <u>1</u>	6.99	8029.0	58 32.4	3.42.Ø	Ø. 24 64	2 31.6	27.2	2.43 A	12:12
10:24.8	4.128	1.791	-	8029.0	3.84 13	2.44.2	6.83 &3	1 32.5	Ø.88 23	8.73 E	12: 8
8.72:@£	8.828	1.091	Ø. 78			2.64 I	62 12.8	3.88 Q	9.03 63	7.ε ε	Ø :9T
8.62:01	9.325	163.2	T.88	8026.0	7.1 E3	CONF	0 01 03	2 00 2	• ••		
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9.08:01	8.828	9.94£	Ø.88	T029.0	9.81 43	8.73 Q		E.8- I-	56 24.6	Z.82 I	14:48
10:30.3	7.088	3.041	ø.39	9026.0	3.78 33	I.6 Ø	4.03 43		4.84 78	42.4 Ø 42.4	74:42
18:28.6	9.288	Ø'981	8.69	9026.0	2.63 83	S.88-@	1.81 88	Ø: 63-I-	4.6 63	ø.s. ø	14:38
10:25.6	9.3EE	130.2	6.13	£026.0	£. <b>₽</b> 2 83	1.81-1-	2.68 73	4.88-2-		8.48-Q	74:30
2.12:01	8.866	Ø. 921	6.63	TØZ6'Ø	6.63 63	<b>⊅</b> '99-I-	<b>₽.</b> 6 63	4.81-6-	4.78 &a	9.7- I-	14:24
	338.4	122.4	7.73	8616.0	2.72 18	1.18-2-	3.44 Q9	7.23-6-	62 10.2		14:18
10:12:3	8.688	4.9II	2.23	9616'Ø	6.8 68	8.I- E-	62 25.5	0.32-4-	7.84 £8	6.8E-I-	
Ø.8 : Ø£		6.9II	5.23	1616.0	64 53.5	1.82-8-	4.81 48	ø.£3-≱-	1.48 38	3.1- 2-	14:12
2.63:6	340.6		9.64	8819.8	£.84 83	3.64-8-	9.6 99	-2-18:3	6. TS T8	2.12-2-	74: 8
Ø.64:6	341.3	9.4II			6.83.3	9.8- 4-	8.31 89	I.46-3-	6.1E 69	-2-35.3	74: Q
2.78:6	8.148	2.811	4.84	1816.Q	60 63 3		0 11 00				
					C'AT T	2.31-4-	3.48 QT	7.34-3-	7.84 IT	6.24-2-	<b>13∶2</b> ∢
6.23.9	3,248	6.III	Ø. E4	3719.0	6. QT T7		I.9 ET	7.64-3-	7.4 22.1	7.24-2-	13:48
I'6 :6	7.248	6.0II	39.2	8916.0	7. 44 ET	1.71-4-		4.44-8-	8.71 77	4.28-2-	13:42
8:52.5	343.3	I'ØII	1.35	Ø916. Ø	0.04 8T	4.6- A-	7.4 8T		8.34 08	8.8- 2-	13:38
I.4E:8	3.44.5	9.60I	E.QE	Ø316. Ø	0.8 \\	8.81-5-	6.62 67	7.82-8-	8.3 38 8.3 50	-1-23.9	73:30
8:13.Ø	3.848	Z.601	7.42	7819.@	8. \QZ \p8	8.8- £-	8. 04 E8	8.03-4-		7.1 Q	13:24
3.74:7	3.03E	I.ear	4.71	Ø216'Ø	Z. ØI Ø6	@.63-1-	ø.81 68	8.24-6-	8.EI 19	2 1 10	70-01
A TA.T	סבש ב	. 0								~ L	SLIWIT
1.63:3	3.638	8.801	ø.ø	Ø8Ø6. Ø	8.64 401	3.62 S	102 20.6	2.8 I	3.6 30r	Q.12 4	STINI I
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5e2 4.68	= T 6J	Del									
5,00				870	2 NAL 32 7	'R ECLIPSE O	A JOS SAJUNI	<b>1</b> ▼			

#### TOTAL SOLAR ECLIPSE OF 22 JUL 2028

8.28:2	7.191	ø.eøe	ø.ø	1240.1	1.73-671- 2.31-03-	4.83 eTI @.11-13-	4.73 871 8.13-64-	STIMI
				LILAT	4.63-031- 8.16-04-	4.42-181- 8.84-14-	I.14-031- 7.81-68-	4:15
3:16.7	Ø. TTI	1.818	8.71	4740.1	2.03-431- 9.82-38-	4.13-481- 4.38-78-	6.13-436 -164-61.9	9:7
3:35:5	7.88I	7.525	7.42	3640.1	6.88-831- 9.12-88-	8.52-831- 8.52-45-	3.14-031- 3.12-28-	Ø:Þ
3:61.4	2.681	1.828	6.62	6030.1	9 ME-MAI- 9 10-55-	9 00 931 0 00 70	3 1, 231 2 10 CC	- '
ĭ.3 :4	1.461	3.288	3.48	1230.1	7.3- TAI- 8.34-08-	1.13-841- 8.44-18-	3.12-741- 1.74-62-	3:64
Ø. 71:4	9.89I	1.888	9.75	1.053Ø	9.21-441- 8.82-82-	8.43-541- 6.82-62-	I.28-441- 0.28-72-	84:8
8.72:4	8.202	1.048	1.14	1.8537	8.14-141- 8.72-82-	8.02-I4I- 4.42-TS-	2.6-31.2 -142 -3.2	3:42
0.75:4 3.75:4	6.88S	344.1	43.9	1.0544	8.32-981- 3.78-42-	4.2- 981- 0.48-82-	7.84-621- 9.14-62-	3:36
2.34:4 4:45.2	9.0IZ	348.4	2.84	6430.I	7.91-781- 4.73-22-	-23-53.6 -136-55.4	4.44-781- Q.S- SS-	9::8
		352.8	2.84	1.0553	9.12-25.5 -135-21.9	-22-21.6 -134-56.6	8.74-381- S.08-02-	3:24
4:52.2	7.412		6.94	1.0558	7.62-881- 0.1- 02-	3.6- 881- I.73-02-	1.83-881- 8.3- 91-	3:18
4:58.1	218.4	3.738		8880.1 8330 r	5.14-151- 1.54-81-	3.41-151- 5.65-61-	2.8- 281- 3.74-71-	3:12
6:2:9	8.222	5.3	1.13		8.33-921- 2.12-71-	0.82-621- 8.72-81-	-16-35.4 -130-22.6	3:6
4.8 :3	2.822	4. T	Ø.23	1.056ø	£ 93-001- 0 16 21	8.24-721- 8.12-71-	0.85-821- 0.62-31-	ø : E
7.8 :3	2.822	12.5	8.23	1.0560	▶.@I-82I- I.32-3I-	8 07 101 0 10 11	2 00 001 2 00 11	
			1.70	J.056Ø	-16-24.6 -126-25.6	7.73-321- 3.12-81-	4.63-821 -1284-63.4	5:24
8.6 :3	7.0ES	7.71	7.23		8.65-421- 8.62-41-	8.11-421- 8.82-31-	7.7- 321- 8.28-81-	2:48
9.6 :3	7.282	8.22	52.4	699Ø.1	9.13-221- 5.96-61-	8.52-221- 0.72-41-	8.61-521- 4.24-21-	25:42
ø.8 :3	9.882	8.72	8.13	1.0558		7.28-\021- 9.23-EI-	8.82-121- 7.73-11-	2:38
5: 5.1	4.462	8.28	7.03	1.0555	9.0- I2I- I.33-2I-	8.78-811- 4.41-81-	3.55-911- 3.81-11-	Z:30
8. Ø : 3	Ø.462	1.78	€.64	1.0662	-12-16.3 -119 -5.6		1.25-711- 4.34-41-	2:24
4:22:1	232.5	2,14	3.74	1.0548	3.4- TII- 4.84-II-	0.85-311- 8.14-21-	1.42-311- 8.81-01-	81:2
6.74:4	Ø. Ø£2	Ø.34	4.34	1.0543	11-16.9 -114-56.1	6.72-11-6.11-27-3	4.8- 511- 9.83-9-	2:12
2.98:4	4.822	48.5	6.24	1.0537	0.85-111- 3.73-01-	9.8- 211- 4.83-11-	6.85-011- 8.74-9-	2:6
1.62:4	9.122	9.13	Ø. Ø4	1.0229	8.T- QII- I.84-QI-	7.78-60I- S.34-II-		ø : Z
8.71:4	7.312	9.43	3.38	1°0250	7.02-T01- E.44-Q1-	3.64-801- 8.54-11-	8.03-T01- E.34-9-	6.6
				araa: T	6.0I-40I- 8.43-0I-	8.78-801- 3.43-II-	9-24-101- 2.33-6-	7:24
8.8 :4	7.802	Ø. 73	7.SE	0190:1	2.72-001- 2.12-11-	8.44-99- 0.22-21-	5.2- 101- 0.12-01-	1:48
3:48.1	200.5	4.63	1.82	7640.I	2 72-881- 2 12-11	8.0- 36- 0.81-EI-	3.82-86- 0.11-11-	1:45
3.62:8	7.0e1	7.13	4.22	0840.I	4.84-36- 1.81-12-	0.74-78- I.8- 3I-	2.2- 86- 4.84-21-	1:36
3: 5.4	8.771	8.43	4.41	1.ø455	0.63-88- 6.83-£1-	0 ZV-Z8- 1 0 31	8 8 20 7 07 07	
4.62:2	1.831	<b>≯</b> .89	ø.ø	1140.1	3.01-87- 2.41-81-	3.64-37- 0.8- e1-	0.36-37- T.14-71-	STIMIJ
YTIJATOT	WIDTH	Z∀	TJA	DITAR	LATITUDE LONGITUDE	LATITUDE LONGITUDE	AUTITUDE LONGITUDE	UNIVERSAL TIME
DURATION	HTA9	NNS	NNS	DIAMETER		SOUTHERN LIMIT	NORTHERN LIMIT	1100272111
					CENTER LINE	TIMI I MODUTINO	TINI I MODIFICAL	
200 6:00	- I BA	190					•	2AR05 146
5 <del>9</del> 2 6.68	T e.t	140		070	וע ברדדופב חו דג פחד ז	LUIAL SULA		

#### ANNULAR SOLAR ECLIPSE OF 1 JUN 2030

4:12.5	0.548	9.862	ø.ø	₽286.0	-162-53.5	8.1 AE	1.26-32.1	3.72 28	5.63-431-	34 64.1	STIMIJ
4:27.5	8.02£	8.382	12.9	£856.0	I.T- TAI-	41 2.Ø	8.04-641-	6.33 %4	3.31-131-	40 53.2	ø :8
4:35.6	Z.80E	8.672	6.22	6756.0	6.63-661-	9'71 77	<b>8.</b> ≱£-7££-	6.74 EA	9.13-241-		79:7
2.24:4	I.862	P. 872	1.82	1689.0	7.91-481-	2.78 84	5.0- ZEI-	4.0 84	8.44-881-	3.11 TA	84:T
Ø 87 7	3.682	8.782	4.28	IØ≯6.Ø	6.1Z-6ZI-		9.12-721-		2.26-161-	7.41 64	24: T
	2.282	7.132	2.88	6016.0	7.13-421-		2.4- 221-	T'TZ 64	1.84-821-		98:7
4:53:1			4.65	3149.0 0010.0	0.8E-02I-		9.63-811-		-122-20.3		øs:Z
8.73:4	8.372	9.332					1.6-311-		8.2- 8II-	2.06 66	7:24
5: 2.1	A. WTS	8.642	42.4	1249.8	-116-29.3				8.03-511-		81:7
6.3:3	9.392	7.242	Ø.34	9249. Q	2.82-211-		111-12.1				21:7
2.9 :3	9.192	6.362	8.74	Ø£46.@	7.0E-801-		8.42-T@I-		8.24-601-		
5:12:5	228.3	7.822	€.64	££46.0	-104-32°2	EE 14'I	3.68-801-		-102-38.5		9 : 7
8:14.8	2.552	2.122	1.13	9849.Q	6.14-001-	1.74 33	1.83-66-	Ø. E4 43	8.1E-1@1-	1.23 83	Ø :T
6:91:9	263.3	213.4	5.53	8£46.0	g·6+-96-	6.11.83	1.41-96-	7.8 33	2.82-76-	E. 81 73	<b>19:9</b>
9.81:3	221.6	£.3@2	7.83	Ø446.0	-92-58.4	6.82 83	<b>₽.</b> ££-26-	8.22 33	7.32-86-	1.88 73	84:8
8:61:9	7.092	Ø. 791	9.43	I446.0	7.8- 98-	Z.8E 33	<b>5.43-88-</b>	9.18 33	3.42-68-	0.84 TB	8:45
5:20.6	7.642	9.881	2.33	Z446.0	7.02-38-	6.68 83	8.91-38-	5.88 33	1.32-38-	6.74 Ta	98:3
6.82:3	2.642	Ø. Ø81	3.33	8449. Ø	8.48-18-	5.48 83	2.14-18-		Ø.82-18-	I.S4 73	Ø8:9
8.02:3	3.942	4.17I	4.33	2442.8	5.13-77-	56 21.4	9.Y- 8Y-	4.8I 33	8.88-TT-	7.82 Ta	6:24
			I.33	2449.Q	8.0I-4T-	4.I 88	9.85-47-	2.88.43	5.24-57-	8.7 73	81:9
5:20.3	9.032	Ø. E91							5.43-69-	9.68 93	ZI:9
5.21:3	8.132	1.431	4.43	1446.0	8.28-0Y-	<b>55 34.4</b>		2.08 43	8.6- 88-	2.4 83	9:9
6.11:3	8.632	3,841	3.53	9£49.8	ø.83-88-	E. Ø 33	8.24-78-	3.73 83		3.12 33 5 1 93	ø :9
0.81:3	6.832	6.8EI	2.23	7849.Q	6.32-88-	p'61 pg	1.61-48-	1.81 53	9.82-29-	3 10 33	פי ש
8:21:3	7.832	131.5	7.03	9849.Q	Z:99-69 <del>-</del>	53 31.4	9.73-09-	6.18 23	£.03-83-	9.18 43	2:24
1.11:3	Ø. 292	124.5	6.84	8.9432	-56-28.3	5.36.3	9.78-73-	6.88 13	Ø. ÞI-33-	5.48 E3	2:48
Ø 8 : 9	Ø.882	8.711	8.84	8246.8	1.1- 53-	8.88 13	6.71-43-	8.88 03	8.86-13-	2.62 23	2:42
8.4 :8	9. \Q\C	3.111	4.4	4249.Q	5.55-94-	58 23.6	3.73-03-	1.18 94		5.81 18	2:38
		9.3QI	7.14	8149.Q		I.3 94	7.48-74-	48 15.5		9.49 64	Ø8:9
8: Ø:S	6.372		7.88	8149.8		2.78 74	6.8- 44-	6.03 84	I.04-04-	Ø. 52 84	2:54
3.83:4	281.9	6.66								9.98 84	2:18
6.13:4	<b>7.88</b> 2	3.46	35.4	9046.0		45 58.4		1.81 34	8.44-86-	0.24 44	21:3
7.84:4	4.862	2.68	31.5	7689. Q	3.04-4E-	1.8 44	3.04-86-	7.82 E4	2.18-28-		
Ø.Ih:4	3.3&£	1.48	Ø.TS	78£6.@	4.2I-0E-	7.33 IA	£.72-2E-	41 25.Ø	4.34-72-		9:9
4:34.3	315.4	8.87	21.5	4789.0	-24-54.3	4.71 ee	<b>₽.</b> £8-72-	3.73 88	Ø.83-12-	6.1E EE	ø :9
4:25.9	0.82E	6.2T	6.81	3356. Q	7.78-71-	35 41.6	6.E1-12-	9.34 3£	3.6- 61-	7.31 3E	4:24
4:13.4	3.448	1.39	ø.ø	225e.@	1.88-4-	9.34 62	1.83-4-	<b>▶.11.8</b> 2	2.88-2-	1.04 QE	STIMIL
ANNULARITY	HTQIW	Z∀	TJA	OITAЯ	LONGITUDE	LATITUDE	LONGITUDE	LATITUDE	LONGITUDE	BOUTITAL	TIME
NOITARUG	HTA9	NUS	NNS	DIAMETER							UNIVERSAL
	. /				R LINE	CENTE	HIMIT N	RAHTUOS	TIMIL N	HETHER NORTHEF	
oe2 8.19	= T st	Del								8	SAROS 128

#### TOTAL SOLAR ECLIPSE OF 25 NOV 2030

017017	LIGIT	0.012	a.a	T404:T	7'0- TOT-	8.42-82-	6.35-131-	6.14-02-	ø:99-ø91-	0'00-07-	STIMIL
£.28:1	4.811	8.842	ø.ø	IQEQ.I	0 3- 131	8 76-96-	0 30-131-	0 27 30	יובש בפ ש	8 63 30	STIUT I
6.34:1	128.3	9.032	8.8	TSEQ.I	9.89-241-	3.78-62-	6.11-341-	-29-20.5	7.73-041-	<b>4.44-62-</b>	8:24
9.8 :2	4.141	1.832	3.02	3980.1		-34-14.5	-132 -3.5	0.15-45-	-159-68.9	-33-56.5	81:8
1.42:2	1.841	7.882	8.72	9880.1		-36-48.2	9.54-421-		-122-54.2		21:8
2:36.5	7.231	Ø.692	9.55	2040.I		- 38-4Ø.3	6.43-811-		0.9I-7II-		9:8
4.74:2	1.631	8.472 8.932	9.88	3140.1		. 3.7- 04-	2.23-511-			2.48-98-	ø :8
A 74.0	1 931	E ATO	30 8	31MM L	9 9- 511-	3 2 07	113 60 0	, ,,	0 80 011	0 70 00	<b>D</b> -0
0.73:S	128.8	7.672	45.9	1.0425	1.68-801-	2.71-14-	7.71-8 <b>0</b> 1-		0.2- 801-	1.14-04-	7:E4
3: 5.6	6.09I	285.3	6.84	1.0434	4.82-40I-	-42-13.Ø	-106 -2.3	-45-21.2	6:99-801-	8.48-14-	8 <b>7</b> :7
3:13.3	7. <u>2</u> 81	1.162	4.03	Z440.I		-42-57.3	8.0- IQI-	4.7E-E4-	3.6- @@I-	6.81-24-	24:T
3:20.1	2.481	4.792	7.53	8440.I	£.34-86-		8.6- T6-	6.61-44-	6.IZ-86-	9.64-24-	98:7
9.82:E	165.4	3.408	9.83	1.0454		7.83-54-	4.72-E8-		7.84-26-	-43-13.5	Ø8:7
Ø. ΙΕ: Ε	4.88I	3.118	5.63	1.0458	6.85-68-		6.13-68-		9.22-68-		7:24
3:35.3	S. 781	9.918	9. <u>1</u> 9	2940.I	1.21-88-		-86-22.4			1.88-24-	81:7
8.88:8	6.73I	3.828	8.58	4840.I	8.23-28-	1.82-44-	1.82-58-		3.74-28-	8.65-54-	21:7
3.41.1	4.88I	6.758 5.905	1.39	8840.I	7.75-67-	-44-20.5	3.85-97-		1.75-97-	6.48-84-	9:7
7.24:8	6.83I	I.848	5.88	8940.I	8.82-87-	2.6- 44-	1.62-87-	8.43-44-		7.82-84-	ø :Z
7 01.5	0 091	1 016	6 88	0910 1	0 90 92	2 0 11	1 00 02	0 12 11	0 00 02	2 00 07	2
3:64:6	Z.69I	328.9	6.88	89 <b>†</b> ذI	8.61-67-	7.13-64-	4.II-ET-	I.78-44-	8.72-87-	3.8- 64-	6:54
3:43.4	7.69I	8.6	Ø. 78	8940.I	9.31-07-	I.82-£≱-	1.E- QT-	0.51-44-	8.72-&T-	6.64-24-	87:9
3:42.5	4.69I	Y. ØZ	3.88	8940.I	2.41-78-		8.73-99-	7.24-64-	2.0E-78-	-42-14.3	24:8
7.04:E	4.69I	Ø. IE	9.39	9940.I		-42-22.9	6.43-68-	5.8- 54-	7.48-49-	9.68-14-	98:3
1.88:5	2.691	7.04	I.48	4940.I	8. TI-18-		6.83-09-	8.62-24-	7.04-18-	2.63-04-	Ø8:9
3:45:8	6.89I	4.64	5.59	1940.1	1.12-83-	1.48-04-	Ø. 43-73-		5.74-83-	0.5I-04-	42:8
4.08:E	4.88I	£.73	I.03	1.0458	-55-24.5	7.0- QA-	4.43-43-		8.83-33-	6.02-68-	81:9
3:25.4	7.73I	4.48	3.73	1.0453		I.1- 98-	1.43-13-		1.63-23-	7.22-85-	21:9
3:19.5	8.881	8. QT	7.43	8440.I		8.43-75-	7.13-84-	8.18-8E-	6.1- 63-	1.81-75-	9:9
3.11.5	9.391	3.87	3. I3	2440.I	4.82-84- 5.50.01	3.14-88-	7 97-97-	2.81-75-	3.0- TA-	3.8- 88-	ø : 9
0 01.0	8 381	3 92	3 13	CAAR !	7 20 8V	3 17 00	, 2, 2,	0 01 20	3 D 27	_ 0 00	
3: 5.5	1.491	7.18	1.84	1.0434	6.61-64-	-36-2ø.3	6.28-24-	6.23-38-	7.23-64-	8.74-48-	2:24
2.73:2	1.281	<b>4.</b> 88	2.44	1.0426	7.63-66-	-33-6Ø.1	6.01-6E-	-34-20.6	9.38-04-	£.61-EE-	2: <del>1</del> 8
0.84:2	129.5	8.06	0.04	3140.I	0.02-9E-	£.e- 2£-	7.48-38-	1.78-28-	2.4- TE-	6.04-IE-	27:9
7.78:2	1.931	6.46	8.38	5040.I	7.42-28-	7.41-0E-	9.96-16-	8.68-&E-	8.11-66-	5.64-62-	2:38
Ø.82:2	3.131	6.86	8.62	8850.I	7.43-72-	4.1-82-	4.2- T2-	-28-22.5	9.34-82-	3.68-72-	Ø8:9
2:12:2	ğ.34I	8.201	1.62	6980. I	Ø. IZ-22-	7.71-32-	4.12-12-	-25-33.2	7.81-62-	0.1- 32-	2:54
1:53.6	9.EEI	S. Yar	13.4	9550.1	0.3- FI-	7.42-12-	0.14-SI-	6.82-12-	-16-23.6	7.61-12-	2:18
0 03-1	0 001	O LDI	, .,	0000	2 2 7 2	2 70 70	2				
1.18:1	8.811	3.111	ø.a	7620.I	3.13-1-	£.71-81-	<b>▶.</b> 22-1-	E. 04-81-	9.83-1-	0.84-31-	LIMITS
YTIJATOT	WIDTH	Z∀	TJA	OITAR	LONGITUDE	<b>EATITUDE</b>	LONGITUDE	<b>LATITUDE</b>	LONGITUDE	<b>EATITUDE</b>	<b>JMIT</b>
DURATION	HTA9	NOS		DIAMETER							NNINEBSAL
					R LINE	CENTE	TIMIJ N	SOUTHER	N LIMIT	NORTHER	
5 <b>e</b> 8 S.Se	= T st	Del		~~~		70 17707 \	7700 77101			8	SAROS 133

ANNULAR SOLAR ECLIPSE OF 21 MAY 2031

9:53:E	Ø.802	2.062	ø.ø	7846.Q	4.8- @81-	6.88-4-	6.83-621-	9.88-3-	0.2E-0E1-	2.74-8-	LIMITS
							0101 077	0'07 T-	£.31-911-	1.22 B	9:6
7.4 :4	£.361	8.062	3.21	6946. Q	6.0- ell-		8.84-811-				ø :6
9:11:4	Ø.381	8.062	22.3	4646. Q	8.71-111-	2.42	2.3- 111-	1 35.0	Q.IE-III-	2 13 0	<b>D</b> -0
										0100 -	<b>79:8</b>
4:24.1	6.671	7.0eg	6.82	Ø196.0	9.61-8@1-	8. ØĽ Þ	£.8- 8@1-		4.1E-8@I-		
7.15:4	175.3	7.8e2	4.48	8.9622	Z.72-201-	5.92.3	E. 71-201-	4 45.5	8.7E-2@1-		87:8
9.88:4	3.171	Ţ. 062	3.9.2	Z£36.0	9.21-66-	9.0£ 9	6.8- 66-	9.44.5	<b>▶.</b> IS-66-	E. 81 T	Z≯:8
			43.5	1436.0	3.22-96-			1.48 8	Ø.08-86-	8.4 8	98:8
4:42.1	168.4	6.062					2.44-89-	2.41 T	<b>4.83-66-</b>	8.54 8	8:30
1.13:4	165.8	1.162	4.74	6436.0		I.63 7			2.88-19-	9 15.3	8:24
7.83: <i>4</i>	163.5	8.162	1.13	9936.Q		1.18 8	9.92-16-	8.84 T			81:8
6:1:9	9.191	292.3	9.43	1936.0	8.22-68-		<b>⊅.</b> 61-68-	8 12.5		8.04 e	
7.8 :3	Ø. Ø31	8.882	6. Ta	7936.@	T.22-T8-	2.81 6	3.02-78-	8.32.6	~ ~ ~ ~	7.63 6	8:15
Ø:II:9	128'E	9.162	1.13	1736.Q	5.62-38-	6.0E 6	5.82-38-	7.74 8	₽.@£-38-	0.41 QI	9 :8
6:14:9	157.3	4.862	1.48	3736.8	9.14-68-	Ø. I + 6	7.14-E8-	8 28.1	E.I≯-E8-	7.62 @f	ø :8
O AI.A	£ 731	7 300		2230 2	,	<i>D</i> 0					
	01007	6.862	6.88	8736.Q	-81-28.3	6.84 6	7.63-18-	ε.₄ 6	6.83-18-	Z. 62 @I	7:E4
5:18.2	126.3					8.84 6	3.12-08-	3.8 9	4.8I-08-	8.08 QI	84:7
6:21.Ø	122.4	3. S&E	9.69	1836.0	6.81-08-				8.65-87-	10 28.6	7:42
5:23.2	124.6	9.90£	1.27	₱836.@	7.24-87-	6.84 6	4.84-87-	ø:9 6		8.22 \( \text{0.1} \)	98: <u>7</u>
5:24.8	123.9	3.218	5.47	9836.Q	1.6- 77-	3.14 e	<b>6.61-77-</b>	6.63 8			
8:22:3	123.3	7.02E	2.87	7836. @	3.78-37-	9.28 6	4.84-37-	8 21'3	3.16-37-	9. EI QI	Øε: ζ
5.26.2	152.8	1.188	T. TT	8896.0	8.T- AT-	8.02 G	8.41-47-	8.98.3	3.0- AT-	ø.r ør	7:24
8.82:3	152.4	8.44E	3.87	6836.8	8.88-27-	Z.4 €	8.84-27-	I.42 8	9.0E-27-	2.34 6	8I:7
		8.83£	3.87	6836.8	7.01-17-	6.34 8	8.61-17-	9.8	8.I- IT-	I.82 6	21:7
5:25.2	152.1					8.23.8	1.63-63-	7.54 7		T. E 9	9 : L
6.23.3	152.Ø	9.11	8.77	6836.0					I.4- 88-	1.88 8	ø:Z
6:22.Ø	6.131	1.62	3.87	6836.0	-68-15.2	3.83 T	2.82-88-	7.81 T	. 7 00		
					010- 00	0107 /	8.83-99-	Z.03 9	8.46-88-	2.6 8	<b>79:9</b>
9.61:3	162.ø	1.28	8.47	8836.Q	8.84-88-	8.62 T			6.4- 68-	9.88 T	87:9
7.81:3	162.2	ø.e£	72.5	9836.Q	4.71-39-	8.73 8	E.0E-39-	4.81 8			24:8
5:13.4	122.6	2.44	Ø. ØT	4836.0	-63-46.5	2.22 8	6.0- 48-	Ø. 84 3	7.28-89-	2.1 7	
7.9 :3	163.2	I.84	£.78	Z836.@	-62-13.5	Ø. 64 43. Ø	1.82-28-1	Ø.4 3	8.83-13-	6.12.9	98:9
7.3 :3	Ø 121	1.13	9.49	6736. Ø	7.7E-08-	Ø. Ø8 A	T.83-09-	Ø.12 4	1.22-09-	7.8E B	ØE:9
5.1.3	ø.831	3.53	3.18	9739.0	2.83-83-	8.21 4	9.41-63-	6.88 E	8.14-83-	9.13 4	6:24
		5.33	4.83	2739.8	2.41-73-	3 21.3	2.16-73-	2 42.4	Ø. 73-83-	Ø. Ø 4	81:9
4:56.6	126.3				4.42-33-	8.42 2	2.24-33-	8.34 I	4.8- 33-	8.8 8	21:9
7.13:4	6.73 <u>1</u>	8.83	1.33	7936.0					a.8- <u>£3</u> -	2 1.9	9:9
4:46.2	7.631	1.83	7.13	2936.Q	2.72-63-	1 22.9	8.34-63-	7. EA Q			ø : 9
1.14:4	6.131	1.63	Ø.8₽	9996.Q	9.02-13-	9.41 Q	-21-36.6	8.42-@	1.1- 13-	6.83 à	שי ש
											<b>79:9</b>
4:35.5	164.6	ø. øə	1.44	6436.Q	7.1- 64-	ø:I- I-	7.12-6 <b>4</b> -	6.04-I-	6.11-84-	P 10-10	
9.62:4	9.79I	6.09	8.68	I#96.0	1.82-84-	8.32-2-	8.84-84-	ε.8− ε−	0.3- 84-		87:9
4:23.5	8.17 <u>1</u>	7.19	1.35	1836.Q	1.72-54-	9.2- 4-	9.84-64-	7.54-4-	2.3- 64-	-3-21.5	24:3
		8.28	8.62	Ø236. Ø	8.23-68-	7.88-8-	8.41-04-	Ø.88-8-	I.08-68-	7.51-3-	5:36
6.81:4	1.871					9.31-8-	7.65-35-	<b>4.</b> 63-8-	1.43-45-	8.28-T-	Ø8:3
9.6 : h	3.181	7.88	23.3	9036.0	4.71-3E-				3.83-72≥	8.84-01-	2:54
8. Ø : 4	Ø.0er	65.3	4.41	£846.0	7.61-82-	0.88-11-	0.11-82-	1.02-21-	3 83 20	0 01 21	, , _
							1115 07	a.zz	z.7- ar-	7:89-91-	CIWITS
ø.64:8	5.402	7.8a	ø.ø	9446.Q	8,14-31-	8.44-81-	7.74-31-	0.24-71-	0 L- 31-	0 03 31	SIIII I
							= 40 t TD1:0=	70017147	LONGITUDE	PACITIVE	TIME
YTISAJUNNA	MIDTH	Z∀	TJA	OITAЯ	LONGITUDE	LATITUDE	LONGITINE	LATITUDE	ACHITIONO I	adilitita i	UNIVERSAL
DURATION	HTA9	NUS	NUS 5	DIAMETER							IA 203VTIAL
					R LINE	CENTE	N LIMIT	SOUTHER	M LIMIT	NORTHER	
										_	
5e2 7.26	= T sJl	ΘO								8	SAR0S 138
5 2 00	,	-		1802	YAM IS 40	AR ECLIPSE	MMOLAR SOL	A			

Table 77

ANN/TOT SOLAR ECLIPSE OF 14 NOV 2031

9:18.6	6.71	221.5	ø.ø	Ø366. Ø	8. TA 8T	7.02 8	2.84 87	1.71 8	3.34 87	8 26.5	CIMITS
1:91:0	Z. 4.	8.132	3.5	ø966. ø	1.4 28	Z.3I 7	4.21 28	≯.8 T	81 65.2	Z.22 T	87:22
71. <u>2</u> .9	γ. τ	2.49.5	<u>1.</u> er	3000.1	8.48 36	2.54.5	7.48 36	8.83 Z	6.48 36	0.43 S	22:42
16.11:0	2.6	8.842	8.82	9200.1	7. IA IQI	2.8 I	4.14 101	8. <u>8. 1</u>	101 42.0	3.8 I	22:38
I0.02:0	9. Þ.I	1.842	8.28	1400.1	186 12.3	9.I- Q	106 12.0	ğ. 2. 3	7.21 881	ø. 9- ø	82:32
11.72:0	ø.er	8.742 1.919	6.7£	1.0063	7.83 ear	Ø. 23-@	189 53.3	8.84-Q	1.43 601	£.73-0	22:24
13.88:8	22.6	5.842	42.5	£300.1	5.4 EII	8.82-1-	7.8 811	-1-22.3	8.4 811		22:28
T4.68:0	7.82	245.1	3.34 3.01	2700.I	115 53.4	1.88-1-	7.23 311	0.84-I-	0.43 311		21:22
17.44:0	4.82	5,543	4.03 9.34	9700.I	7.82 811	9.51-2-	118 25.8	8.3- S-	3.72 811		8:52
T4.64:0	7.8E	8,142	6.83	3800.I	9.74 02I	5.32-2-	9.84 \QI	6.81-2-	9.84 02I	7.88-2-	Ø : ZZ
				ו שמסב		0 00 0		0 81 0		7 66 0	b . CC
TT. £3: 0	8.28	239.5	1.73	Ø6ØØ.1	122 69.6	1.16-2-	122 58.3	2.22-2-	7.0 ESI	0.04-S-	51:24
T4.73:0	8.48	9.882	1.09	▶600.I	125 3.5	7.18-2-	125 2.1	-2-22.5	15e 4'6	0.14-S-	21:48
T3.0 :I	35.6	Ø. EES	6.29	8600.I	8.1 721	8.72-2-	126 59.7	0.8I-S-		2.78-2-	21:42
TE.E : I	7.88	2.822	4.39	toto.t	128 54.1	1.91-2-	128 52.3	8.8- S-	128 56.Ø		21:38
13.3 :£	3.78	1.622	<b>8.</b> 78	EQIQ.I	130 42.9	3.8- 2-	8.04 QEI	9.83-1-	6.44 BEI		SI:30
TO.7 :I	1.88	4.812	3.69	3010.1	132 28.4	Ø.03-1-	132 26.1	6.6E-I-	7.06 SEI		51:5 <b>₹</b>
TI.8 :I	<b>⊅.8</b> £	9.8 <b>%</b> S	e.ar	9010.1	134 11.5	7.62-1-	0.6 AEI	8.91-1-	134 13.9		21:18
T3.8 :I	38.5	9,661	8.17	aata.t	135 52.7	8.3- I-	138 60.1	7.33-0	132 22.3		51:15
T1:8:1	4.88	ø.øer	1.27	aata.r	7.28 TEI	£.8£-@	0.08 TEI	8.82-Q		4.84-Q	51: 8
T7.7 :1	Ø.8E	2.081	8.17	3010.1	2.21 981	8.7- Q	8.6 <b>6</b> 81	9.2 Q	1.31 981	2.71-0	21: Ø
13.8 :1	3.75	Ø.171	6.0L	polo.1	140 E1.8	4.72 Q	8.84 @4I	I.78 @	140 64.8	T.TI @	50:64
T8.4 :I	7.88	7.291	3.69	I.ØIØ2	142 32.Ø	7.3 I	ã.62 2≯I	1 15.2		Z.83 @	2Ø∶ <b>4</b> 8
18.2 :1	7.38	122.6	T. T8	øøiø.i	144 13.6	8.74 I	144 10.5	0.73 I	7.81 pp1	9.88 I	2Ø:42
T8.63:@	34.5	9.6 <b>&gt;</b> I	9.39	7600.1	145 67.4	8.88 2	146 64.3	8.2 <del>4</del> 2		6.42 S	28:38
Ta.83:@	1.68	7.441	Ø. £8	£600.1	2.44 TAI	8. ES. E	I.IA TAI	4.28 E	2.74 TA1	3 12.4	88:92
Te.S3:@	4.18	140.5	Z. Ø3	6800.I	ø.36 e≯1	4.81 A	1.28 941	4 28.5		£.01 4	₽2:0Z
T8.84:0	3.62	Ø.7ει	2.73	1.0084	1.18 131	7.71 B	151 28.3	6.25.3	121 33'8	1.01 3	SQ:18
TS.44:0	4.72	1.481	6.63	8700.1	123 34.0	6.22.3	163 31.5	<b>⊅</b> .62 8		6.31.8	78:12
TE. 9E: @	6.42	131.5	4.03	1700.1	126 46.9	0.88 T	122 <b>4</b> 3.6	4.68 T		8.82 T	9 : ØZ
T8.88:0	1.22	2.621	7.84	£300.1	158 9.3	8.03 8	£.7 83£	8 56.3	4.11 831	8 45.Ø	20: Ø
Te.72:@	8.81	1.721	45.5	1.0054	160 48.4	8.81 QI	7.84 Ø31	10 21.6	1.03 091	e.ii ai	79:6T
T3.12:0	ø.ar	172.1	Ø.8£	5400.I	0.64 £31	11 23.5	8.74 £31	4.73 II	163 50.4	9.64 II	87:6I
T4.41:0	3.0£	1.821	9.28	QEQQ.I	4.12 Tar	3.44.EI	8.02 Tai	4.74 EI	£.22 781	13 41.8	79:45
T4.8 :0	6.4	Ø.ISI	6.92	4100.1	171 45.2	1.73 31	6.44 ITI	16 58.4		1.88 81	98:6I
2.8 : Q	7.2	2.811	19.2	Z666.@	9.03 TTI	8.84 8I	7.03 TT	0.84 81	9.03 TT1	3.64 8I	Ø8:61
7.91:Q	18.5	112.4	Ø.A	8466.0	2.82-881-	24 22.3	-168-35.4	9.81 42	3.81-881-	2.18 \$2	19:24
9:23:6	7.22	9.0II	ø.0	9866.Q	5.42-24.3	8.84 32	1.12-491-	25 41.3	0.32-431-	1.63 32	STIMIL
YTIAAJUNNA	нтаім	Z∀	TJA	OITAR	LONGITUDE	TAITIONE	LONGITUDE	TOUTING.	LONGITUDE	TOUTIONE	<b>3MIT</b>
DURATION	HTA9	ทักร		DIAMETE	301220110 I		2012201101				ONIVERSAL
					B LINE	CENTE	N FIWIT	SOUTHER	TIMIL N	NORTHER	
93.2 Sec	= T sJ	20								_	LT CONVC
223 6 80	- T 5.41	<b>-</b> 0		T007	. AON 67 10	70 17707 115	700 LOL/NN	,		8	SAROS 14

#### 87 sldaT

#### ANNULAR SOLAR ECLIPSE OF 9 MAY 2032

Delta T = 93.7 Sec

8.24:Q	₽.06	7.208	ø.ø	6686.0	1.2- @8-	6.62-33-	£.82-@£-	£.8- 83-	3.33-08-	0.02-33-	LIMITS
T.8E:Q	2.37	8.118	ε.7	6166.8	6.01-02-	4.42-23-	1.72-12-	8.8- 63-	7.01-61-	4.74-13-	Ø : Þī
01+019	A. QT	314.4	9.6	9266.0	8.73-91-	9.86-13-	1.34-71-	8.8- 23-	Ø.71-81-	6.7- 13-	13:28
8:34:5			£.11	å866. å	9.32-41-	8.4- 13-	4.0- 3I-	Ø.18-13-	-13-22°0	4.04-03-	13:22
7.2E:Q	8.88	6.918				8.14-03-	0.44-21-	7.4- 13-	-11-25.3	9.02-09-	13:24
2.1E:Q	8.89	2.915	7.21	4866.0	0.71-21-				9.2- QI-	Z.8- 03-	73:25
6.62:0	£.13	8.128	13.8	8£66.0	1.62-01-	-50-25.3	-10-45.2	7.34-03-		1.83-94-	73:EQ
8.82:Q	ø:69	2.828	6.4I	1466.0	8.66-8-	9.61-03-	3.83-8-	1.28-03-	4.22-8-		13:48
7.72:0	ø. 73	325.1	1.31	£466.0	7.4- T-	8.3- Q3-	T.&2-T-	T.22-03-	8.64-8-	4.64-64-	
8.82.8	2.23	9.928	18.5	9466.0	7.35-3-	6'Ø- Ø9-	7.64-3-	8.81- <u>0</u> 3-	-2-22.5	7.34-94-	13:46
		7.828	2.71	8466.8	7.11-4-	8.83-64-	1.42-4-	8.EI-03-	Ø.Ø8-£-	3.44-64-	13:44
Ø.82:0	3.53		8.71	6469.8	7.13-2-	2.63-64-	8.2- 6-	-68-13.4	2.14-2-	3.34-64-	73:4S
8.3S:Q	Ø. 23	4.0EE				8.1- Q3-	0.34-I-	<b>≯.3I-03-</b>	-1-26.5	7.84-64-	Ø⊅:€I
8.42:Q	8.03	1.288	£.81	1366.8	0.36-1-	8 1- 83-	מ שור מ	, 31 22	2 20 .		
I.42:0	4.64	7.888	7.81	Z966.@	0.12-0	₽.8- @3-	0.0E-0	9.61-03-	8.21-&	8.63-64-	13:38
	48.3	335.4	1.91	£366.8	6.03 Ø	6.21-03-	8.24 Q	9.32-03-	8.83 Q	7.0- 03-	13:38
8.52:0		0.755	4.9I	4369.8	ğ. I. Z	E.12-03-	1 23.4	8.88-03-	2.8.2	₽.6- @3-	13:34
Z. EZ: Ø	8.74				8.9 E	4.18-03-	9. Š. Ę	-58-43.5	8.81 8	7.61-03-	13:35
8.22:@	4.84	7.888	8.61	9966.0			7.01 p	1.88-83-	4.23.4	7.18-03-	13:3Q
9:22:Ø	9.34	8.048	8.61	9966. Q	2.71 4	2.64-03-			7.62 3	-58-45.3	13:28
£.22:0	6.44	8.14E	6.91	9966'Ø	6.83.9	7.88-88-	6.7 <u>1</u> .8	9.8- 13-		9.0- 19-	13:58
Z.22:0	4,44	3.548	6.6I	7366. Q	I.0E 8	6.11-13-	8.4.5	7.62-13-	3.38 8		13:24
Ø:22.1	Ø. 44	342.1	6.6I	7366.8	I.88 T	-21-58	8.0E T	9.04-13-	1.14 7	4.71-13-	
i.22:8	Ţ. £\$	8.848	6.61	7366. Ø	Ø.2⊁ 8	4.74-13-	1.78 8	<b>4.</b> 63-13-	7.84 8	6.35-13-	13:22
	3.54	348.4	7.91	9966.8	I.84 6	6.7- 23-	9.54 6	0.02-23-	9.23 6	2.83-13-	13:20
2.22:0	3 67	, 9,0		0200 2							07107
£.22:@	43.5	350.0	9.6I	9966'Ø	8.43 QI	Z.@E-23-	3.03 QI	-25-45.6	6.83 å£	-52-18.3	13:18
	9.54	7.138	£.9I	9966.8	12 2.3	-62-64.4	II 28.3	I.7- 83-	1.8 21	2.24-23-	13:16
8:22:0		353.4	Ø. 91	9966.8	9. ØI EI	8.02-E3-	E.7 EI	6.88-83-	13 14.3	1.8- 63-	13:1¢
8.22:Q	43.9			4366.8	9.02 AI	4.64-63-	7.71 ÞÍ	0.5- 43-	14 24.0	2.86-63-	13:15
2.52:Q	6.44	9:99E	9.81			4.02-43-	9.08.3I	7.48-43-	1E 3E 8	9.9- 49-	#13:1Q
9.£2:@	6.44	356.8	18.2	£366.0	15 32.9			2.6- 33-	4.64 BI	9.68-43-	13:8
2.42:Q	7.34	3.838	9.7I	1966.Q	I. 74 8I	1.43-43-	8.44.8I			9.91-99-	13: 8
8.42:Q	9.94	E.Q	۵.71	Ø966'Ø	£.4 81	6.0E-33-	3.2 81	Ø. T4-33-	Ø:9 8T		13: 4
8:32:Ø	8.74	1.2	£.8I	8466.Q	19 25.2	1.11-83-	19 24.2	9.82-83-	19 26.2	3.43-33-	73: Z
ğ. 92 : ğ	Z. 64	Ø. 4	12.5	9466.Q	7.03 02	5.33-83-	8.03 QZ	6.41-73-	8.03 02	4.75-88-	
2.72:0	Ø. 13	ø. 9	14.6	4466.0	22 22.Ø	4.44-48-	22 23.3	<b>▶</b> .3- 83-	8.0Z ZZ	8.42-73-	13: Ø
C LC.N	בוש	<i>D</i> 0	• • •								00.77
£.82:@	Ø. £3	I.8	9.61	I466.0	8.I 42	3.68-83-	24 4.3	1.6- 63-	2.83 62	4.71-83-	12:58
	8.33	ē. ģī	12.3	7866. Q	9.03 32	-69-42.3	Z2 26.7	8.6- 08-	2.34 45.2	Ø.71-63-	12:56
9:62:0			6. QI	£899.8	1.88 72	8.33-09-	2.8 82	9.82-19-	8.34 TS	6,32-03-	15:24
Ø.18:0	8.83	7.21			3. ES QE	7.82-28-	4.44 ØE	2.8- 58-	3.8 08	4.84-18-	15:25
8.2E:@	ø. £8	12.5	1.6	8266.8				4.28-38-	2. g . g g	Ø.48-88-	75:20
1.35:0	6.89	Ø.61	8.8	2266.8	<b>6.78 88</b>	4.82-48-	34 26.5	A CE32.	0 6 66	<i>D</i> 70 00	
9.04:0	8.38	Ø.72	ø.ø	≯066.0	8.54 14	6.36-68-	41 20.6	8.11-@T-	9.81 Eb	4.84-68-	LIMITS
YTIAAJUNNA	WIDTH	Z∀	ΤJΑ	OITAR	-ONGITUDE	I BOUTITAJ	LONGITUDE	LATITUDE I	_ONGITUDE	I BOUTITAL	TIME
MOITARUQ	HTA9	กักร	NOS	DIAMETER					LTWT"	ИОВТНЕВИ	UNIVERSAL
					S LINE	CENTER	Y LIMIT	SOUTHER!	TTMT   E	AGDITACIA	
5 <del>9</del> 5 7.86	= T st	l <del>e</del> d								:	SAROS 148

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#### TOTAL SOLAR ECLIPSE OF 30 MAR 2033

0.02:2	5.247	8.88	ø.ø	9840.I	<b>+</b> .83-631-	1.21 88	T.8- <b>₽</b> 21-	84 41.2	2.43-331- 1.1 97	STIMIL
6.08:2	£.487	3.511	3.8	1.0453	158 12.8	Z.0 eT	8.11 241	6.7 TT	1.08 241 7.23 37	18:14
8.28:2	3.787	6.411	4.6	1.0455	126 3.6	1.98 77	1.05 241	7.23 37	7.8- 871- 7.14 87	18:12
2.48:2	742.3	116.3	ø. ør	7340.I	154 57.2	76 22.4	143 2.3	8.14 47	4.68 871 8.48 77	
7:3E:Z	748.6	112.1	3.01	6940.I	164 29.6	3.6 37	I.44 E41	2.48 87		Ø1:81
2.88:2	8.837	4.411	e. ět	0940.I	154 27.8	0.00 EY	144 32.9	3.62 27		18: 8
7.88:2	1.487	3.511	I.II	1940.1	7.44 431	2.83 27 8.83 27	146 27.2		9.82 %71 5.21 37	9 :81
Ø. 78: S	1.877	2.211	ē. <u>i i</u>	2940.I	0.81 881 7 AN A31			E. 72 IT	2.21 269 12.2	78: <del>1</del>
8.78:S	8.287	9. QII				6.84 IT	146 26.4	I.72 07	72 55.5 168 40.6	18: 2
D 75.0	9 682	OBIL	E.II	2940.I	1.65 531	3.84 QT	0.0E TAI	8.82 69	8.14 831 8.64 17	Ø :81
8.86:2	3.267	₽.60I	2.11	1940.1	1.58 83.7	6.34 69	8.78 841	0.2E 89	I.e eai e.ah bt	17:58
₽.8E:S	8.208	T. Tal	Ø. II	1940.I	157 56.2	7.84 88	1.03 641	3.88 78	8.1 %71 2.14 99	93:71
2:32.6	9.118	102.9	9. øt	Ø9+Ø.I	7.6 631	8.84 T8	2.7 131	1.24 88	9.02 ITI 9.78 88	
8.48:2	6,618	6.E&I	ī.ģī	1.0458	16ø 34.2	4.13 88 50 51.4	9.62 291	7.84 38	7.21 871 2.48 78	19:71
2.88:2	4.828	8. IQI	9.6	1.0456	3.11.591	8.4.8	153 58.4	I.83 48		17:52
2:31.4	6.628	4.66	<u>7</u> .8	1.0454	1.8 481	2.83 48	155 34.8	0.4 48		Ø9:71
	0 000	, 00	2 0	1310 1	r 3 /8:	0 03 18	0 16 331	0 V V9	7.36-871- 9.11 33	84:7I
2:20.2	6.787	<b>6.78</b>	ø.ø	1.0436	1.03 471	0.61 43.Ø	7.22 671	7.1 83	1.82-371- 8.74 48	STIMIZ
YTIJATOT	HTGIW	Z∀	T⊿A	OITAЯ	LONGITUDE	<b>BOUTITA</b> J	LONGITUDE	<b>30UTITA</b> J	LATITUDE LONGITUDE	TIME
NOITARUG	HTA9	NOS	NOS	DIAMETER		• • • • • •				ONIVERSAL
					ER LINE	CENTE	N LIMIT	SOUTHER	NORTHERN LIMIT	14203VTM1
296 0.46	- 1 PO 1	9/1								

Delta T = 95.7 Sec

TOTAL SOLAR ECLIPSE OF 20 MAR 2034

6.38:1	2.201	I. \Q\Z	ø.ø	1.0289	2.18-29-	1.84 48	7.88-26-	34 18.5	4.36-26-	35 13.8	STIMIL
	-			anna: T	1.32-77-	8.01 4£	7.03-97-	9.88 88	7.E- 8T-	94 45.0	11:24
8.å :2	115.1	1.192	13.1	AEEQ.I			1.85-88-	3. IS SE	9.8- 78-	1.48 EE	8 <b>†:</b> II
7.22:2	124.4	1.432	23.2	1.0360	6.03-99-	8.73 28		8.8 IE	9.41-09-	3.82 28	Z7:II
6.88:2	130.4	2.642	S. ØE	6780.1	0.6- 09-	31 45.8	7.4- 03-		Ø. I – 88 –	8.21 18	11:36
2:52:5	138.1	Ø.342	8.35	1.039¢	2.1- 88-	8.48 QE	5.2- 33-	Ø. 73 es		8.8 88	Ø8:II
3: 4:5	138.8	2.142	8.04	3040.I	0.84-03-	8.42 62	1.63-03-	4.84 82	9.54-03-	8.53.8 28.53.8	11:24
3:15.2	1.241	9.752	45.2	9140.I	2.11-74-	2.31 82	4.61-74-	8.88 TS	3.5- 74-		81:11
	8.441	9.552	€.94	1.0425	9.0- 44-	8.8 TS	8.11-44-	7.82 82	-43-60.2	27 45.3	
8.42:8		I.082	ø. £3	Z840.1	9.6- Ih-	9.83 32	-41-55'2	Z. ØZ 3Z	Ø.73-04-	8.78 82	11:12
8.88:8	2.741		3.83 8.53	1.0438	0.48-88-	24 21.3	7.84-86-	24 12.9	3.61-86-	26 29.9	9:11
8.14:E	4.641	1.922		5440.1	3.0I-8E-	8.44.62	-36-26.9	£.8 £2	4.43-38-	1.62 42	ø:II
7.74:E	121.2	8.122	8.63	T GAA3	3 61.96	8 77 60	0 00 00	• • • • • • • • • • • • • • • • • • • •	•		
				011017	0:00-00-	₽.88 2Z	9.41-48-	8.0 S2	5.65-55-	8.81 62	10:64
3.53.5	6.231	8.812	8.28	8440.I	6.83-88-		9.9- 28-	20 54.8	5.25-15-	0.11 22	84:0I
3:58.4	164.3	8.QIZ	3.39	1340.1	9.13-1E-	8.28 12		8.64 61	7.18-62-	7.3 12	7 <b>0:</b> 45
4:2:4	122'8	1,402	6. Ta	1.0464	9.13-62-	7.72 Q2	8.11-0E-	18 45.3	2.88-72-	8.0 02	10:36
9.3 :4	1.881	1.961	ø.ør	1°0428	<b>6.83-72-</b>	0.82 ei	7.71-82-		8.44-32-	18 56.3	78:38
Ţ.Ţ ; Þ	7.731	8.381	9.17	1.0458	2.8- 82-	7.81 81	7.72-82-	2.14 71		2.23 71	10:24
I.9 : h	128.5	1.971	7.27	1.0458	6.81-42-	6.⊅I TI	3.04-42-	8.78 ar	-23-56.1		81:01
3.6 :4	1.631	164.5	1.87	1.0458	6.28-22-	4.II 8I	-55-22:1	16 34.3	9.6- 22-	16 48.5	21:01
	9.631	152.8	9.27	1.0458	4.74-02-	7.8 31	9. QI-IZ-	5.15 A1	1.42-02-	16 45.1	
Ø.6 : Þ		7.141	Ø.27	7340.1	8.2- er-	14 6.4	2.82-91-	7.82 EL	<b>6.86-81-</b>	1.24 41	9 :01
7.7 : A	8.631	9. ISI	8.07 8.07	1.0455	2.71-71-	8. <u>2</u> £1	I. IÞ-71-	12 26.4	-18-53.1	8.98 EI	ø :øt
4: 5.4	6.631	131 0	3 67	3370 1	0 21 21	0 0 00					
			0.00	1.0462	Z.0E-3I-	9.0 SI	-12-24·4	11 24.3	9.3- 31-	8.88 SI	<b>79:6</b>
4: 2.3	7.63 <u>I</u>	123.6	8.89		8.04-81-	3.83 QI	0.8- 41-	10 22.6	Ø.81-E1-	3.48 II	87:6
3:58.2	129.3	8.811	2.88	6440. I		8.83 6	8.21-21-	9.12.9	9.22-11-	10 32.4	24:6
8.63:6	128.6	2.11 <b>1</b>	8.69	1.0445	4.74-11-			7.61 8	4.42-6-	9.0E 6	98:6
3.47.5	8.731	9.90I	T. 0a	1440.1	8.64-6-	2.88 8	0.41-01-	7.81 T	6.61-7-	8.82.8	ø£:6
8.04:E	1.991	e.s@r	3.73	1.0435	6.44-T-	8.83 T	T.6- 8-		2.7- 3-	2.72 T	₽2:6
3.88:8	164.3	8.66	54.1	1.0429	4.28-3-	8.23 8	2.73-3-	8.71 8	9.54-2-	7.32 8	81:6
3:24.7	6.131	٤.٢و	4.03	1240.1	2.e- E-	3.13 3	2.48-8-	5.71.3		5.4.3	ZI:6
3:15.3	Ø.641	8.36	9.84	1.0413	₽.2E-0	9.03 A	₽.73-@	7.81 A	6.8- Q		9:6
7.4 :8	145.4	9.56	1.24	Z040.I	8.22.2	8.6⊁ €	3.73 £	3.16.6	2.48.5	4 22.9	ø :6
	6.04I	8.26	4.75	Ø65Ø.1	5.54 3	I.64 2	8.71 3	9.81 S	9.6 9	3.12.5	٥٠ ه
Q:53:Q	OMIL	2 00	, 20	2002	• • • •						-0.0
	L.OOT	2.19	9.IE	9750.1	8.14 e	8.84 I	8.41 6	Ø. TI I	9.8 QI	0.02 Z	<b>79:8</b>
8.68:2	135.4		25.4	7350.1	8. I 4 4 I	Z.84 Q	14 13.Ø	8.71 Q	1.11 31	4.81 I	87:8
2:24.5	128.3	3.86			21 65.2	6.11-8	21 20.0	9.04-Q	2.28 22	E. 81 @	2⊅:8
Ø.3 :S	5.811	ø. øe	7.8I	1.8331	0 33 10	0 11 2	D DO 10	0 2		>	
			~.~	017017	0:07 10	8.73-Q	8.82 TE	1.42-1-	1.48 TE	3.0E-0	STIMIJ
0.88:I	6.86	I.0e	ø.ø	<b>6720.1</b>	3.02 78	£ 73-8	A 90 TC				
		71/	170	OTIVU	DOLLENO.	LATITUDE L	TOMETIONE	LATITUDE L	ONGITUDE.	J BOUTITA,	TIME L
YTIJATOT	WIDTH	ZΨ	TJA	OITAR	adi ittono	I POLITITA I	2011220110				NNIVERSAL
DURATION	HTA9	NUS	NUS	DIAMETER	3NT3 1	UT 1 N T 2	ITWT7 P	SOUTHERN	TIMIT!	NORTHERN	
					HUT I	CENTER	TIVE	407UTI 102			
											SAROS 130

Delta T = 96.2 Sec

SAROS 135 ANNULAR SOLAR ECLIPSE OF 12 SEP 2034

2:43.5	9.191	2.372	ø.ø	9836.Q	ø.81 3	1.14-04-	4 23.8	8.82-14-	9.63 4	9.83-68-	LIMITS
2.84:2	8.741	284.3	2.11	9196.Q	18 48.8	0.31-9£-	1.62 71	2.7- @4-	1.43 61	1.32-88-	ø :81
7.84:2	Ø.881	4.262	1.12	2496.0	I.74 62	8.31-76-	4.42 es	1.63-78-	8.7 <b>0</b> 8	£. EE-8E-	<b>≯</b> 9:∠ī
2:68.5	7.82I	8.792	7.72	6996'Ø	36 23.Ø	8.78-38-	8. P.I 88	3.81-88-	£. \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\	7.83-48-	84:71
2:51.8	5.62I	Z. 208	Ø. 55	2799.8	8.9I IA	9.Y- 48-	41 18.5	5.44-48-	I. 02 IA	1.25-55-	24:71
8.23:S											
	Ø. 611	£.8&£	8.7£	£896.0	6.61 34	2.44-28-	45 23.1	6.81-88-	45 16.4	-32-10.5	38:71
2:53.9	116.4	I.QIE	7.14	2696.0	6.64 84	7.42-16-	4.64 84	0.73-16-	0.78 84	8.23-&£-	Ø8:71
7.43:2	115.5	9.515	45.3	6696.Q	9'Øt 19	3.8- &£-	9.84 I3	2.8E-&E-	51 32.2	1.85-62-	42:71
2:56.4	ø.alt	8.718	7.84	8079.0	84 18.Ø	9.33-82-	8.72 A3	3. <i>≱</i> 2-62-	5.8 43	-28-26.9	81:71
Ø.83:S	6.701	321.8	8.13	2179.Q	5. 04 83	6.64-72-	Ø.13 83	2.21-82-	2.62 93	8.31-72-	21:71
2:56.5	Z.8@I	1.928	9.43	7179. Q	9.03 83	8.46-82-	5.2 63	1.2- 72-	Ø.68 83	8.7- 82-	9:71
2:56.9	T. AQI	7.0EE	2.73	1279. Ø	8,13 %8	-25-27.5	7.E 18	0.43-32-	Ø. 68 Ø8	1.1- 32-	ø :Zī
£.73:2	0.001	0:000	0:00	071010	+·++ <b>70</b>	0:17-67-	£.73	1.14-47-	0:10 70	7:00 07	
	9.EQI	335.8	9.69	3279.0	4.44 29	8.12-21.8		7.74-42-	62 31.5	-23-56.1	16:54
3.73:2	102.8	341.3	9,19	827e.0	2.18 48	7.71-62-	9.44 49	0.54-62-	6.71 48	-22-52.5	84:81
7.73:2	102.2	4.748	4.69	1879. Q	1.51 88	6.41-22-	6.82 88	7.68-22-	6.63 39	-21-5Ø.2	16:42
8.73:2	8.IQI	324°I	8.49	££79.\	Ø.13 78	<b>4.81-12-</b>	1.3 89	<b>6.78-12-</b>	6.88 T8	1.64-82-	16:38
6.73:S	T.IQI	Þ.I	6.39	3879.Q	Ø.82 68	2.81-82 <b>-</b>	4.04 ea	8.78-\S-	8.II 68	2.64-61-	ØE:9T
8.73:2	8.101	1.6	3.99	8879.Q	8.83 &Y	1.41-81-	3.EI 17	0.88-e1-	I.AA QT	£.03-81-	16:24
8.73:2	1.201	1.71	8.33	9879.Q	2. 0E 27	1.81-81-	72 45.3	6.68-81-	72 15.3	9.23-71-	81:91
9.73:2	9.Z@I	Ø.32	8.89	9879.Q	Ø. I . 4 T	2.91-71-	74 16.3	0.54-7I-	8.34 ET	7.33-81-	ZI:9I
8.73:2	4.EQI	7.28	6.39	9879.Q	9.1E 3T	-16-23.4	3.74 37	1.74-81-	75 16.4	8.63-31-	9:91
0.73:S	184.3	6.68	6.49	3879.0	8.8 TT	9.82-31-	3.61 TT	-12-22.4	T. TA 8T	6.4- 31-	Ø :91
010017											
8.83:2	105.4	46.5	63.5	4879.0	8.88 87	7.48-41-	0.63 87	-14-58.8	8. 02 87	9.01-41-	72:2 <del>4</del>
2.88:2	7.8 <b>0</b> 1	52.3	7.13	2879.0	8. 12. 3	6.14-61-	6.82 \@8	2.8- ÞI-	8.33 97	<b>6.71-81-</b>	12:48
2:55.6	2.8&£	3.73	7.63	Ø879. Ø	1.13 18	2.03-SI-	1.8 28	8.41-51-	81 34.2	-12-25.9	12:45
Ø.33:2	6.60I	ø.29	4.73	7270.0	1.48 88	-11-26'2	83 21.6	-12-24.5	8.31 68	8.48-11-	12:38
2:54.2	T.III	ø.33	8.43	£27e.@	85 22.5	ø.ør-tr-	8.04 38	<b>⊅.</b> 36-11-	<b>9.</b> 4 38	8.44-QI-	JE:30
2:53.4	7.EII	<b>4.</b> 69	Ø.23	6176.Q	8.7I 78	7.12-01-	₽.3E 78	T.TA-QI-	8.63 88	6.33-6-	12:54
2:52.4	6.311	8.27	6'87	4179.0	7.12 es	9.48-6-	I.IA 98	E.I- QI-	4.2 e8	2.8- 6-	12:18
2:51.4	£.811	8.47	9'97	8079.0	9.8E 19	Ø.64-8-	Ø. 73 19	9.91-6-	91 16	6.12-8-	71:91
2.68.2	ø. izi	ø. 7 <u>7</u>	6. I h	INTO.N	6.3 49	1.3- 8-	9. 72 4e	4.88-8-	9.44 69	1.78-7-	12: 8
6.84:2	0.42I	ğ. 67	9.75	£696.8	4.43 86	Z. EZ-7-	8.71 76	9.23-7-	4.18 8e	I.43-8-	Ø :91
0 87.6	D / C 1	W 62	0 28	g 0603	V V3 80	0 60 2	8 21 20	8 03 L	1 16 80	1 73-8-	יבי ש
4.74:2	127.4	9. Ø8	<b>₽.</b> ££	4896.0	7.6 åøt	8.54-8-	9.35 @@I	8. 41-Y-	2.44 ge	9.51-8-	14:64
7.34:S	131.5	1.28	1.82	2796.Q	104 E.5	®.8- 8-	104 35.6	3.04-8-	e. 9e eqi	0.86-3-	14:48
7.84:S	8.881	4.88	8.12	9996'Ø	£.21 9@1	ø.86-3-	7.03 ear	6.21-8-	3.38 8@I	7.E- 3-	14:42
0.14:S	145.Ø	T. 48	12.2	2886.0	I.TI TII	-2-51.5	9.82 SII	4.I- 8-	8.41 811	8.24-4-	14:38
2:38:1	1.831	6.38	ø.ø	øø96.ø	0.18 821	7.34-3-	128 55.Ø	ø. øε−9−	1.84 821	£.4- 3-	LIMITS
YTIAAJUNNA	MIDTH	Z∀	TJA	OITAR	ONGITUDE	LATITUDE	LONGITUDE	LATITUDE	LONGITUDE	LATITUDE	<b>TIME</b>
DURATION	HTA9	NOS	NOS	DIAMETER							NNIVERSAL
					S FINE	CENTER	N LIMIT	SOUTHERI	N LIMIT	NORTHER	•• ••

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#### ANNULAR SOLAR ECLIPSE OF 9 MAR 2035

1:20.4	1.68	7.392	ø.ø	6776. Q	2.84 Te	7.88-8-	8.82 Te	9.83-8-	7.04 Te	0.e- 8-	LIMITS
6.8I:I	ø:18	6.882	ø.8	TØ86'Ø	9.81 301	I.02-6-	8.2 401	1.88-6-	1.22 801	6.8- 6-	Z4:0
			7.6I	££89.8	4.78 3II	8.8- 11-	9.01 311	1.22-11-	116 3.4	9:99-ØI-	98:Q
8. QT: I	6,89	p.692			4.81 ISI	7.35-21-	8.73 \QL	9.74-SI-	121 35.0	7.52-21-	Ø8:Ø
6.8 :I	8,18	271.5	9.82	1986.0			125 14.5	8.8- 11-	125 44.4	8.44-61-	
3.8 :1	3.83	T.ETS	32.1	₽986.0	126 29.6	-13-22.6			129 9.6	4.1- 31-	
8.0 :I	Ø.23	Ø.87S	8.88	3789.0	0.73 82I	7.11-31-	128 44.3	-16-22.ø			
₽.83:Q	6.84	8.872	6.0Þ	≯886.@	131 22'2	-18-25.1	131 44.4	8.46-81-	132 6.4	9:91-91-	
Z.93:0	1.34	281.6	8.44	1686.0	134 34.0	7.88-71-	134 24.2	8.34-71-	8.84 48 <u>r</u>	7.72-71-	<del>-</del>
8.43:0	42.3	8.482	Ø.84	7686. @	136 58.Ø	9.84-81-	2.64 8EI	9.33-81-	8.8 YET	<b>₽.8</b> E-81-	ø :ø
9.53:0	6.68	2.882	ø:19	£066.0	E.II 98I	Ø:99-6I-	E.E 9EI	Z.4- &2-	E. 61 681	8.74-61-	
	9.7£	8.262	7.83	7066.0	9.91 141	1.4- 12-	2.9 141	0.21-12-	141 24.Ø	-20-56.3	23:48
Z:13:0		8.792	2.83	I166.8	8.31 641	-22-11.5	143 8.9	1.91-22-	143 22.6	6.8- 22-	23:42
0.03:0	3.98				9.01 341 9 31 511	2.81-62-	146 4.2	9.32-22-	0.71 341	6. QI-82-	
Ø.64:0	7.48	302.5	4.83	4166.8					4.8 74I	2.71-42-	
Z.84:0	8.88	8.8 <b>0</b> 8	2.09	8166.Q	247 2.3	4.42-42-	146 56.3	7.18-42-		8. E2-32-	
8.74:Q	7.28	7.418	7.13	8166.Q	148 52.1	-26-30.1	148 46.4	5.78-32-	8.73 841		
8.74:Q	8.2E	7.128	6.29	6166.Q	1.14 @31	-26-35.5	16ø 35.6	8.24-82-	15Ø 46.5	-26-28.3	• • • • • • •
2.74:0	9. IE	3.628	9.69	6166'Ø	1.08 231	<b>4.04-72-</b>	162 24.9	8.74-72-	162 35.3	2.88-72-	
4.74:0	4.IE	Ø. 755	0.49	6166'Ø	164 20.2	Ø.34-82-	1.31 431	6.23-82-	164 25.2	7.7E-82-	
7.74:0	3.15	3.54E	9.59	6166.8	156 12.2	2.64-62-	156 7.3	7.83-62-	156 17.Ø	8.14-62-	23: Ø
7 74.0	3 16	D 370	0 00	0100 2	0 01 011	• • • • • • • • • • • • • • • • • • • •					
010+10	7.18	325.9	8.89	8166.0	1.7 831	Z. E3-&E-	168 2.5	8.0- IE-	7.11 831	9.34-08-	22:54
8.84:0		8.Q	4.28	8199.8	0.8 03r	8.83-16-	16ø 1.5	7.4- 28-	160 10.4	6.84-16-	22:48
Ø.64:0	32.28					I.0- EE-	3.6 291	E.8- EE-	1.41 281	8.13-26-	22:42
Ø:68.Ø	Q.EE	Ø.8	1.13	4166.0	162 9.9				164 24.0	5.43-55-	
S:E1.2	Ø.48	6.4 <u>I</u>	4.63	1166.8	164 20.Ø	0.6- 48-	0.81 481	7.11-48-	3.14 881	6.83-46-	
8:52.8	35.2	4.12	4.73	7066.0	8.7E 33I	3.3- 36-	1.48 34.1	7.41-38-			72.22
Z.43:Q	7.88	4.72	1.33	£066.0	6.4 ear	3.7- 86-	9.I 99I	8.71-88-	2.8 691	7.73-38-	
Ø:99:Ø	8.88	1.55	52.5	8686°Ø	4.84 171	6.8- 7£-	8.04 ITI	<b>₽.</b> 61-78-	2.84 ITI	3.83-86-	
ø.83:0	7.04	3.88	9.64	£686.0	174 35.8	-38 -9.5	7.88 ATI	8.&S-8E-	6.7£ ₽71	£.83-7£-	
2.0 : r	Ž.ξμ	8.54	9.84	8886.8	2.34 TTI	2.6- 68-	2.44 TTI	4.IZ-9£-	3.84 TT	1.73-86-	
	2.84	Ø. 64	Ø. 24	6789.8		- 3.7- 04-		8.0Z-04-	9.54-871	- 4.43-66-	52: Ø
9.2 : t	6 87	<i>D</i> 07	D CV	0200 \$	, ,, ,,	3 2 27	• • • • • •				
1: 6.2	7.64	2.43	1.65	@786.@	2.44-471-	· ['b- [b-	I.SA-471-	- 41-18.6		- 7.64-04-	
ø.8 : I	Ø. 43	9.63	8.48	6386.8	8:1- 0/T-	-41-68.1	5.2- QYI-	- 0.41-54-	1.21-071	- 6.24-14-	21:48
1.11:1	2.63	5.33	8.62	7486.8		- 42-48.2	4.82-481-	- T.3- E4-	184-42.3	- 8.0E-S4-	27:12
		Ø. 27	7.52	1889. Q		- 7.18-84-	6'9T-/9T-	-43-61.1	167-64.3	- 43-12.6	21:38
9. 4I:I	6.39						7.66-041-	- 44-22.3		- 6.68-84-	
Ø.91:I	7.3T	3.08	3.31	8086.0	0 66-711-	- 6.0- pp-	7 63-871	2 00 77	,, .	0 00 0.	
1:25.8	2.36	3.36	0.0	4976.0	6.22-721-	- 2.42-64-	8.63-821-	- 43-48.5	8.81-721	- t.83-24-	STIMIL
YTIAAJUNNA	WIDTH	Z∀	TJA	OITAЯ	_ONGITUDE	LATITUDE L	ONGITUDE	LATITUDE L	ONGITUDE	J BOUTITAL	TIME
DURATION	HTA9	NOS	NUS	DIAMETER					LTMTT	ИОВТНЕЯИ	UNIVERSAL
					S FINE	CENTER	TIMIT	SOUTHERN	TIMI	NOTUTONA	
28C 1:06	= 1 63	I Ə (I									SAROS 140

8:09:0

1:16.3

3.08:1

1:42.4

1:52.6

7.1 :2

6.6 :2

£.71:2

0.42:S

0.08:2

4.35:2

1.04:2

1.44:5

2:47.5

2:68.2

2:52:2

3.53.5

2:54.2

2:54:1

2:53.3

2:21.8

3.64:2

2:46.5

8.24:2

4.88:5

1.88:2

2.72:2

4.02:2

8.21:2

2.4:2

1:64.6

3.54:I

1:30.4

7.II:I

8:33:0

YTIJATOT

2.73

9.97

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I.e@I

S.III

115.9

2.411

116.2

112.9

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9.911

9.911

116.4

1.911

115.7

118.1

114.3

113.4

112.3

Ø.III

9'6ØI

6. TØI

Ø.90I

8.EQI

S.IØI

2,86

9.46

I.08

6.58

3.81

4.28

**MIDTH** 

1.872

Ø. 972

2.472

2.272

I. ØYS

7.732

Z92

1.292

9.832

7.432

2.032

245.1

1.682

232.4

8.422

216.3

S. T&S

7.7er

188.2

6.87I

IVØ.2

162.2

164.9

148.2

142.1

136.4

I.IEI

6.321

8.0ZI

T.SII

p. ØII

7.40I

1.86

8.88

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7. ØI

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1.0266

9720.I

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1620.1

7620.I

EQEQ.I

TOED. I

IIEØ.I

1.0314

TIEW.I

SIEQ.I

1.832Ø

1.ø32ø

1.0320

ASEQ.I

SIEQ.I

TIEQ.I

FIEG. I

IIEQ'I

T&E&. I

I.Ø3Ø2

9620.I

Ø620.I

1.0282

ZYZØ.I

1920.I

1.0246

1.Ø228

7eia.i

1.0164

**BATIO** 

6.27.4 142 59.9

I. 6I 67I I. 0E 9I

8.8- 871- 8.84 TI

3.44-371- 1.8 91

\$.15-571- 3.02 02

7.42-171- 8.28 IS

22 43.6 -169-22.9

23 62.6 -167-24.5

Z.82-331- Z.0 3Z

8.55-531- 3.8 SS

7.75-181- 8.11 72

3.14-631- S.31 8S

3.54-731- 8.71 62

30 18.8 -155-42.6

1.85-531- 7.81 IE

9.82-131- 2.71 28

8.51-641- 5.41 55

3.13-341- 8.9 4E

9.02-44I- 3.E 3E

36 55.3 -141-48.8

8.84-881- 8.44 88

7.86-361- 7.16 TE

38 15.5 -132-12.3

38 65.3 -128-22.9

7.8- 421- I.QE 98

3.6- 911- 2.83 98

48 16.3 -113 -2.9

8.81-301- T.TI 04

39 35.5 -92-46.2

4.14-67- I.A 8E

LATITUDE LONGITUDE

8. QZ 8

8.82 QI

8.8 SI

13 40.1

15 7.3

1.78 731

164 36.3

Ø'9Z 69I

173 14.4

176 28.4

5 11.6 142 58.5

8. N. T. 158 10.6

9.8 391 @.8 @I

4.03 631 E.eh II

8.88 ETI E.IS EI

1.23 371 8.74 41

8.24 eyr 2.e at

9.54-771- 7.72 TI

18 43.6 -175-22.1

2.9- ETI- E.TB 9I

8.8- ITI- 8.8 IS

7.1- 631- 0.61 SS

8.8- 781- 8.72 82

I.8- 331- 8.45 42

25 4Ø.3 -163-13.4

8.81-181- 8.44 82

48.8 -159-23.4

28 50.0 -157-26.3

29 68.8 -166-26.6

30 50.3 -153-23.1

31 48.5 -151-15.1

4.1- 941- 2.34 SE

33 40.5 -146-40.8

9. II-44I- I.48 48

36 25.8 -141-33.8

36 15.4 -138-42.1

3.85-351- 4.2 78

37 46.5 -132-13.Ø

9.82-821- 8.82 88

39 2.4 -124-11.4

8.31-611- 8.18 68

39 51.4 -113-28.9

8.84-301- 4.33 98

8.75-56- 8.61 6E

9.44-6Y- 3.74 TE

LATITUDE LONGITUDE

6.14 241 4.14 B

7.33 871 8.03 St

7.62-871- I.II 81

2.7- 871- 8.85 91

8.63-671- 8.64 NS

21 56.7 -171-46.6

4.44-63I- 9.7 ES

3.34-731- 8.71 42

25 25.8 -165-48.6

7.23-531- 8.25 82

7.88-181- 1.88 72

7.63-631- E.SA 82

7.0- 831- 2.34 es

9.83-331- 8.84 ØE

3.53-531- I.74 IE

32 46.0 -151-42.6

1.82-841- 8.84 88

2.2- 741- 1.65 48

7.62-441- 0.88 38

8.84-141- 6.45 88

37 14.4 -138-51.3

3.01-35I- I.I 85

38 44.5 -132-11.3

3.81-821- 8.82 98

4.33-621- 6.73 98

7.03-811- T.42 04

0.44-SII- I.I4 04

7.84-401- 8.88 QA

1.13-19- 4.03 es

7.0E-67- 7.6I 8E

LATITUDE LONGITUDE

I.88 8

8.98 QI

1.42 21

13 28'8

1.72 31

121

7.69 89I

7.64 SYI

176 4.5

79T

8.2

4.8

LIMITS

3:3Q

3:24

3:18

3:15

9:5

Ø : E

5:24

2:48

2:42

5:38

5:3®

5:24

2:18

5:15

9:2

Ø : Z

1:24

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7:45

1:38

J:30

1:24

1:18

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# FIFTY YEAR CANON OF SOLAR ECLIPSES: 1986 - 2035

2035 SECTION 4 - GLOBAL MAPS OF SOLAR ECLIPSES: 1986

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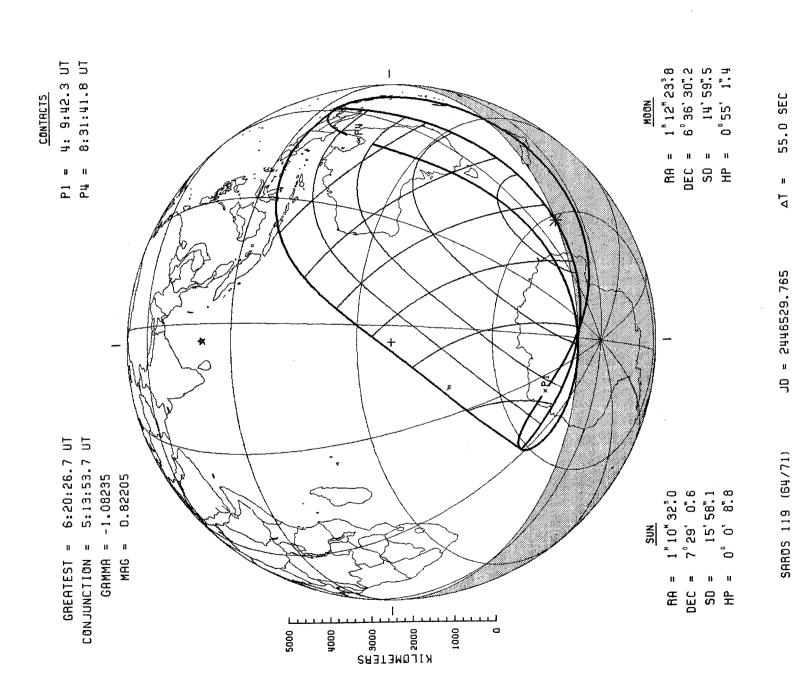


Figure 31

## ANN/TOT SOLAR ECLIPSE -

1986

ന

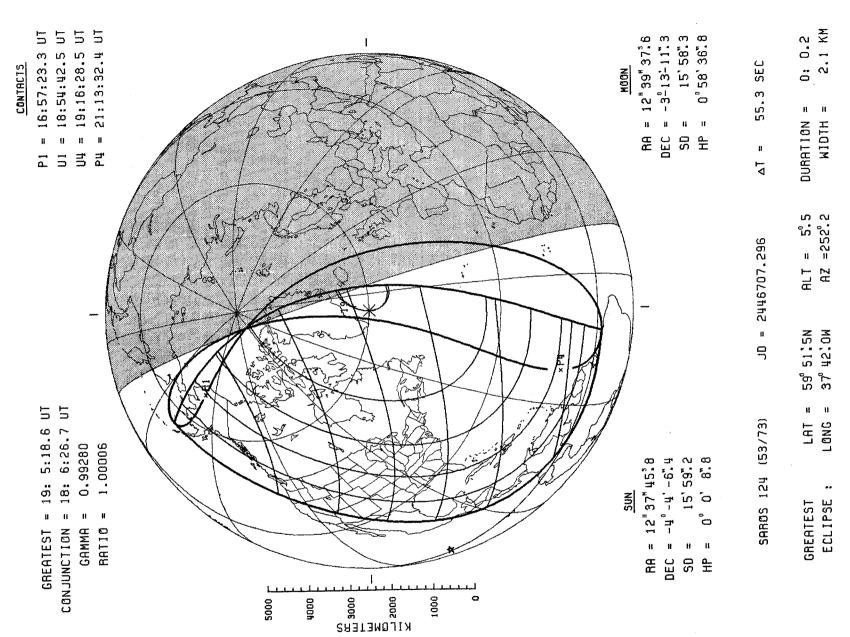


Figure 32

## 1987 MAR 29 ı ANN/TOT SOLAR ECLIPSE

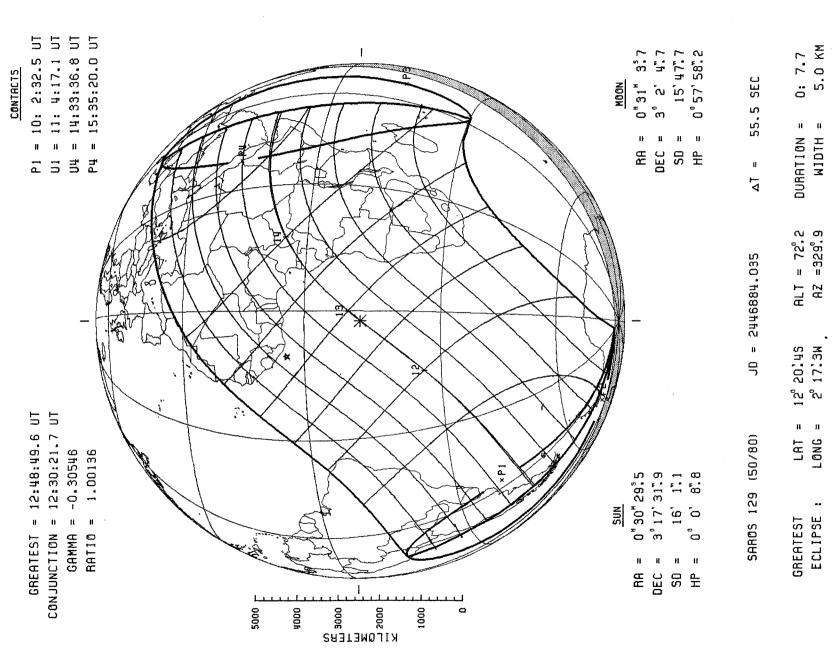
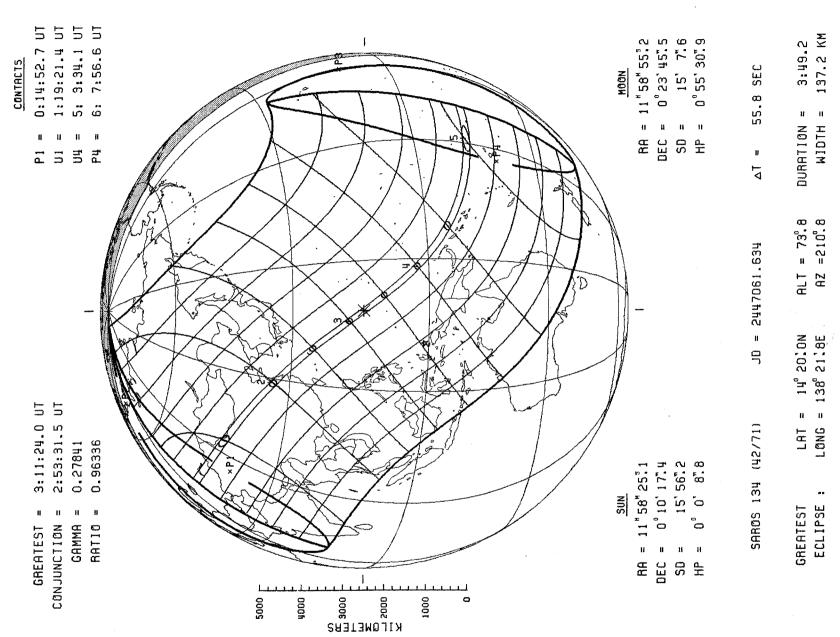


Figure 33 145

## SEP 23 **ECLIPSE** SOLAR ANNULAR

1987



igure 34

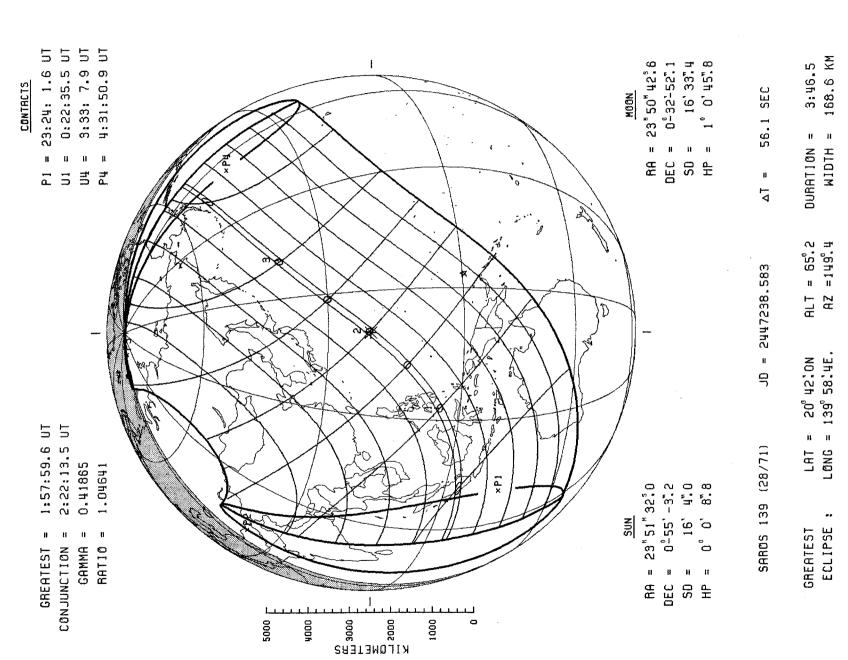


Figure 35 147

## 1988 SEP **ECLIPSE** SOLAR ANNULAR

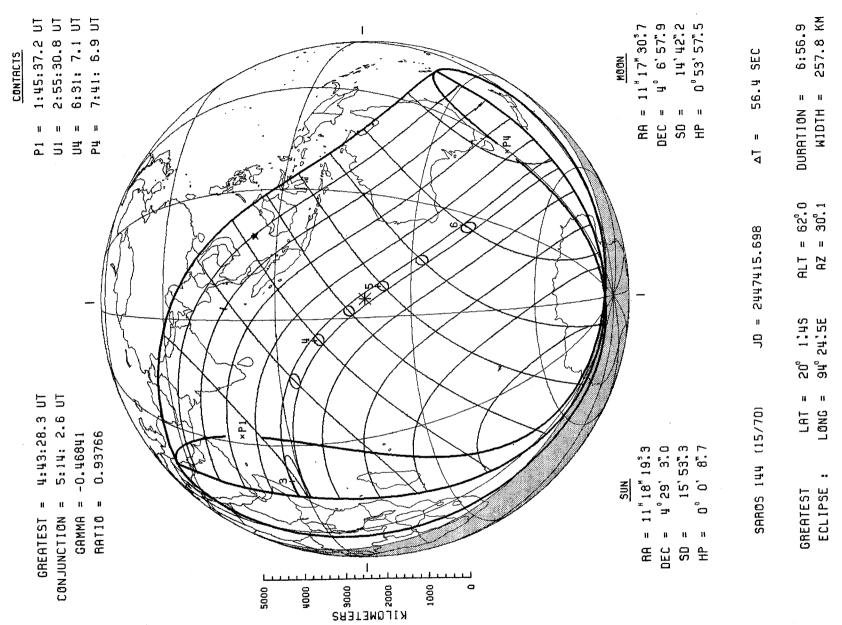


Figure 36 148

# PARTIAL SOLAR ECLIPSE -

7 MAR 1989

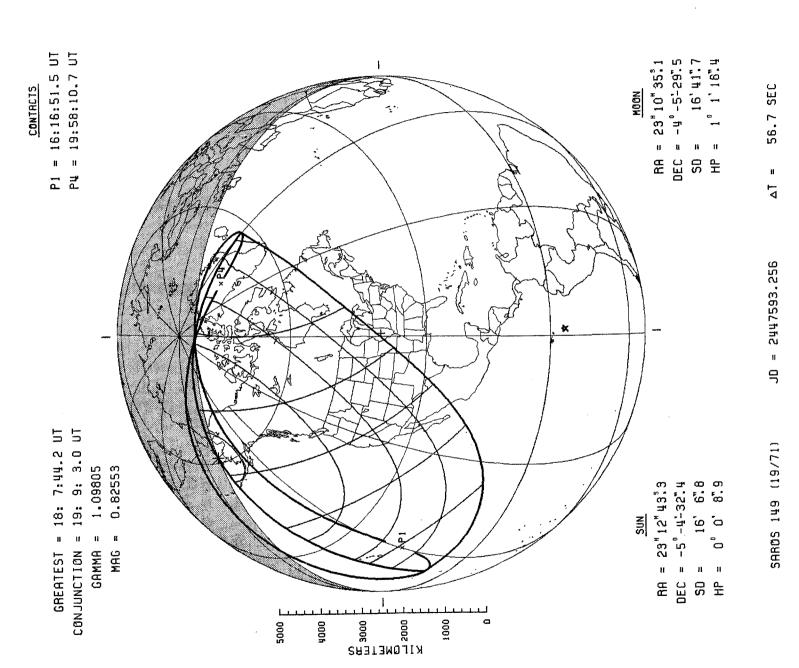


Figure 37

## AUG 31 ı SOLAR ECLIPSE PARTIAL

1989

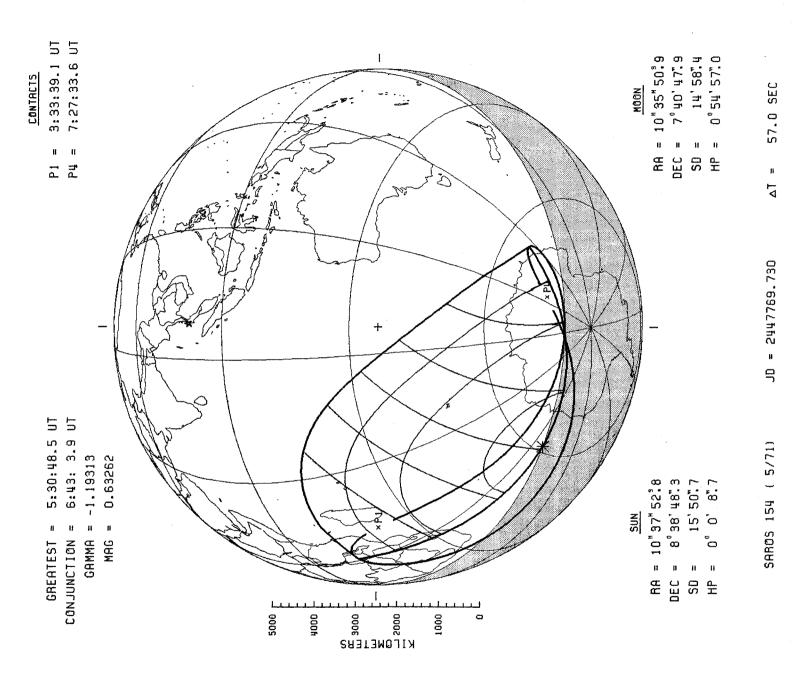


Figure 38

## 1990 JAN **2**6 1 ANNULAR SOLAR ECLIPSE

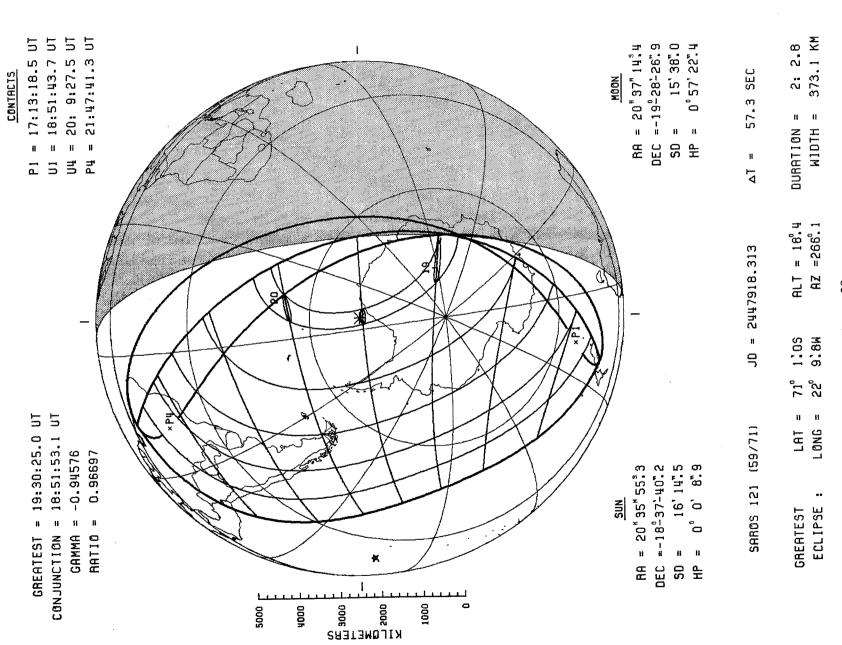


Figure 39 151

#### 1990 JUL 22 ı **ECLIPSE** SOLAR TOTAL

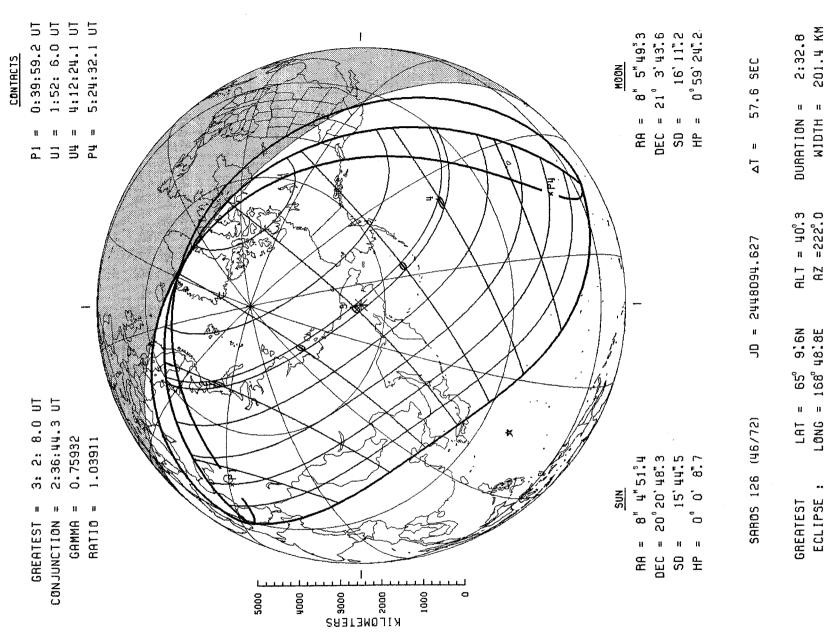


Figure 40

## 1991 JAN 15 ı ANNULAR SOLAR ECLIPSE

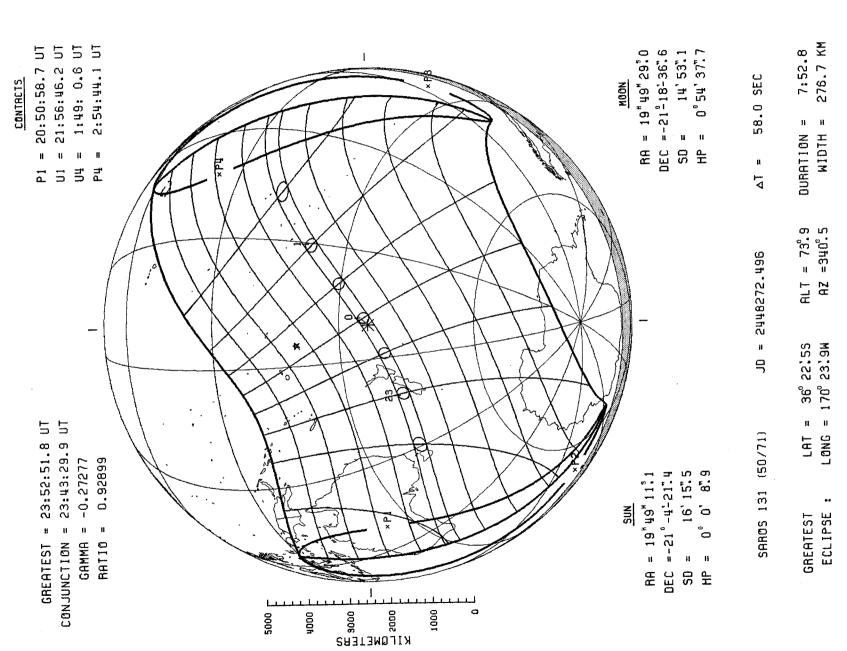


Figure 41

## 1991 JUE 1 SOLAR ECLIPSE TOTAL

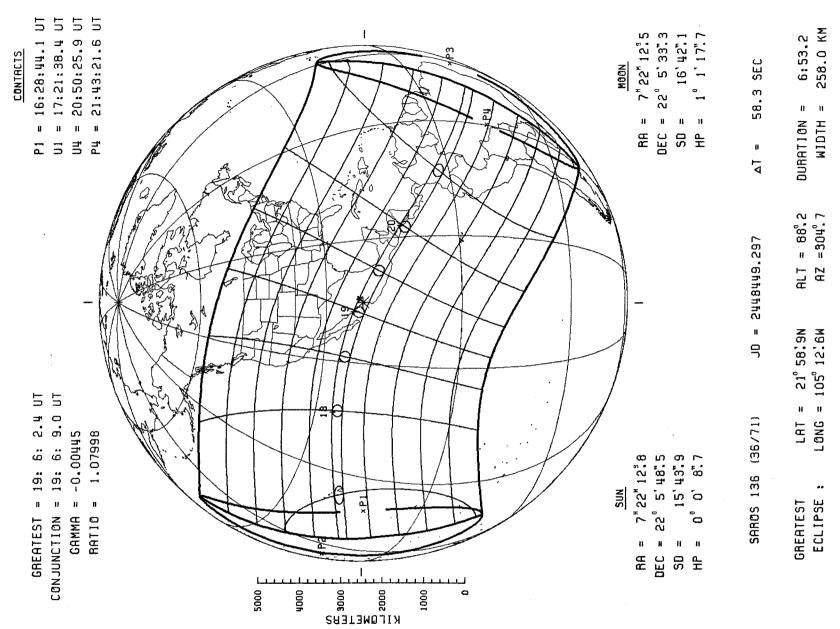


Figure 42 154

## 1992 JAN J SOLAR ECLIPSE ANNULAR

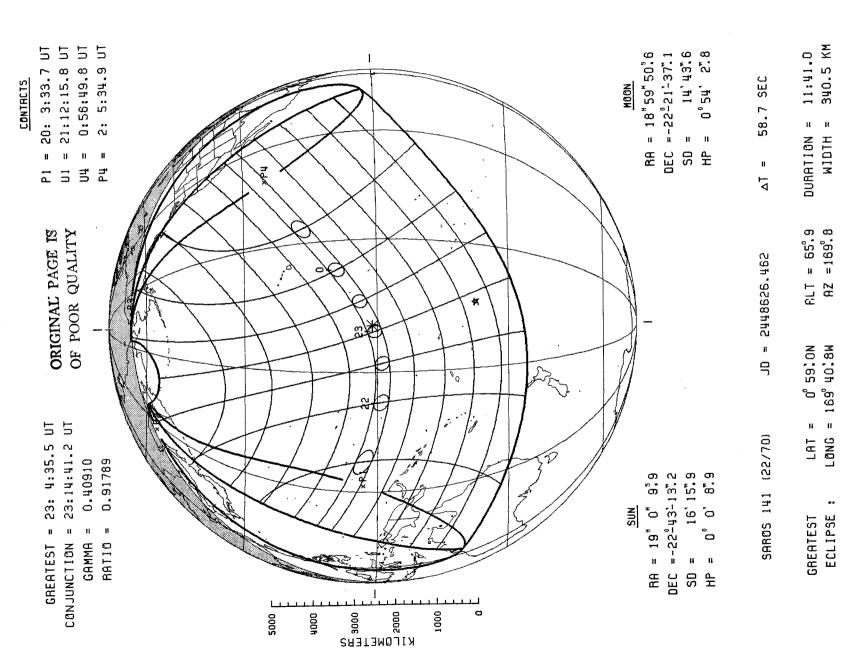


Figure 43 155

## 1992 S 30 ı TOTAL SOLAR ECLIPSE

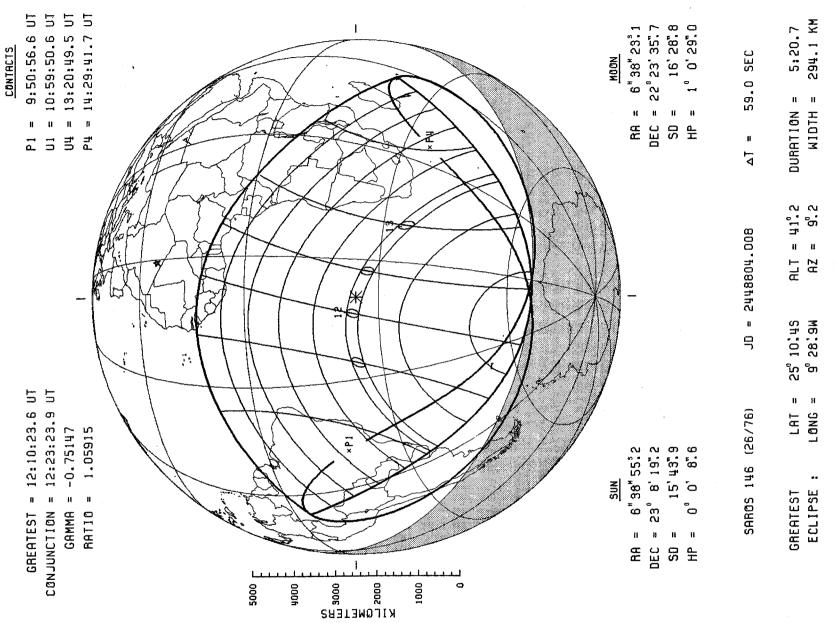


Figure 44 156

## DEC 1992 2ŭ SOLAR ECLIPSE PARTIAL

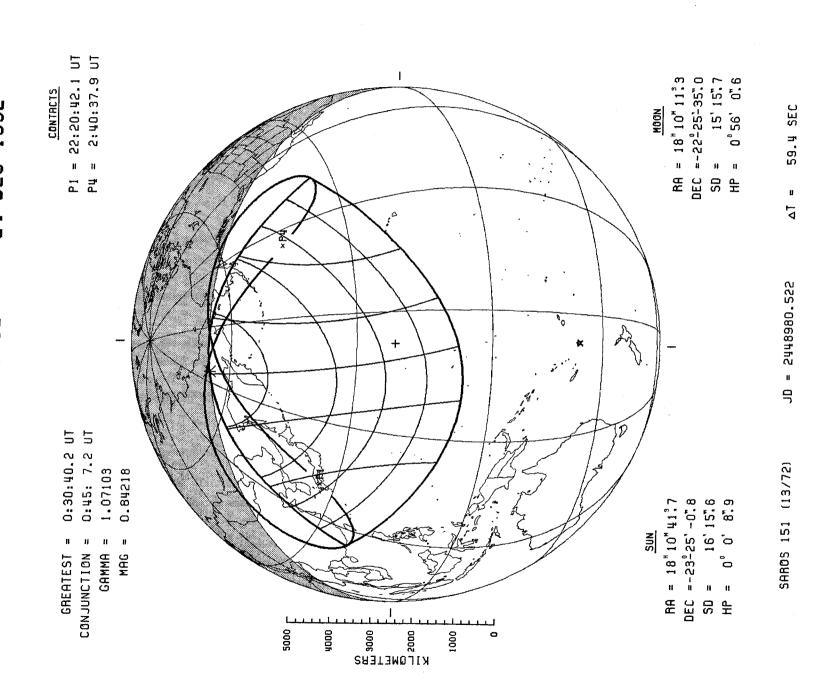


Figure 45

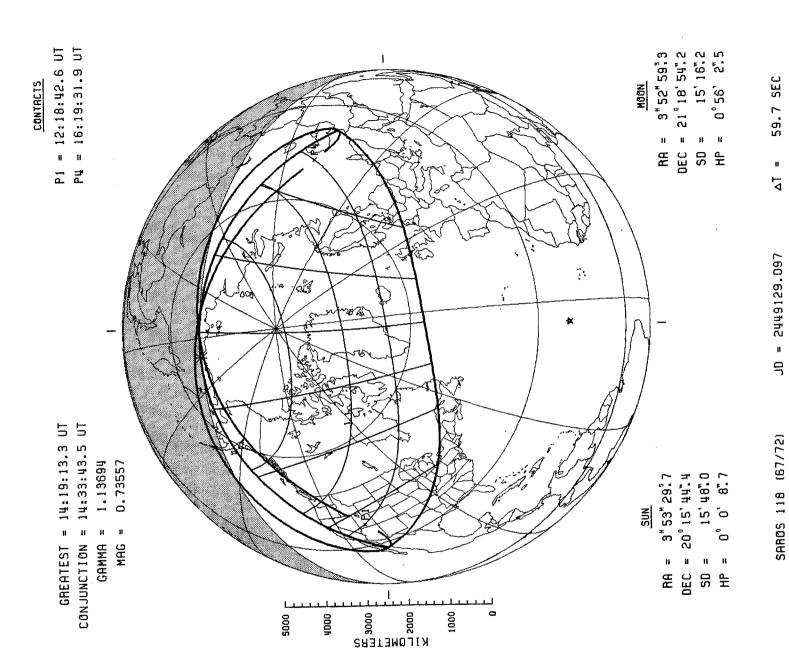
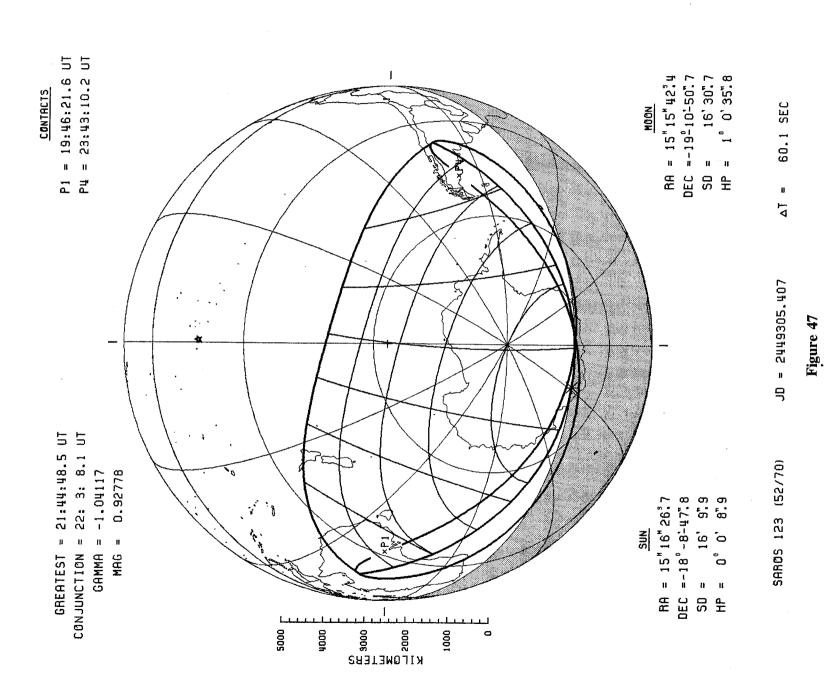


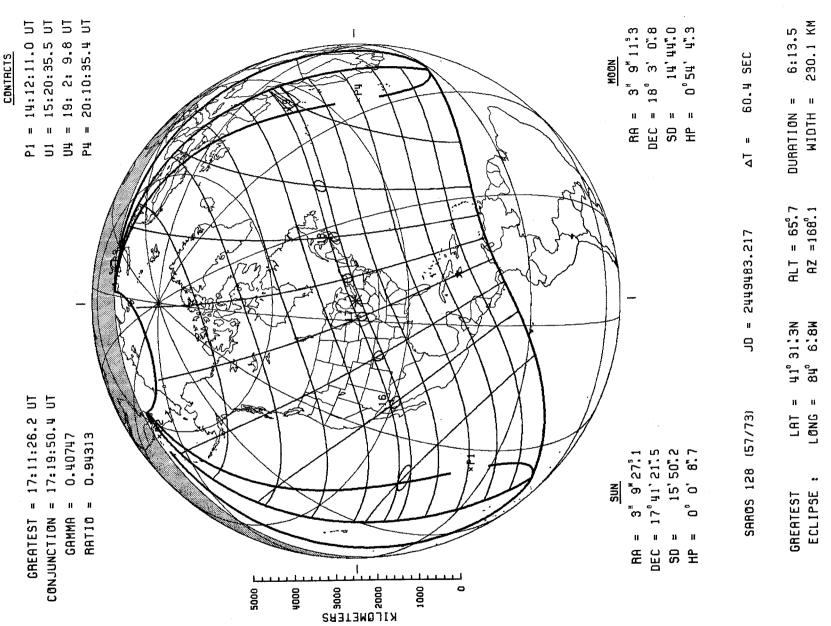
Figure 46

## 13 NOV SOLAR ECLIPSE PARTIAL

1993



159



## TOTAL SOLAR ECLIPSE - 3

1994

N0 N

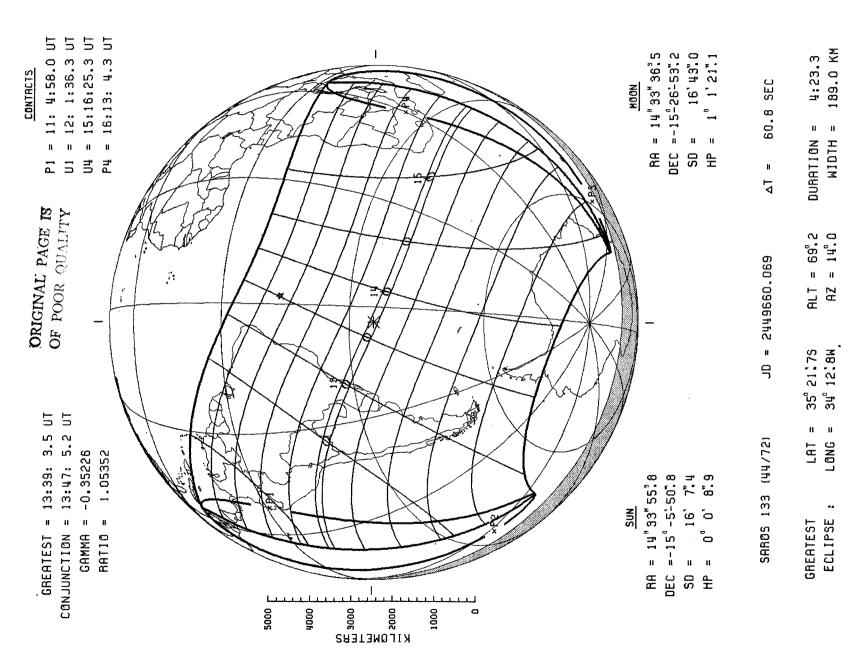


Figure 49 161

#### 1995 APR 29 **ECLIPSE** SOLAR ANNULAR

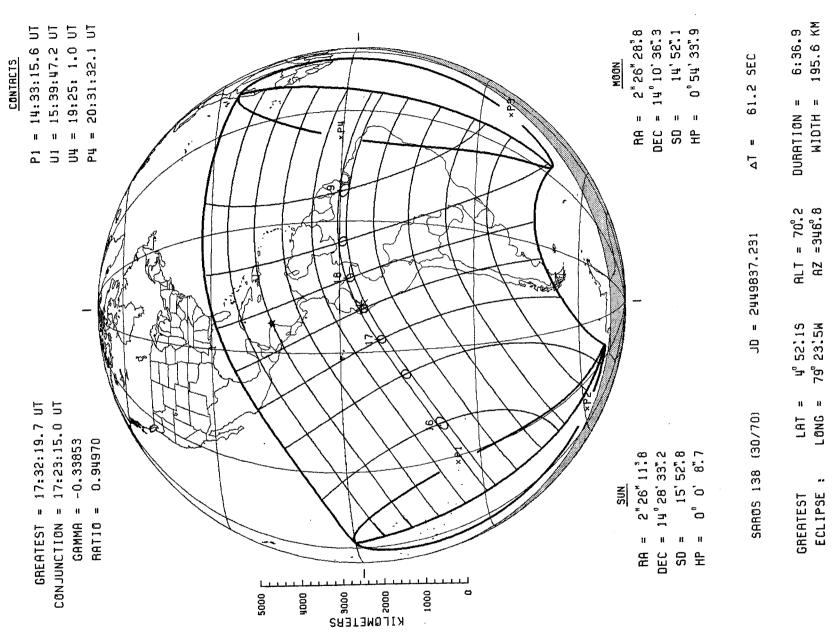


Figure 50 162

#### 1995 OCT 24 ŧ **ECLIPSE** SOLAR TOTAL

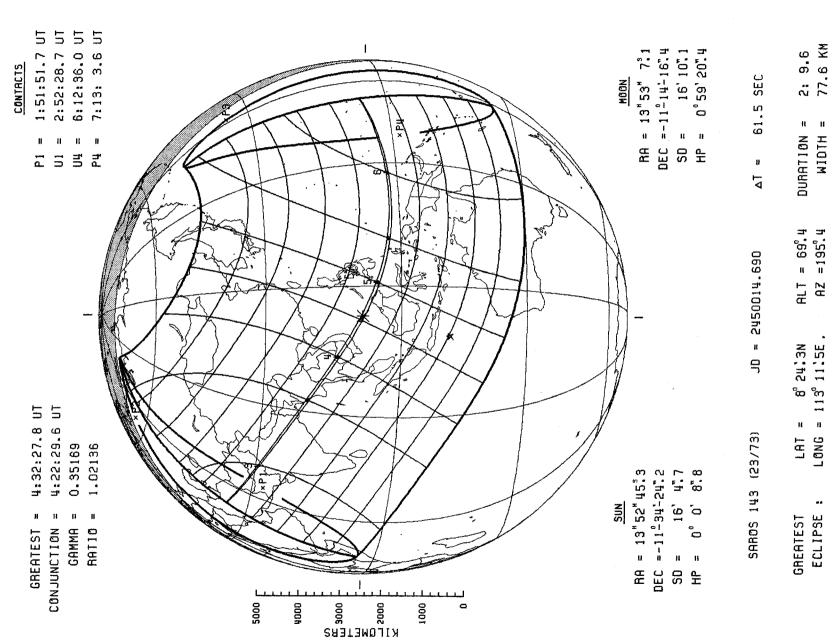
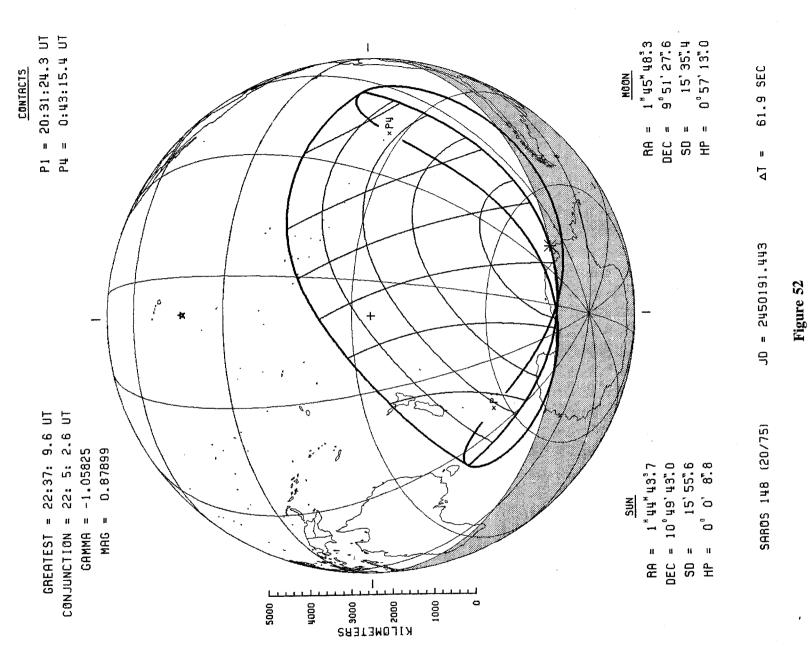


Figure 51 163

### 1996 APR 17 ı SOLAR ECLIPSE PARTIAL



#### 1996 OCT 12 ı **ECLIPSE** SOLAR PARTIAL

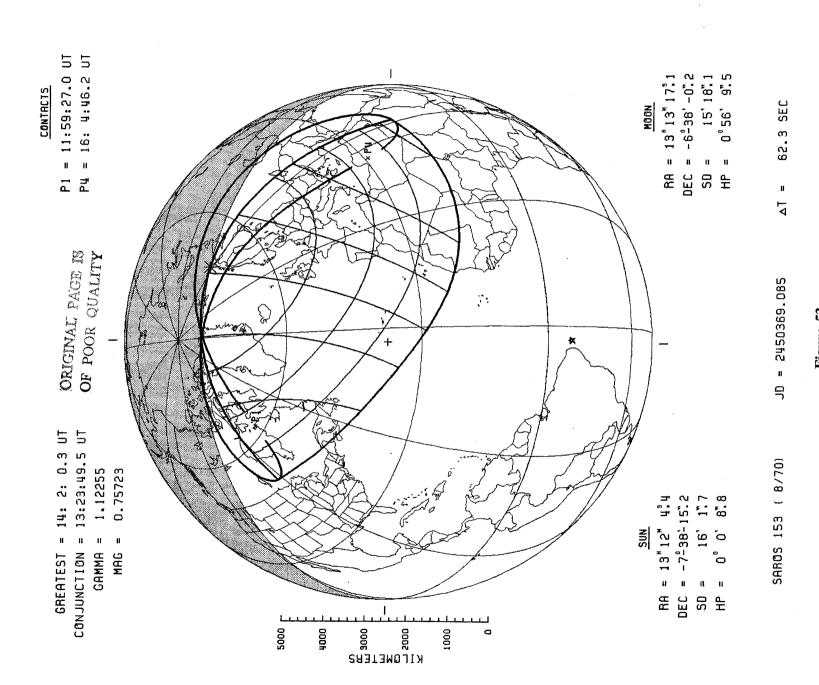


Figure 53

Figure 54 166

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### 1997 SEP N ŀ SOLAR ECLIPSE PARTIAL

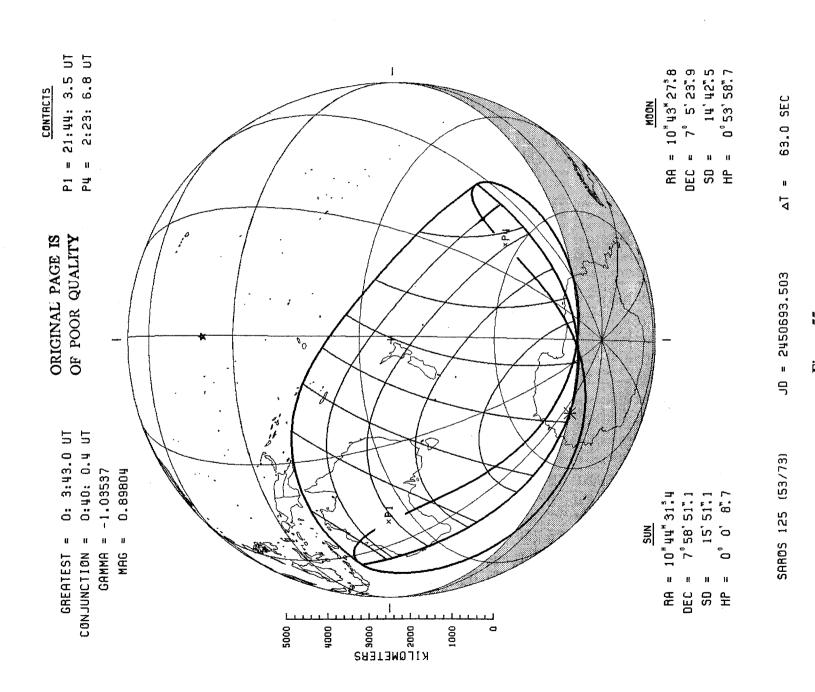
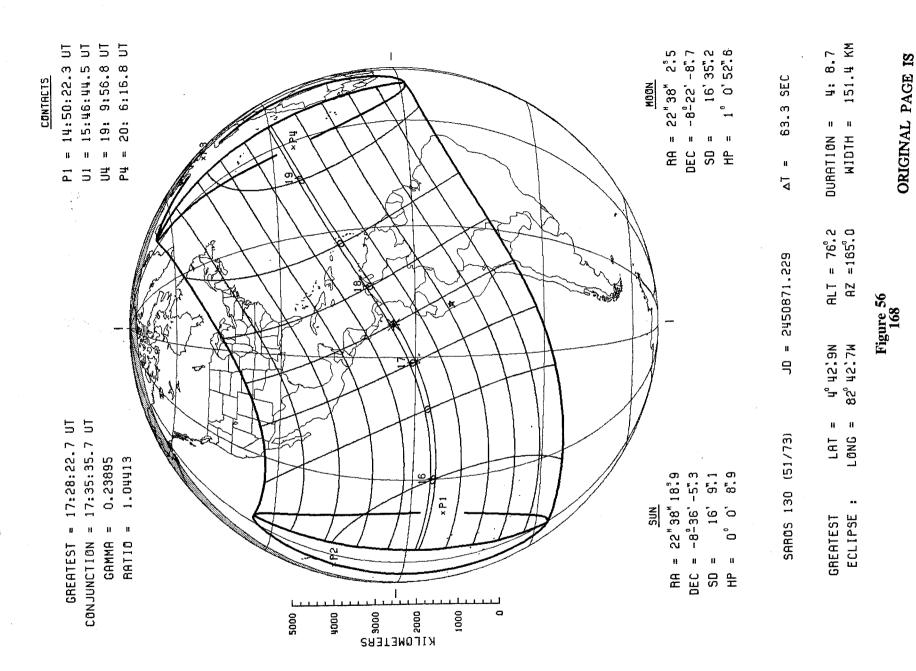


Figure 55



OF POOR QUALITY

## 22 RUG 1998 ı **ECLIPSE** SOLAR RNNULAR

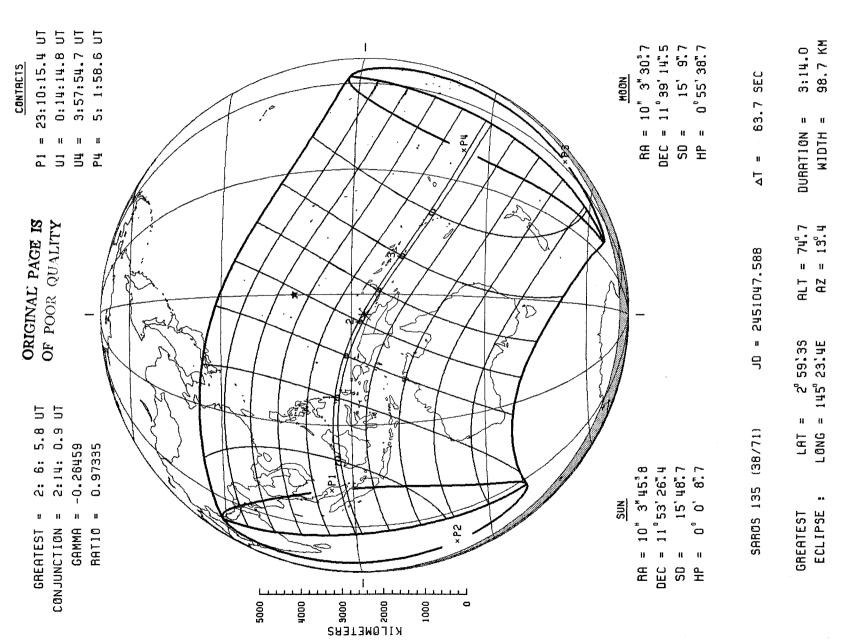


Figure 57 169

## FEB **ECLIPSE** SOLAR RNNULAR

1999

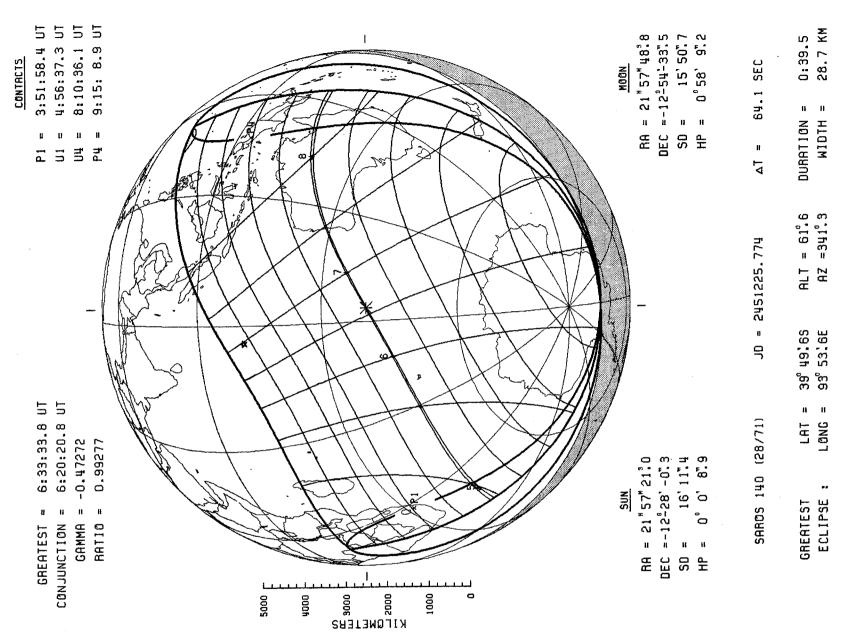


Figure 58 170

## 1999 AUG SOLAR ECLIPSE TOTAL

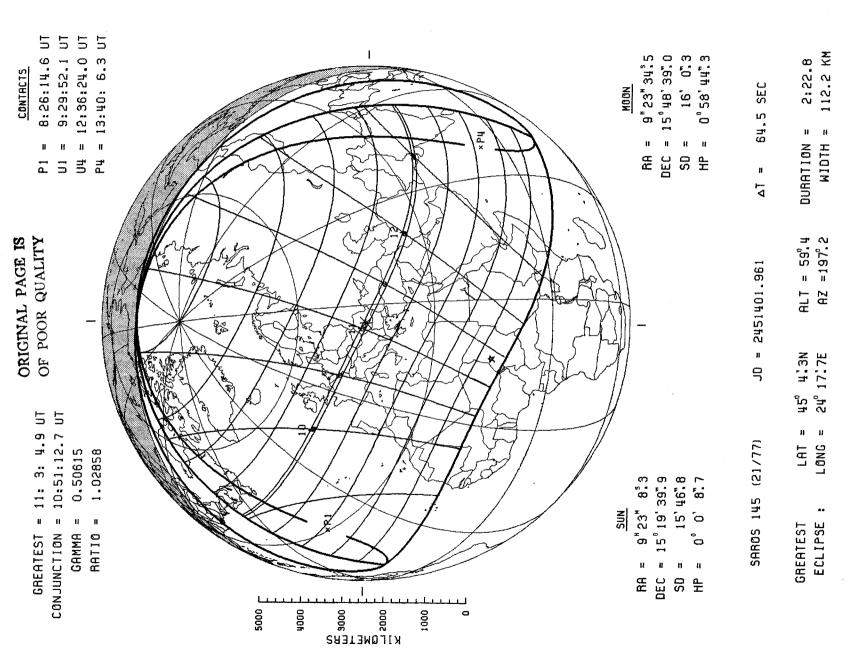
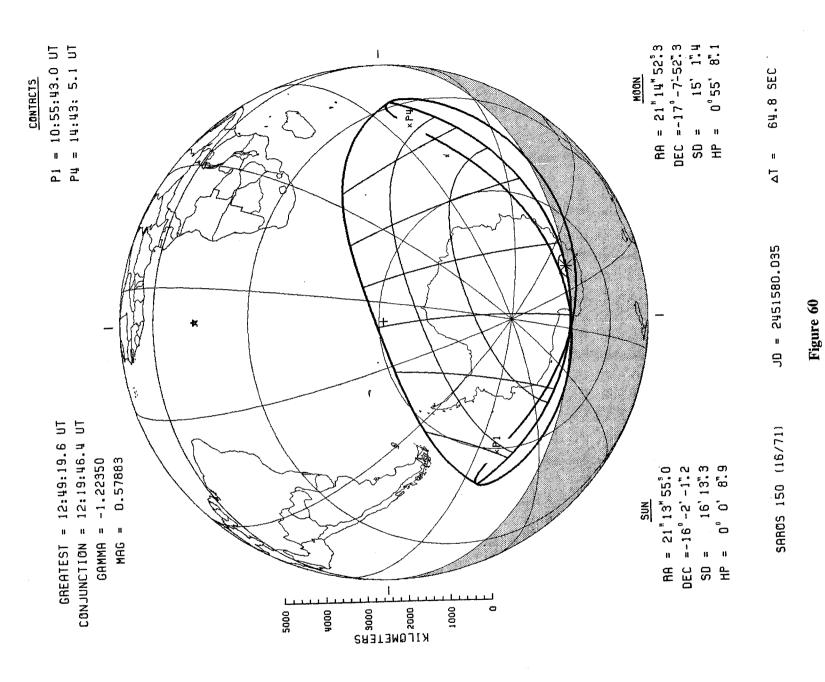


Figure 59 171

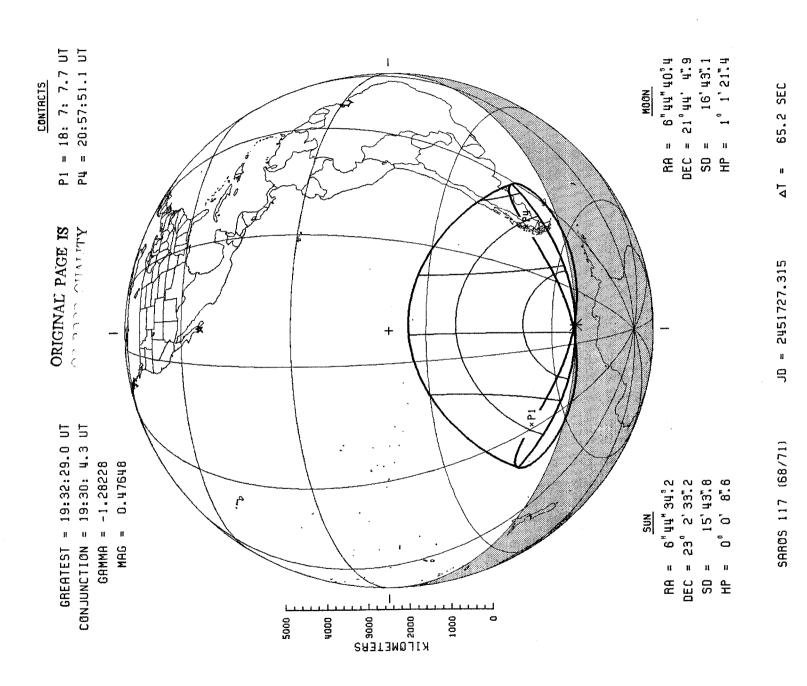
## FEB ហ SOLAR ECLIPSE PARTIAL

2000



173

Figure 61



2000

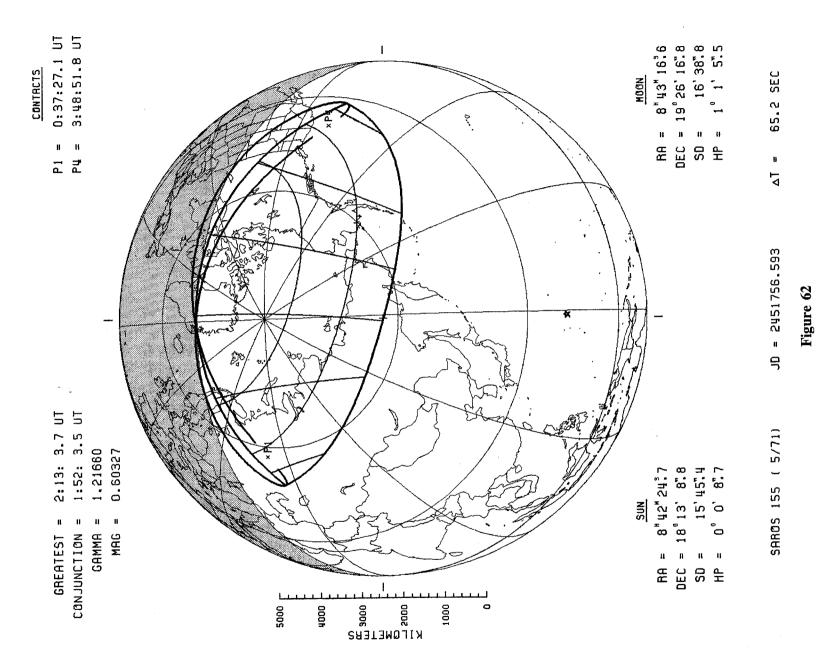
ı

**ECLIPSE** 

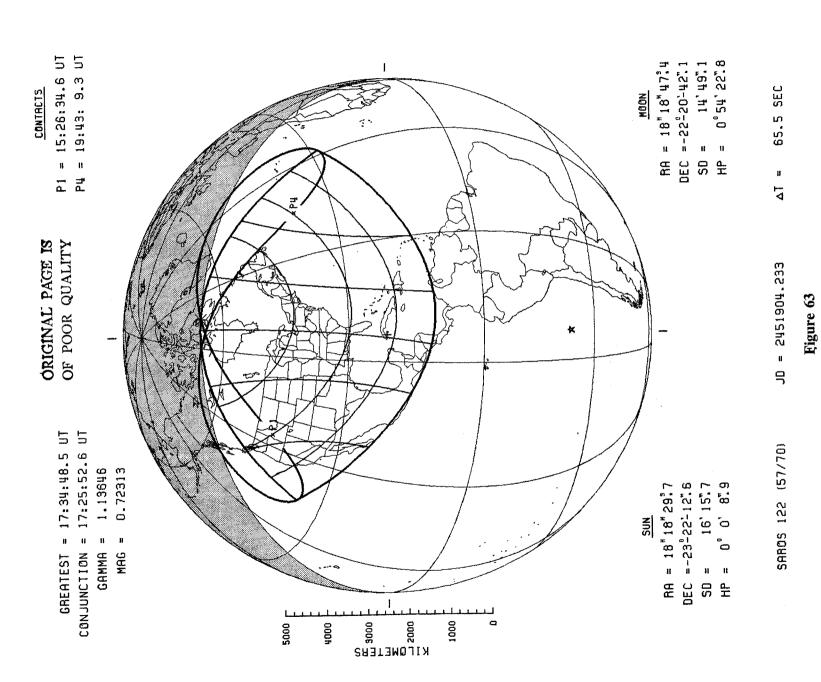
SOLAR

PARTIAL

## 2000 31 SOLAR ECLIPSE PARTIAL

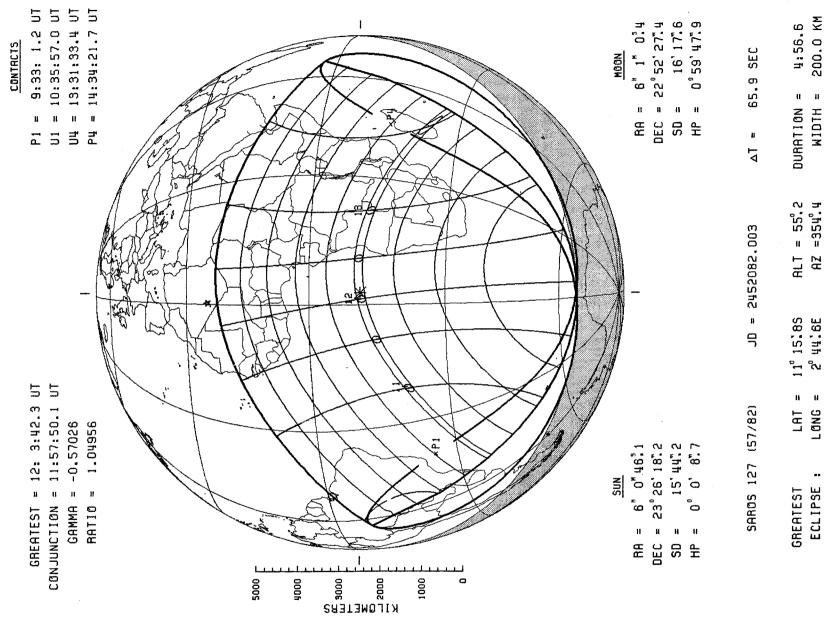


## 2000 DEC 25 SOLAR ECLIPSE PARTIAL



175

## 2001 NDC 21 SOLAR ECLIPSE TOTAL



#### 2001 OEC ゴニ ı **ECLIPSE** SOLAR ANNULAR

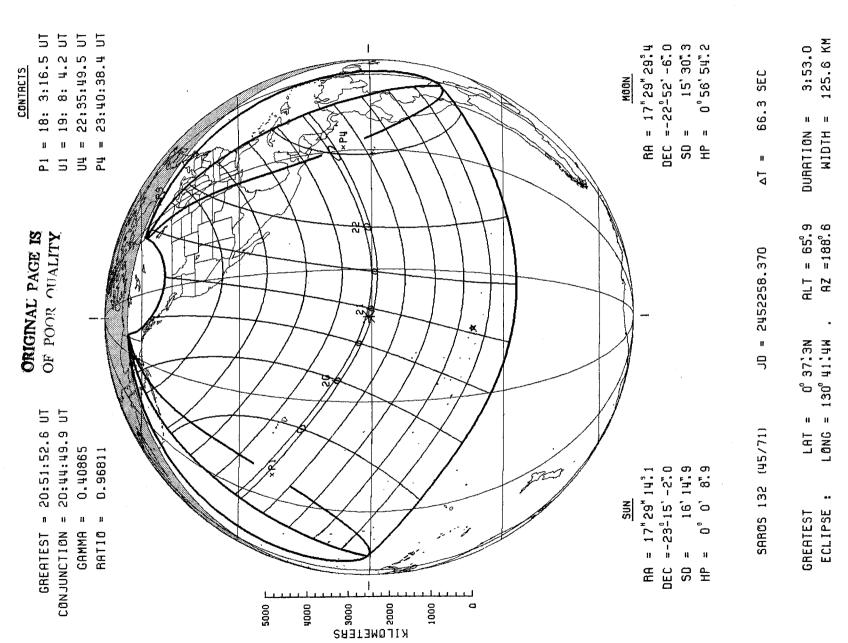


Figure 65 177

## 2002 NOC 10 ı ANNULAR SOLAR ECLIPSE

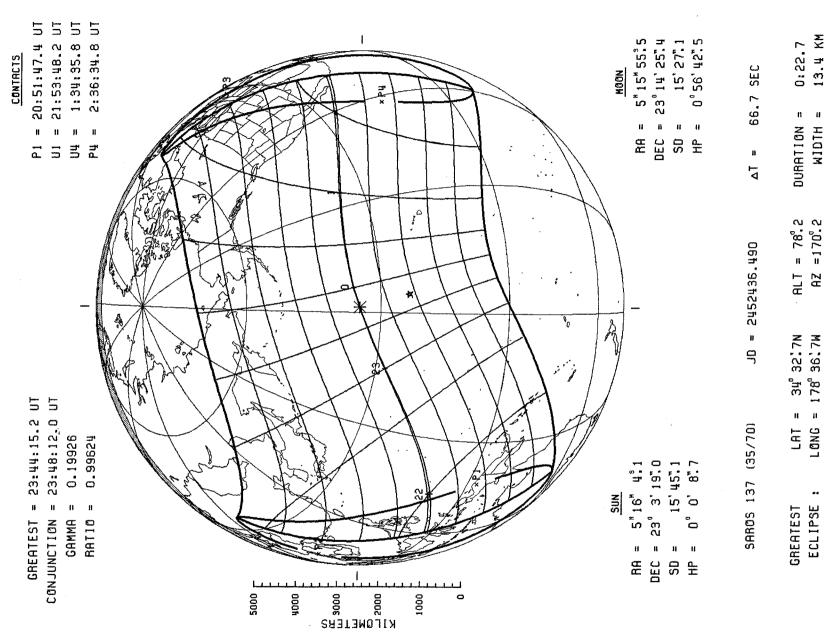


Figure 66 178

### OEC ゴ ł SOLAR ECLIPSE TOTAL

2002

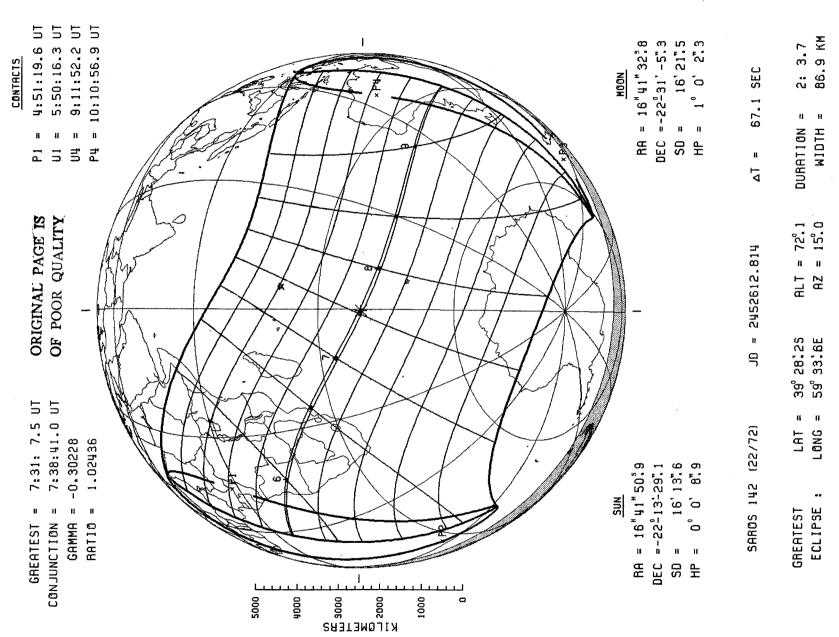


Figure 67

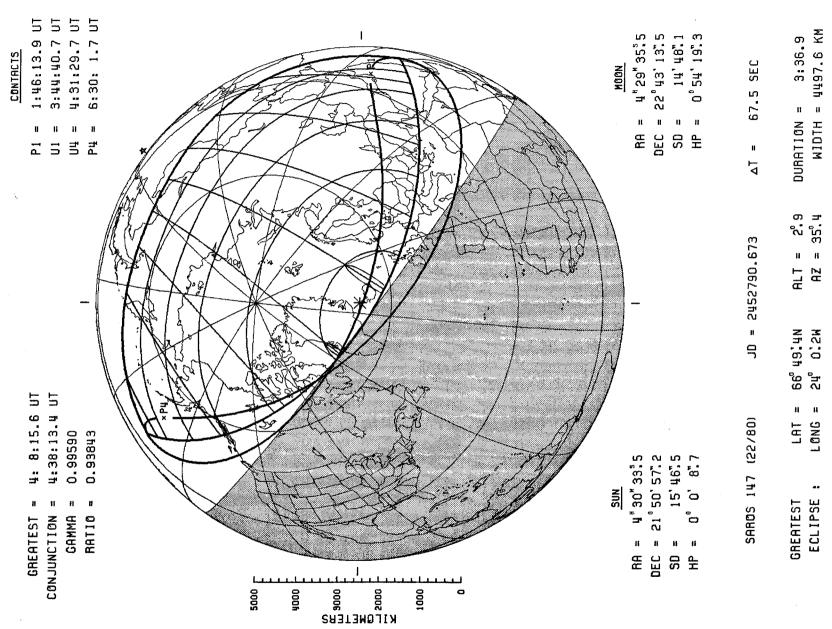


Figure 68 180

### 2003 NON 23 ı SOLAR ECLIPSE TOTAL

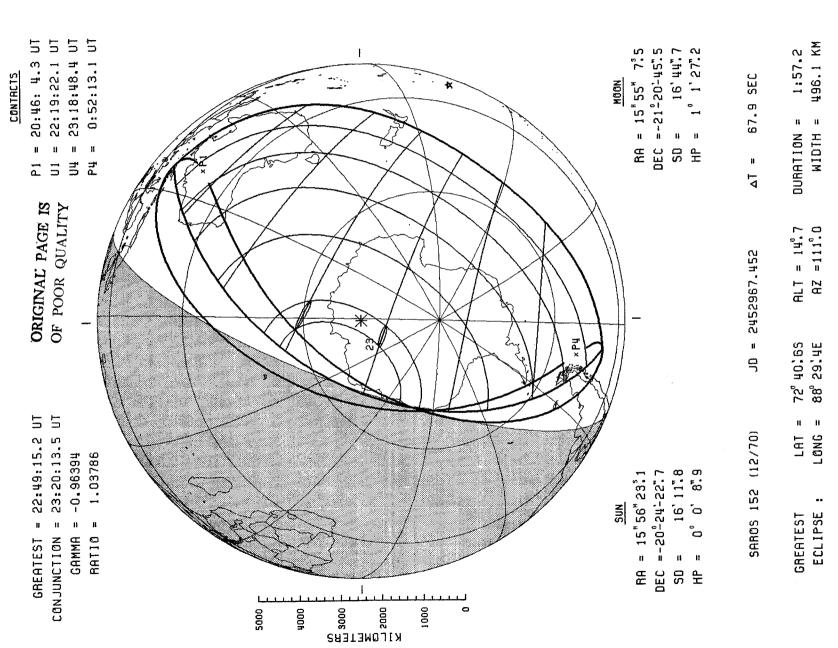
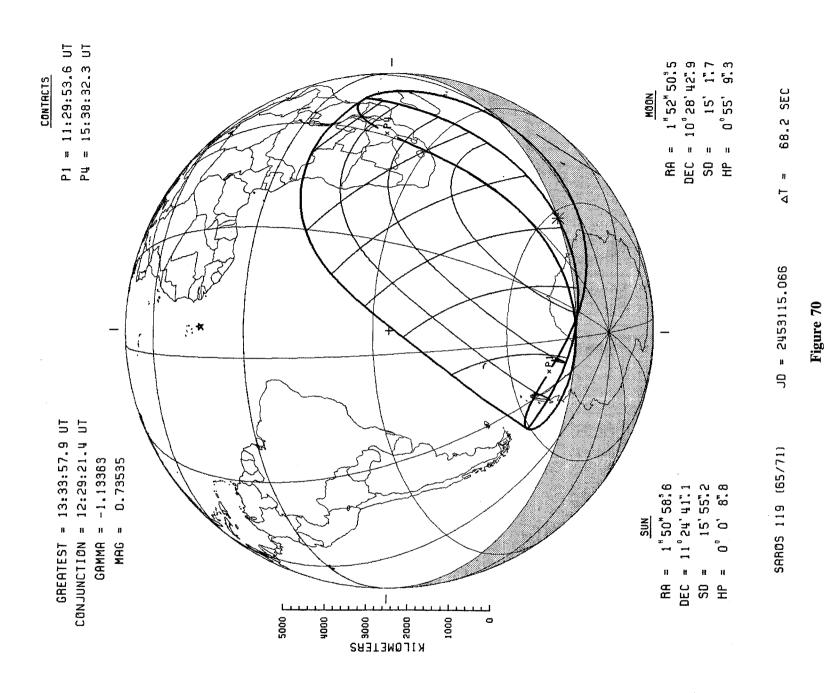


Figure 69

# PARTIAL SOLAR ECLIPSE -

2004

**19 APR** 



i.

#### 2004 OCT 11 1 **ECLIPSE** SOLAR **PARTIAL**

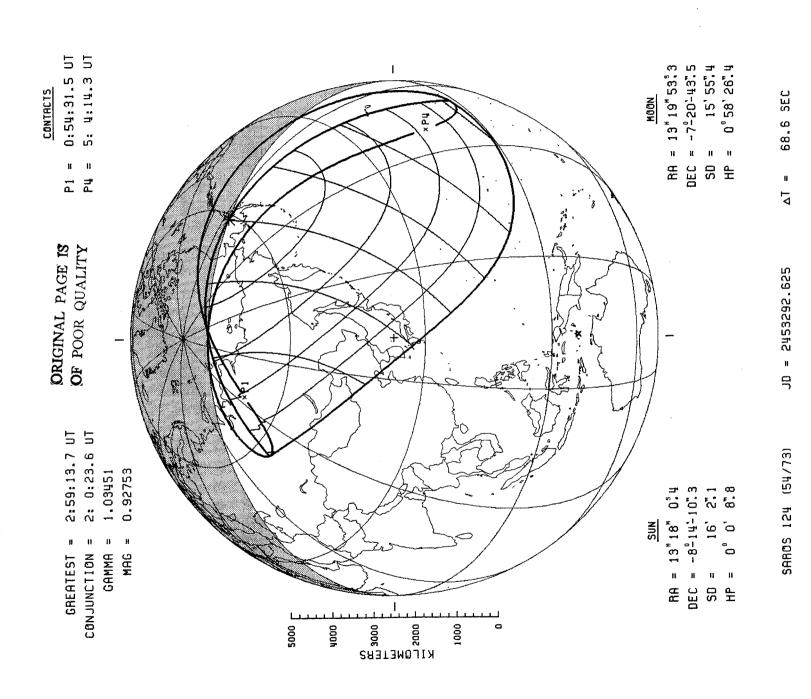


Figure 71

# ANN/IOT SOLAR ECLIPSE -

2005

APR

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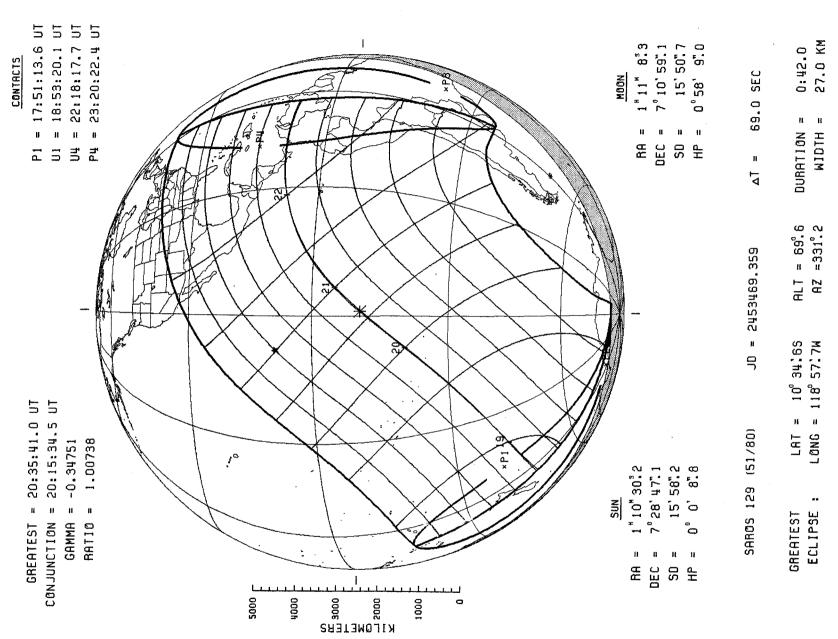


Figure 72 184

### 2005 OCT ന ı **ECLIPSE** SOLAR ANNULAR

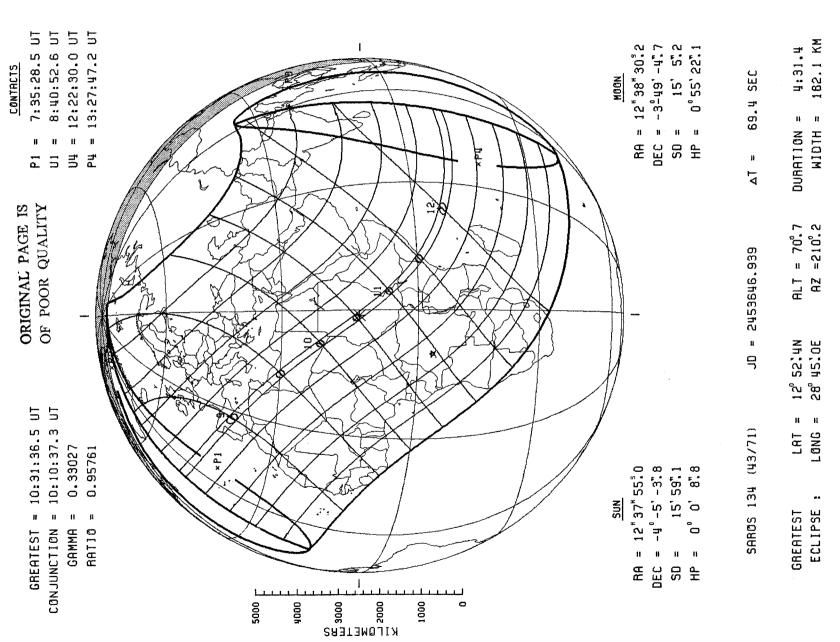


Figure 73

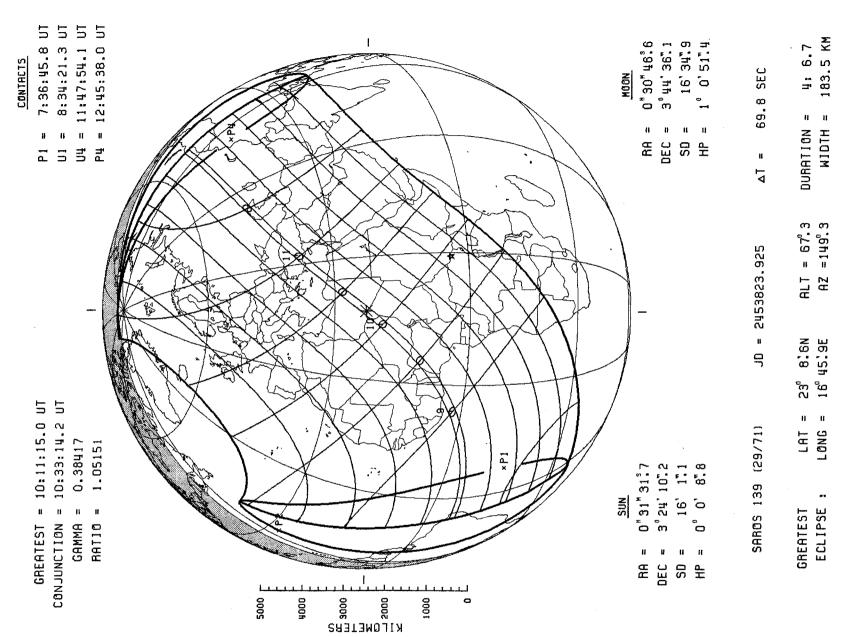


Figure 74 186

## 2006 SEP 22 ı SOLAR ECLIPSE ANNULAR

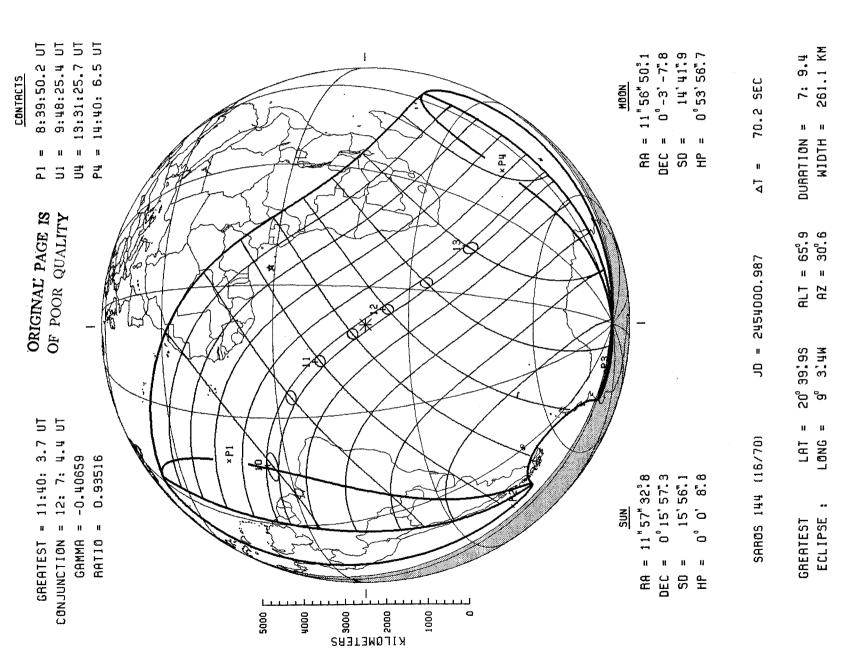
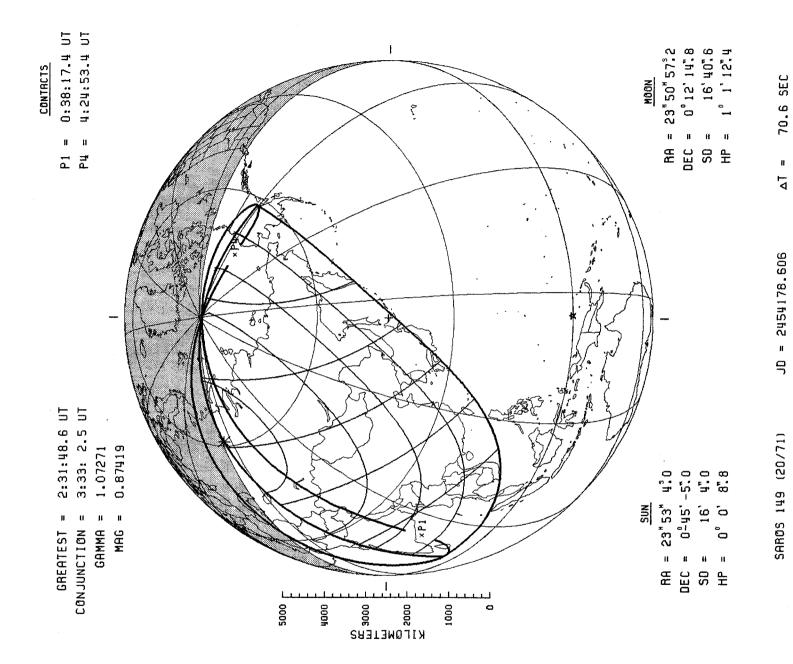


Figure 75

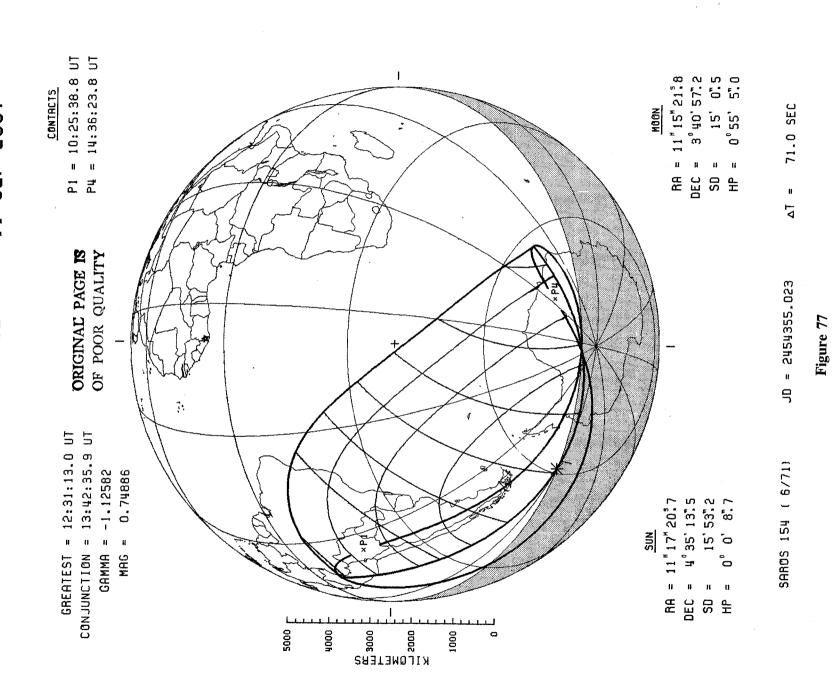
Figure 76

2007

19 MAR



# SEP 2007 ı SOLAR ECLIPSE PARTIAL



189

# ANNULAR SOLAR ECLIPSE -

2008

FEB

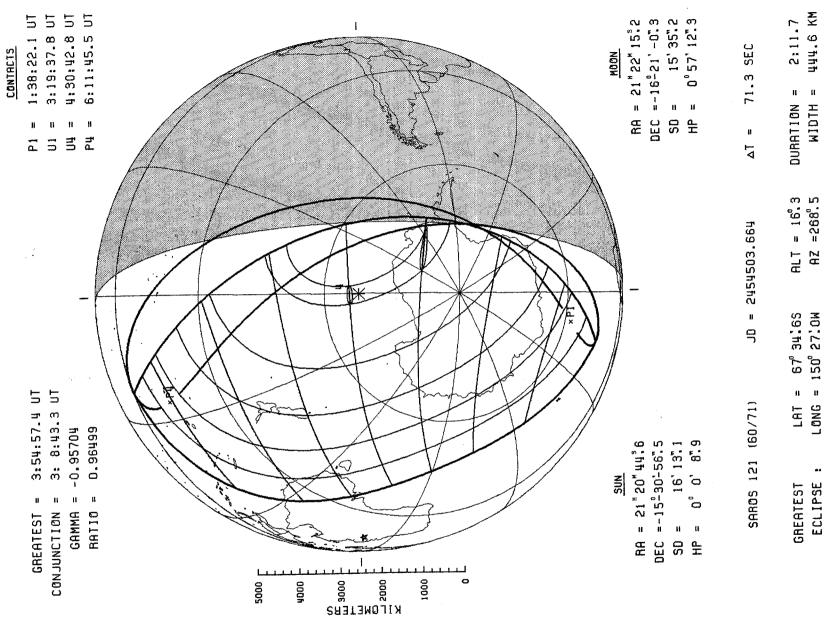


Figure 78

# 2008 AUG SOLAR ECLIPSE TOTAL

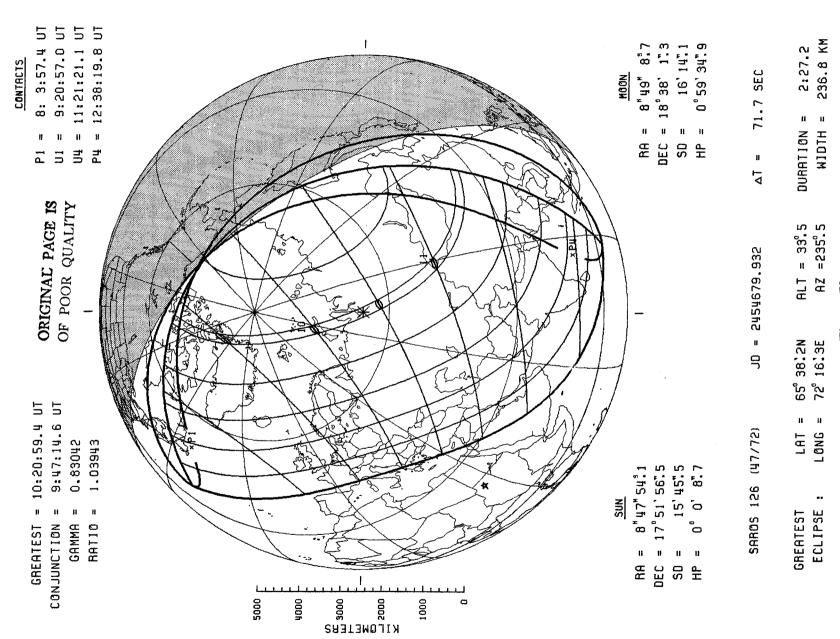


Figure 79

## 2009 JAN **5**8 **ECLIPSE** SOLAR ANNULAR

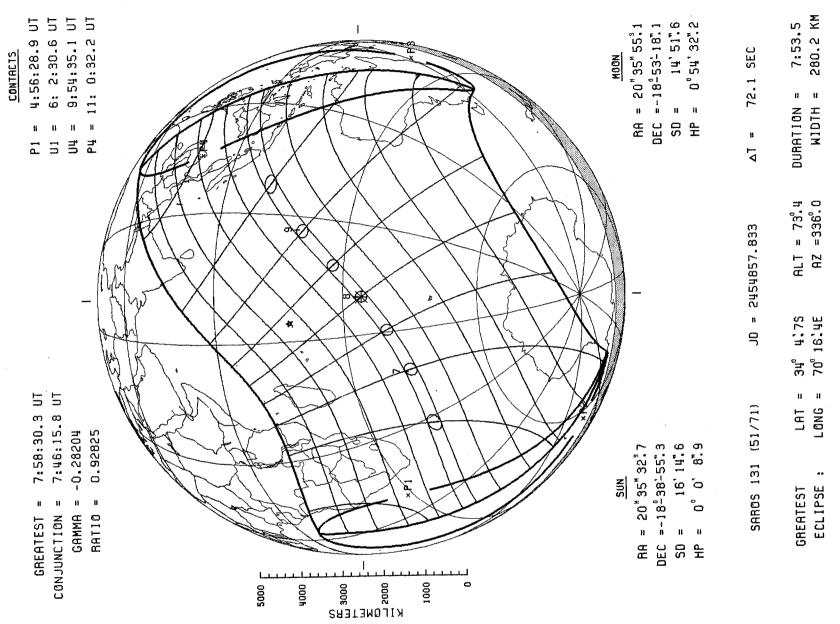


Figure 80 192

## 2009 JIT 22 ı TOTAL SOLAR ECLIPSE

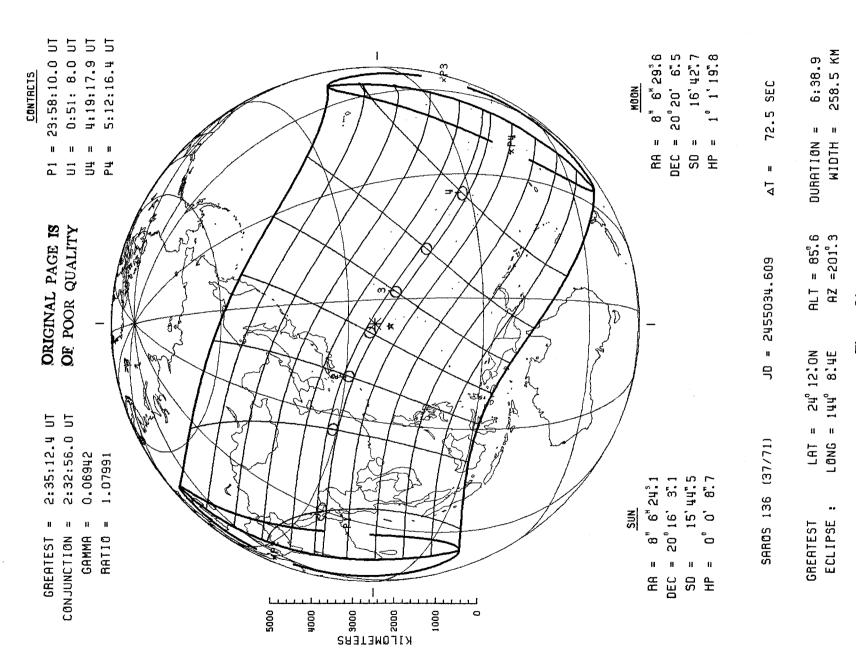


Figure 81 193

## 2010 JAN 15 ı ANNULAR SOLAR ECLIPSE

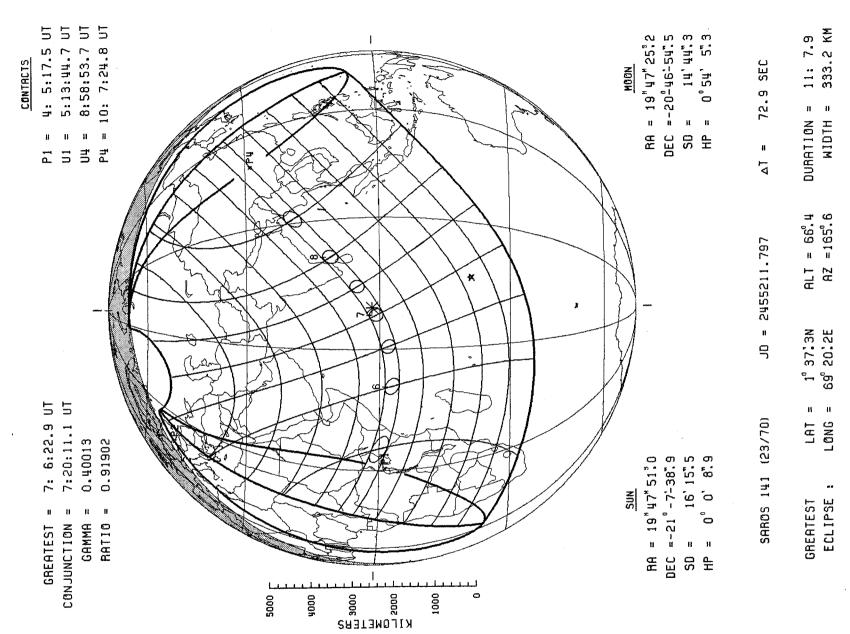


Figure 82 194

# 2010 ٦ TOTAL SOLAR ECLIPSE

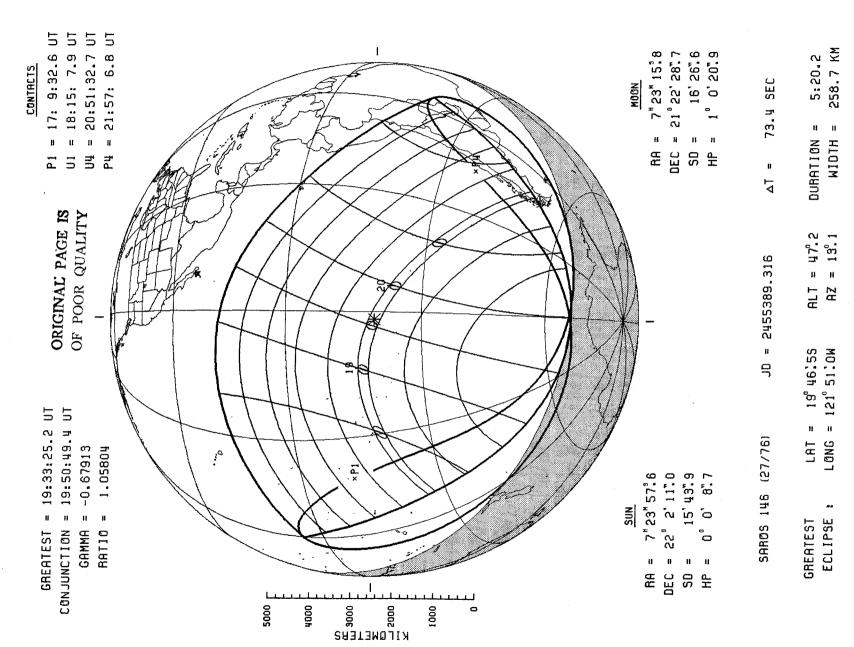
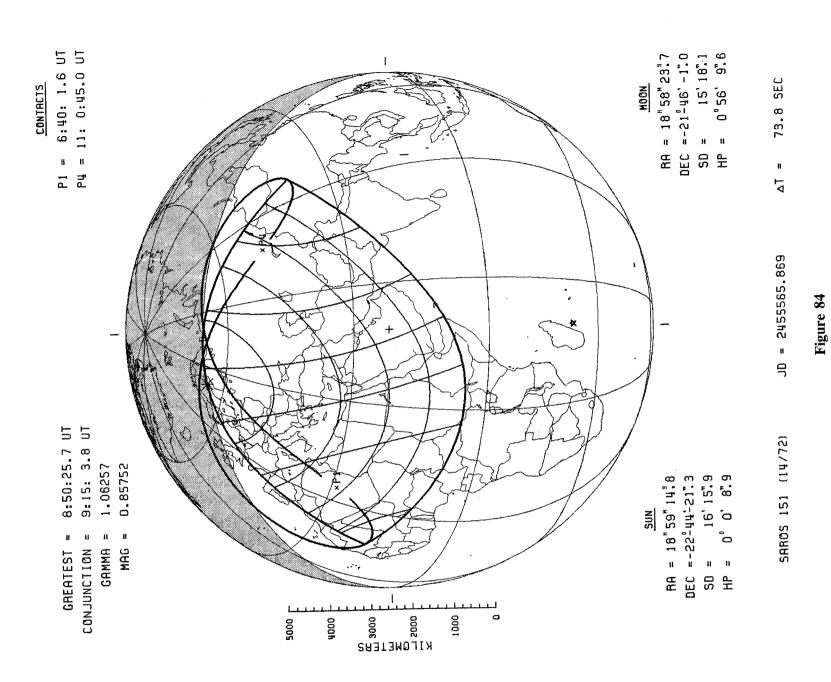


Figure 83

# ı SOLAR ECLIPSE PARTIAL

2011

A N N



# JUN 2011 SOLAR ECLIPSE PARTIAL

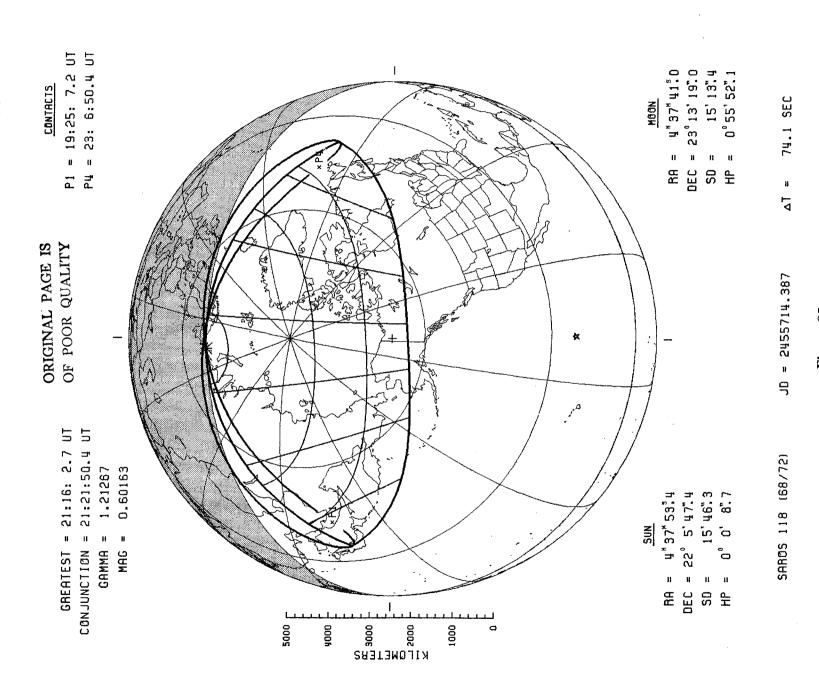
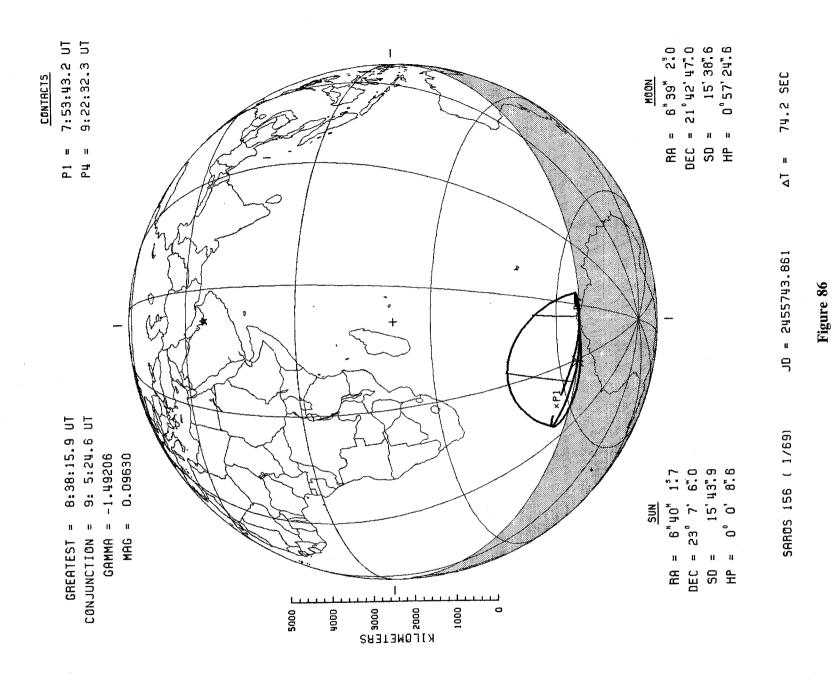


Figure 85

# PARTIAL SOLAR ECLIPSE -

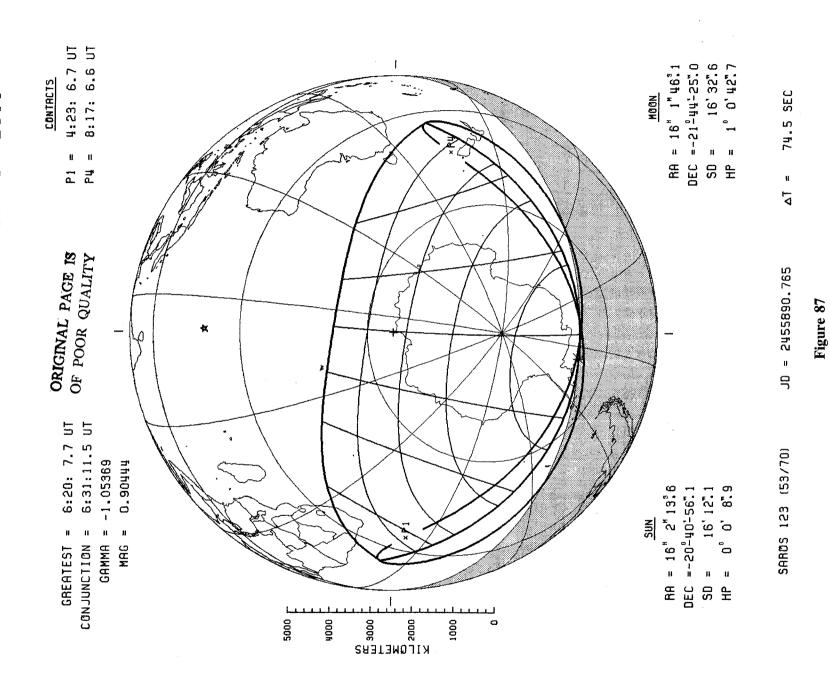
2011

JUL

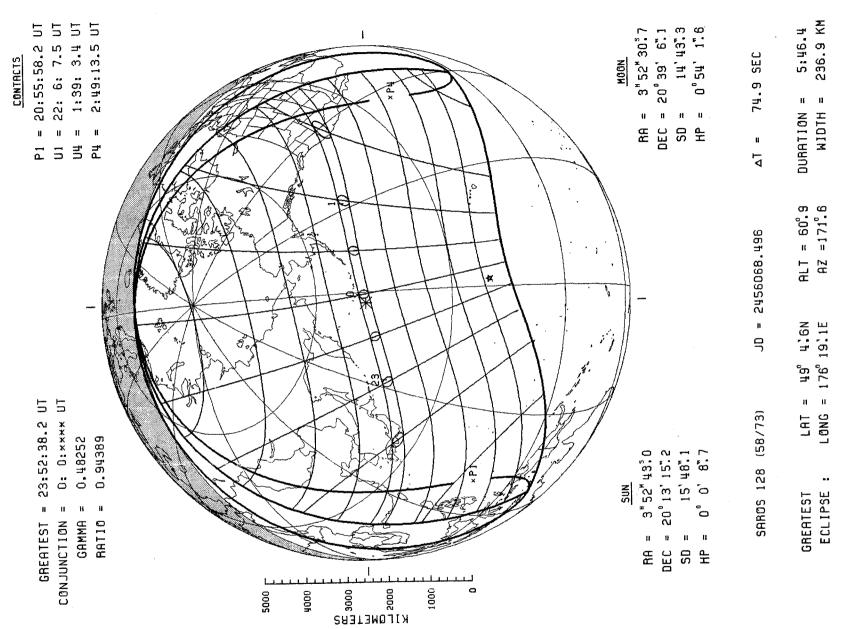


ı

## 2011 25 NOV I SOLAR ECLIPSE **PARTIAL**



# 2012 20 MAY **ECLIPSE** ANNULAR SOLAR



## 2012 13 NOV 1 SOLAR ECLIPSE TOTAL

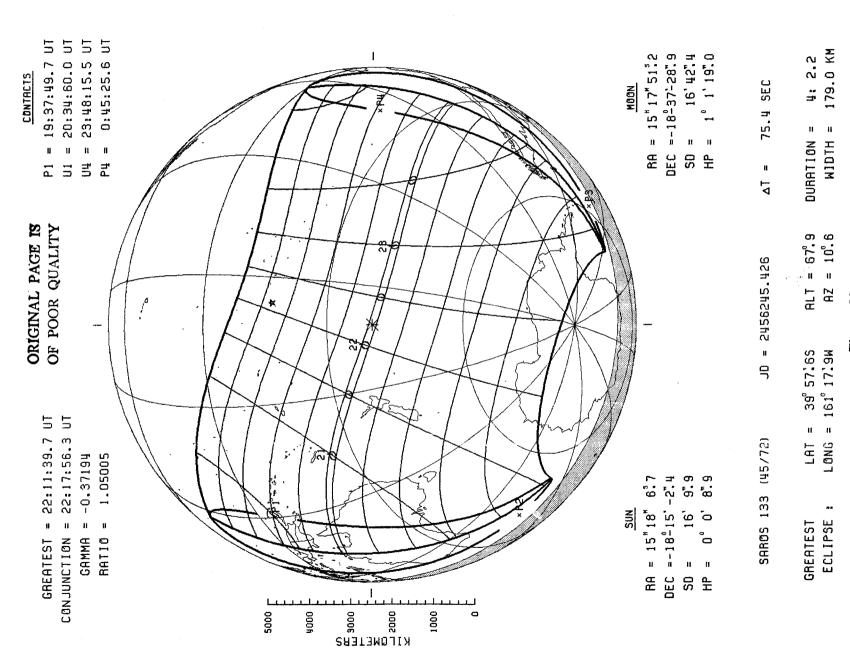
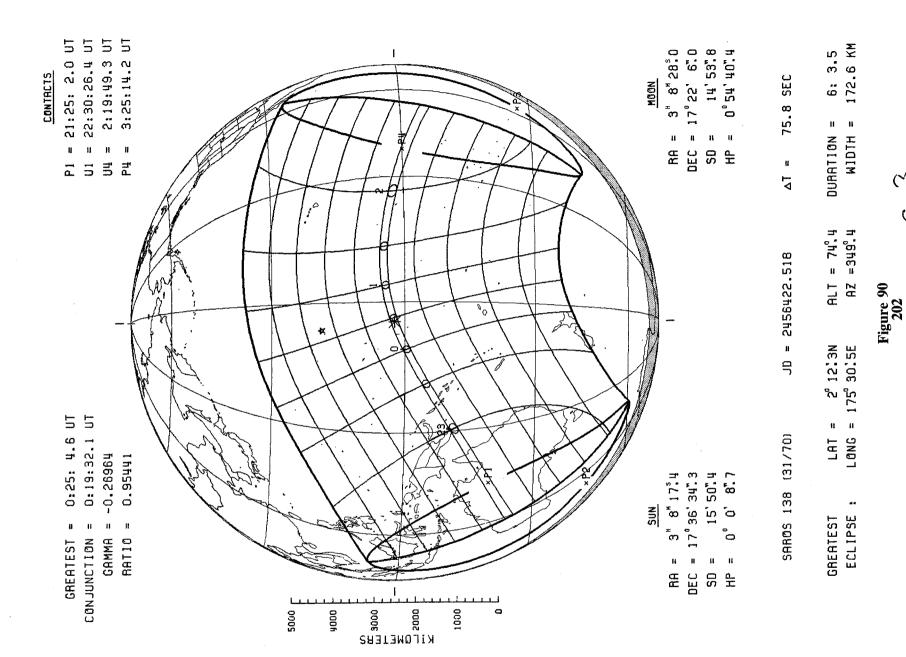


Figure 89 201



# ANN/TOT SOLAR ECLIPSE

2013

3 NOV

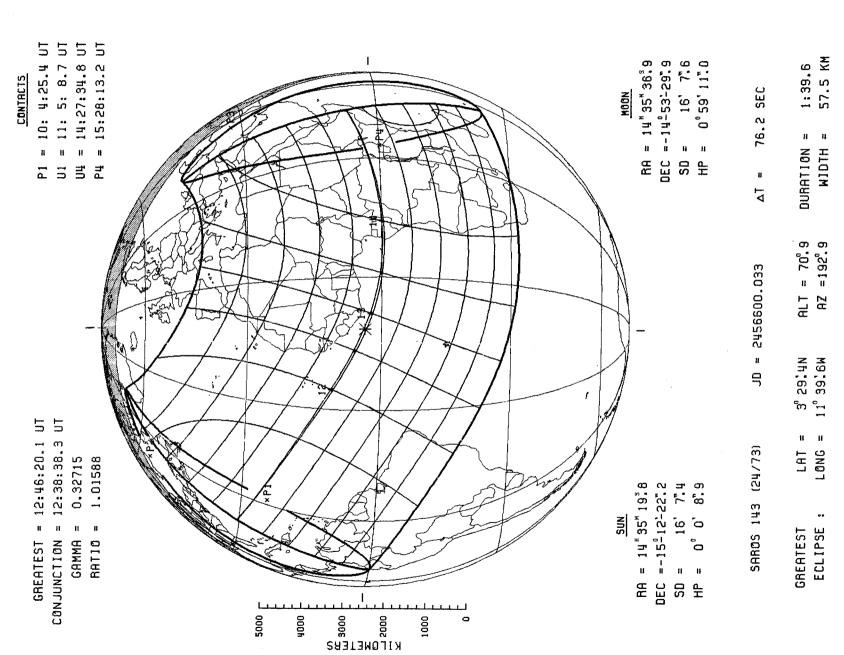
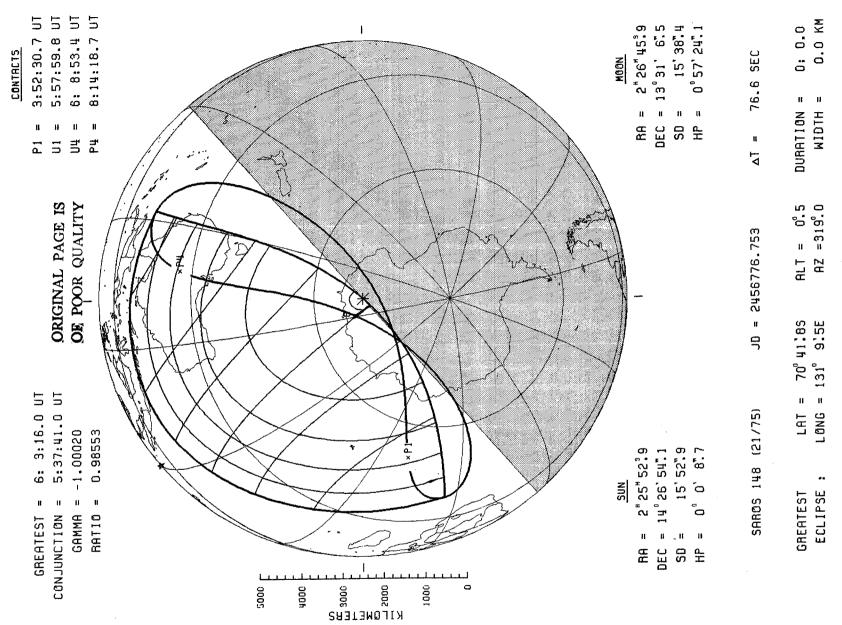


Figure 91 203

## 2014 APR 29 **ECLIPSE** SOLAR ANNULAR



### 2014 OCT 23 ı SOLAR ECLIPSE PARTIAL

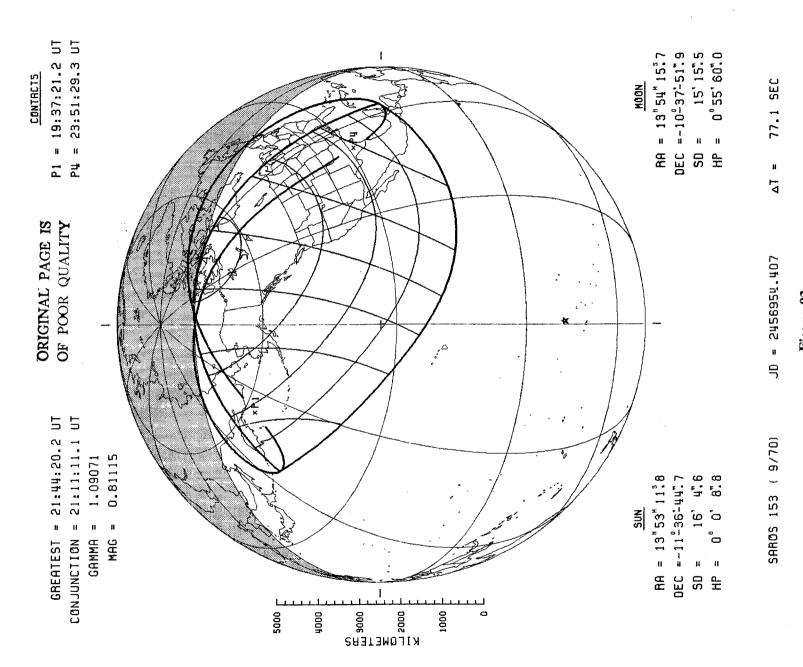
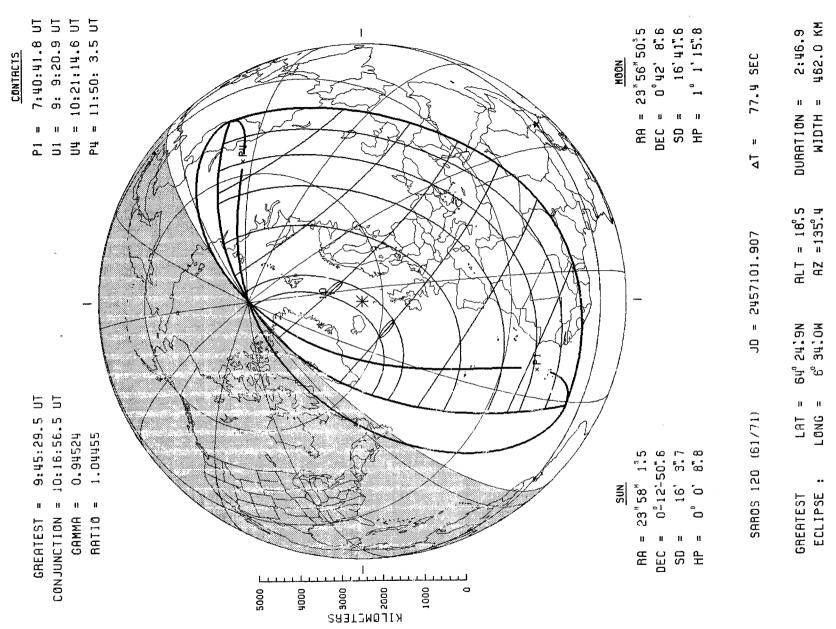
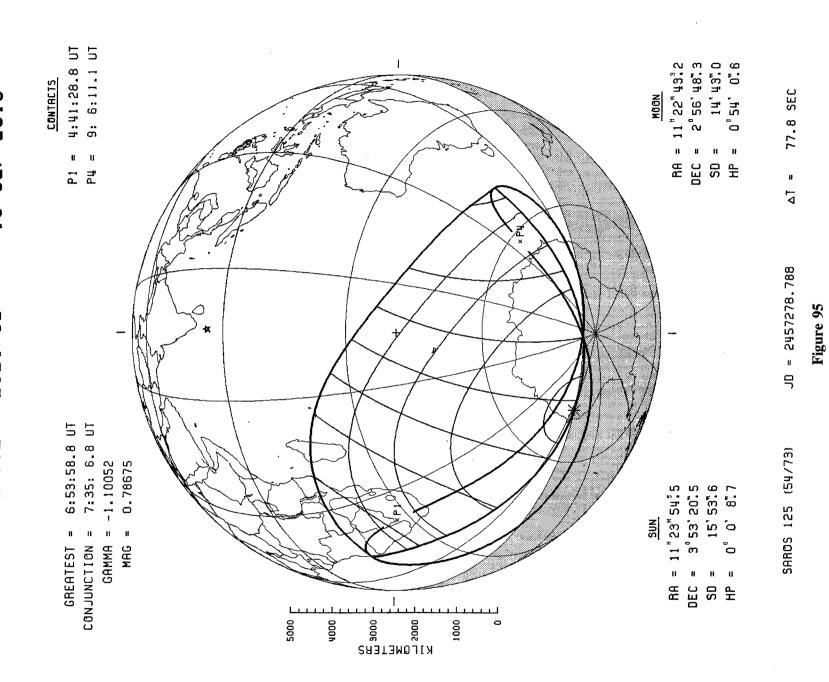


Figure 93

# 2015 20 MAR SOLAR ECLIPSE TOTAL



## 2015 SEP 13 SOLAR ECLIPSE **PARTIAL**



#### MAR တ ı **ECLIPSE** SOLAR TOTAL

2016

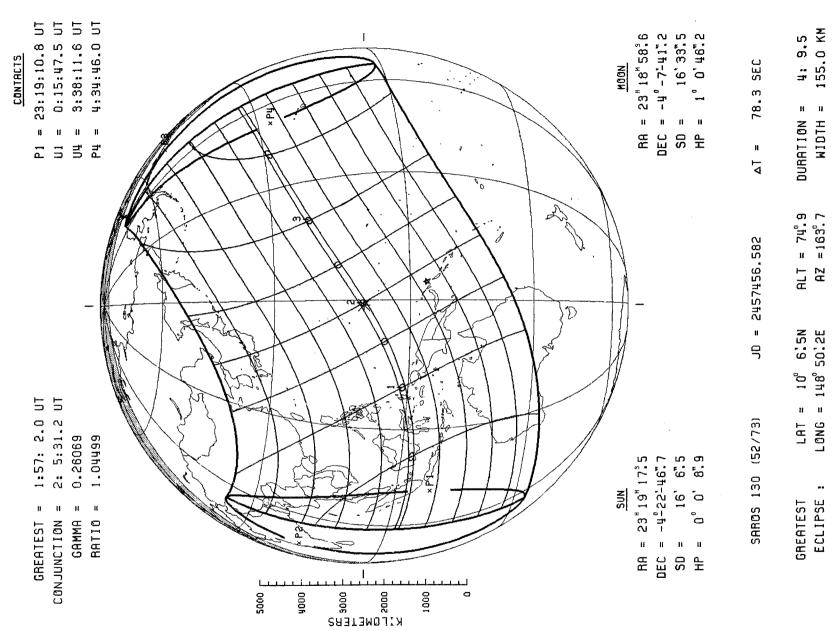


Figure 96 208

# 2016 SEP ı ANNULAR SOLAR ECLIPSE

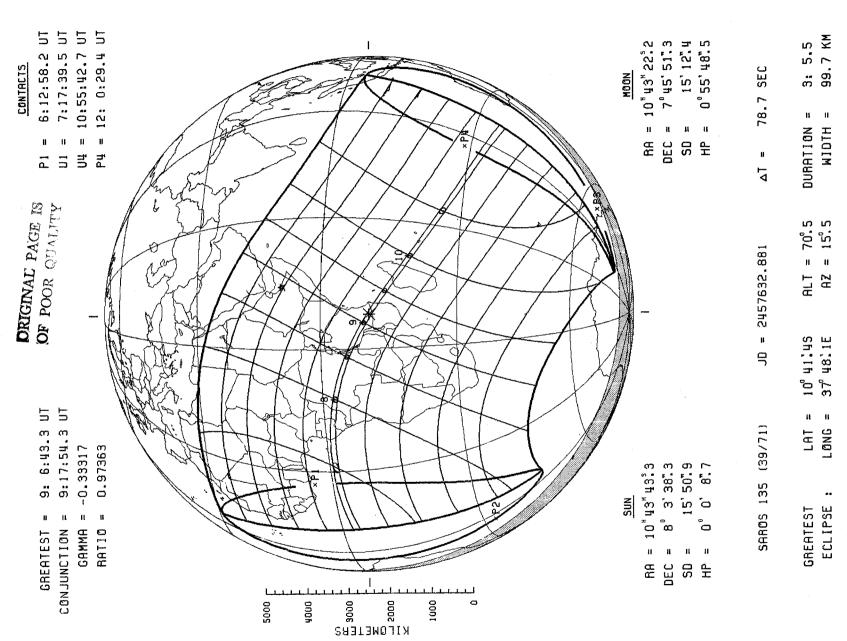


Figure 97 209

# FEB 2017 **5**8 ı ANNULAR SOLAR ECLIPSE

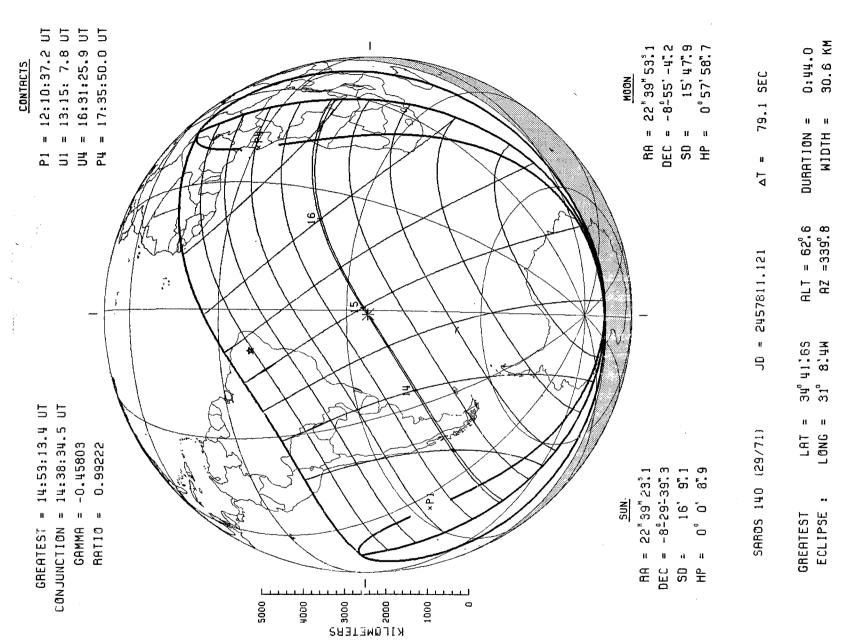


Figure 98 210

# 21 RUG 2017 TOTAL SOLAR ECLIPSE

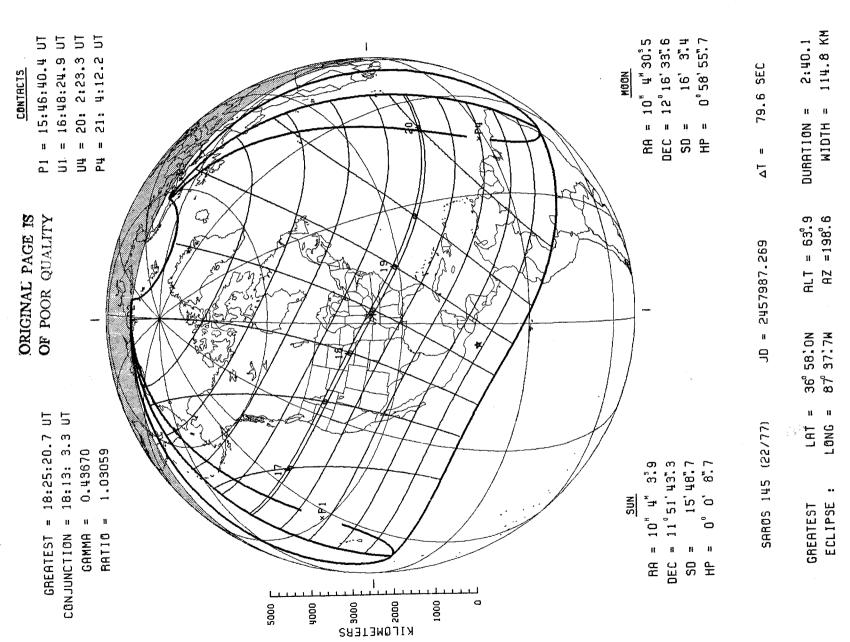


Figure 99

# PARTIAL SOLAR ECLIPSE -

2018

FEB

15

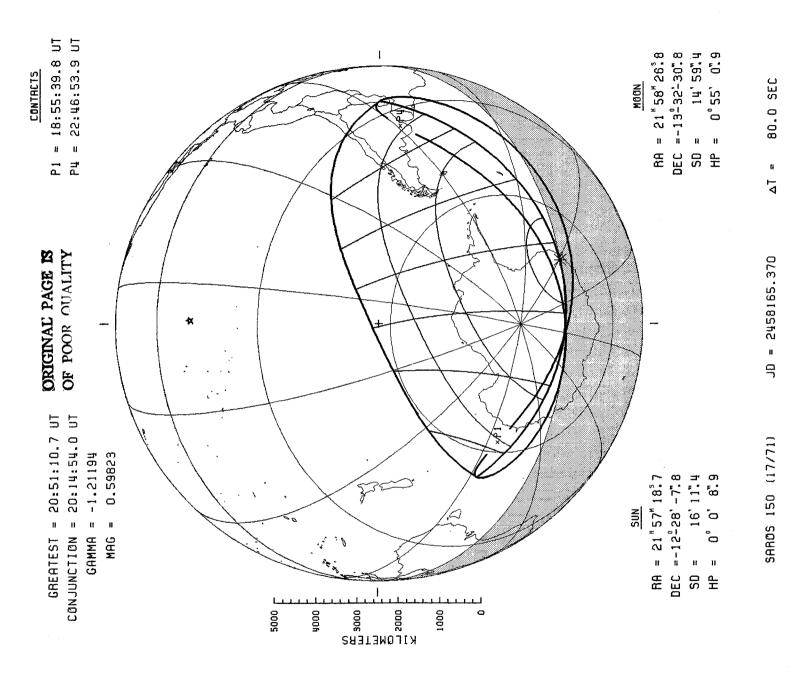
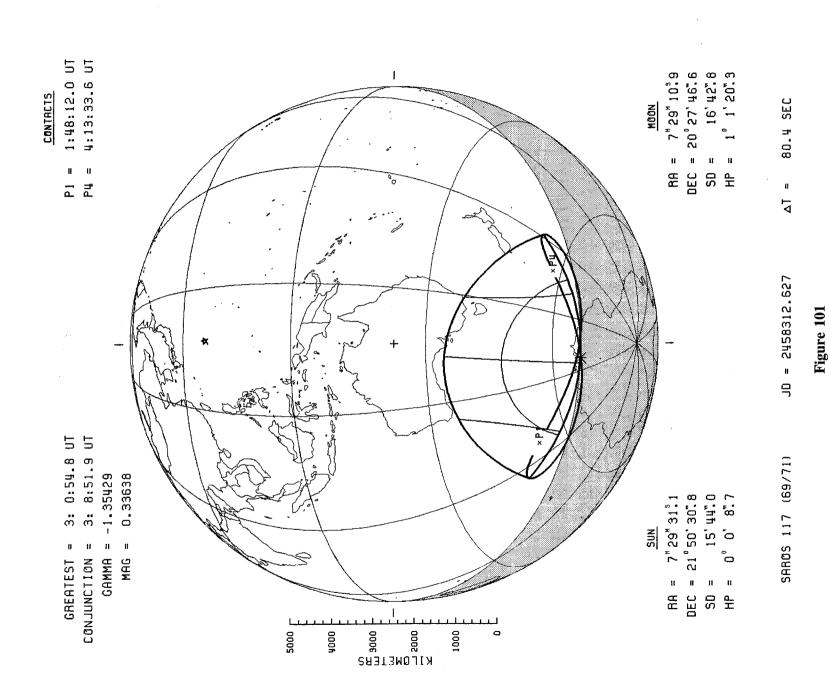
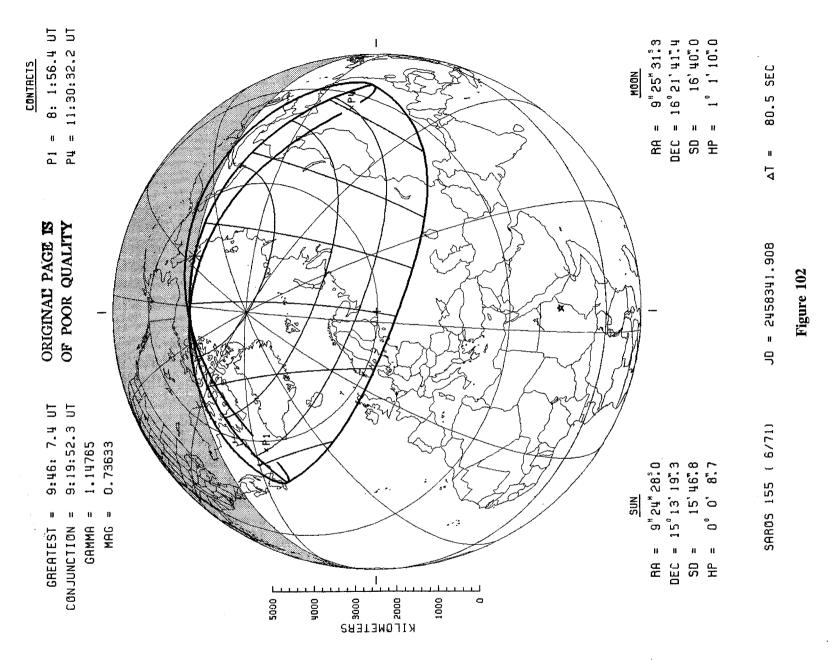


Figure 100

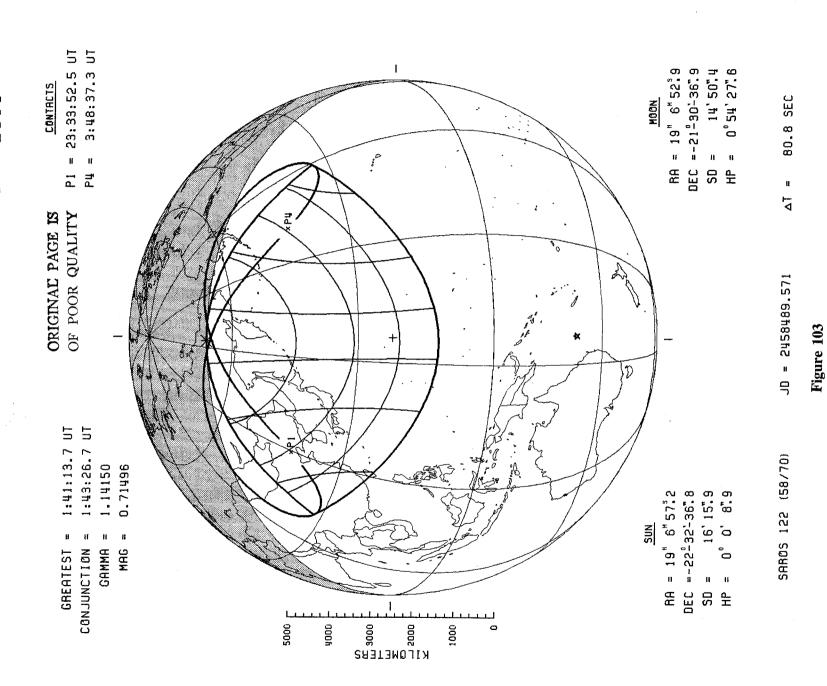
### SOLAR ECLIPSE PARTIAL



### AUG ı **ECLIPSE** SOLAR PARTIAL



### 2019 JAN 9 SOLAR ECLIPSE PARTIAL



215

# TOTAL SOLAR ECLIPSE - 2 JUL

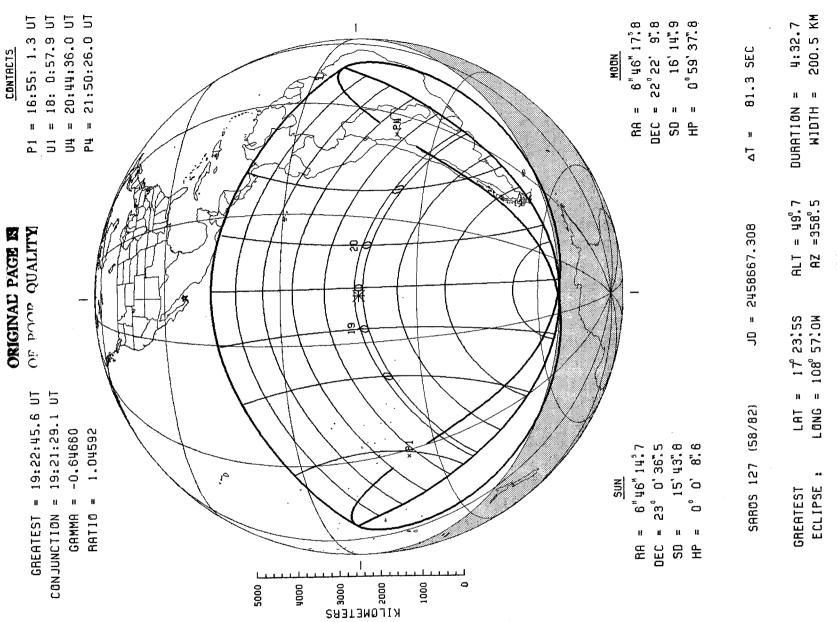


Figure 104 216

#### 2019 DEC **5**8 ı **ECLIPSE** SOLAR ANNULAR

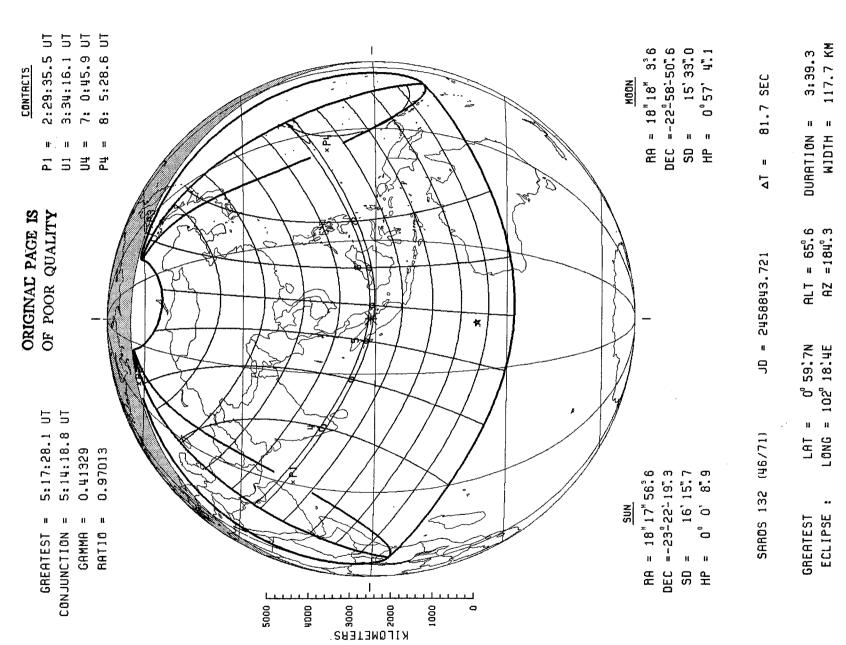


Figure 105 217

### 2020 N D C 21 **ECLIPSE** SOLAR RNNULAR

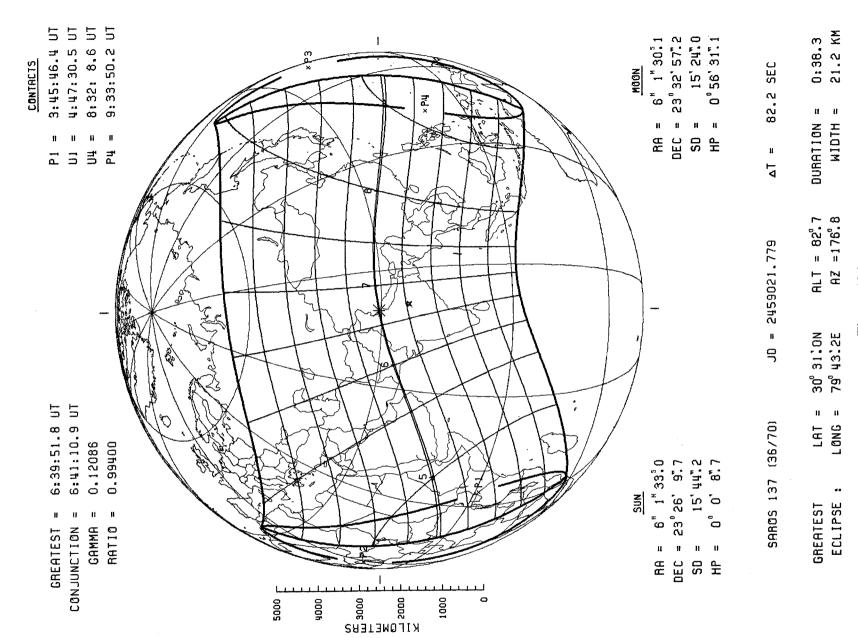


Figure 106 218

### 2020 DEC ゴ ı SOLAR ECLIPSE TOTAL

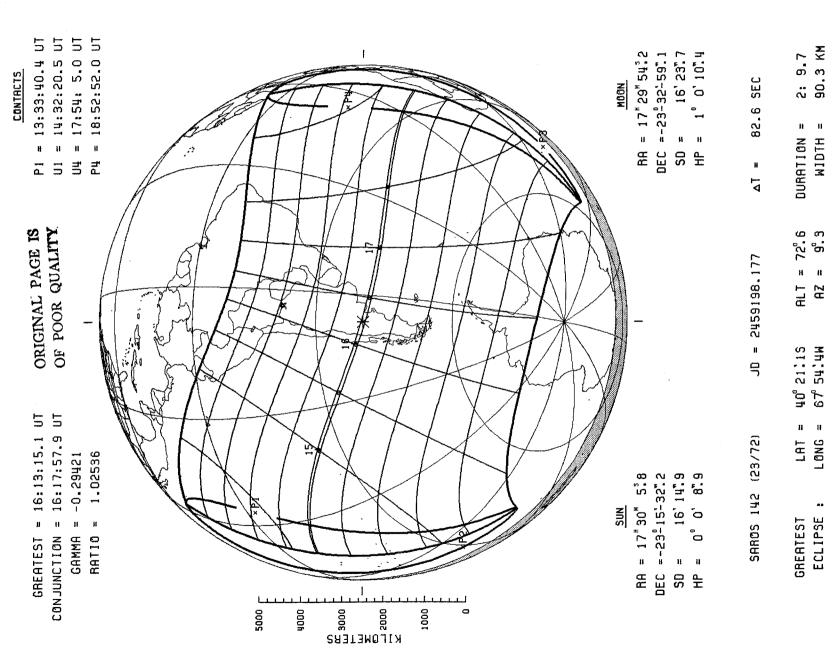
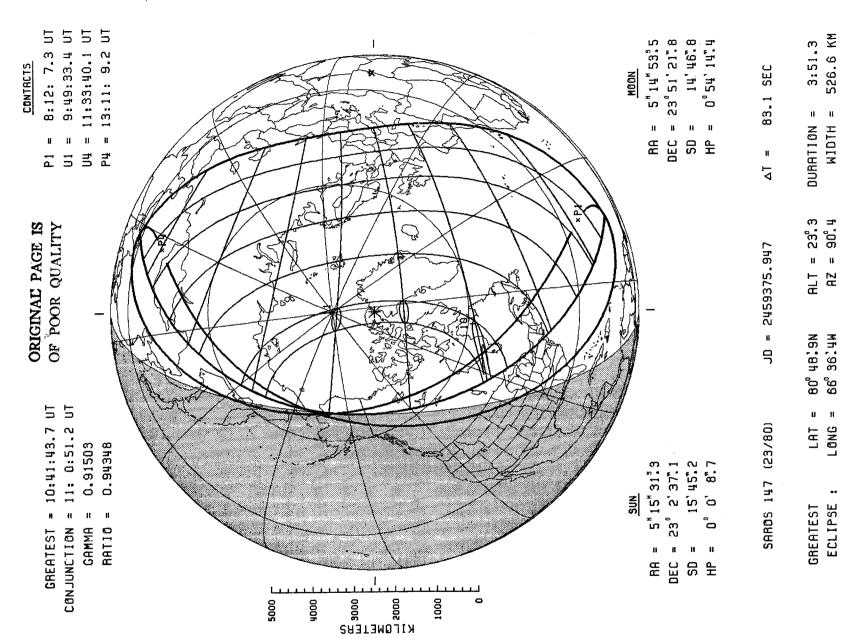


Figure 107

### JUN 2021 10 **ECLIPSE** SOLAR ANNULAR



### DEC 2021 SOLAR ECLIPSE TOTAL

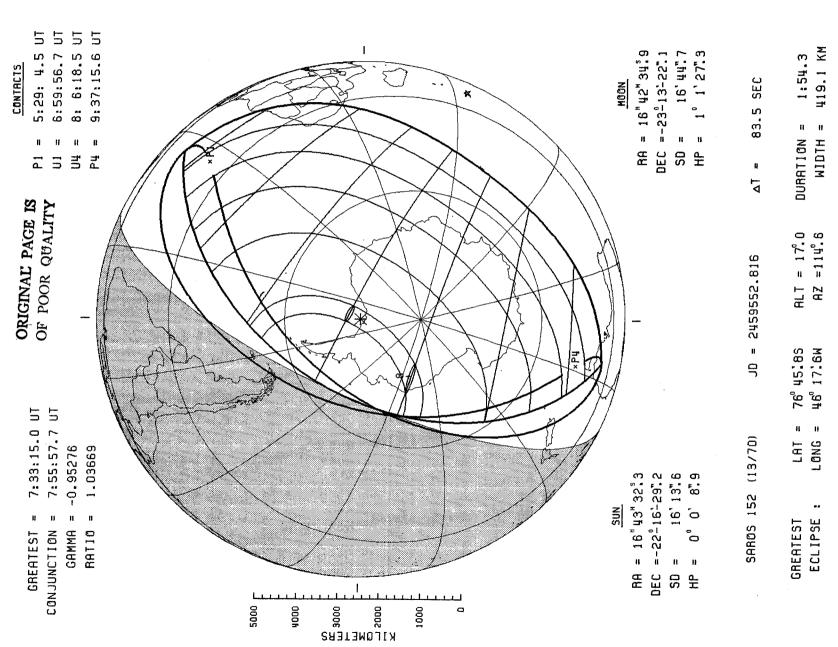
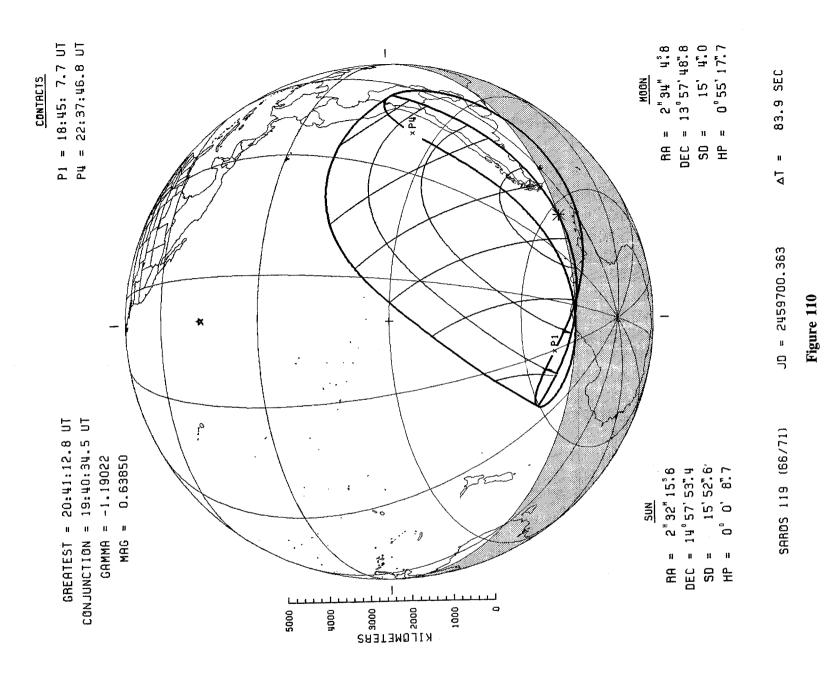


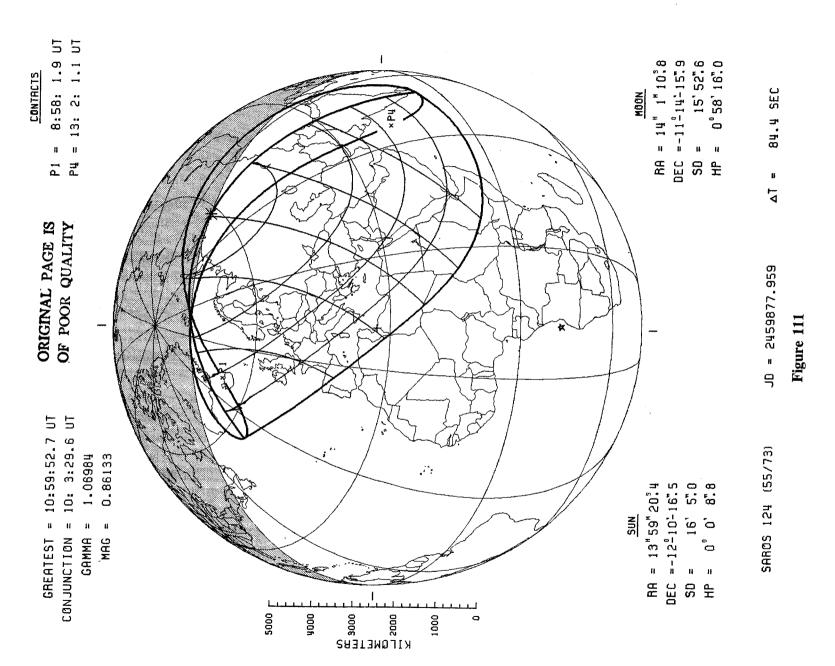
Figure 109

## 30 APR 2022 I PARTIAL SOLAR ECLIPSE



222

### 2022 25 OCT SOLAR ECLIPSE PARTIAL



### **20 APR** ı SOLAR ECLIPSE **RNN/TOT**

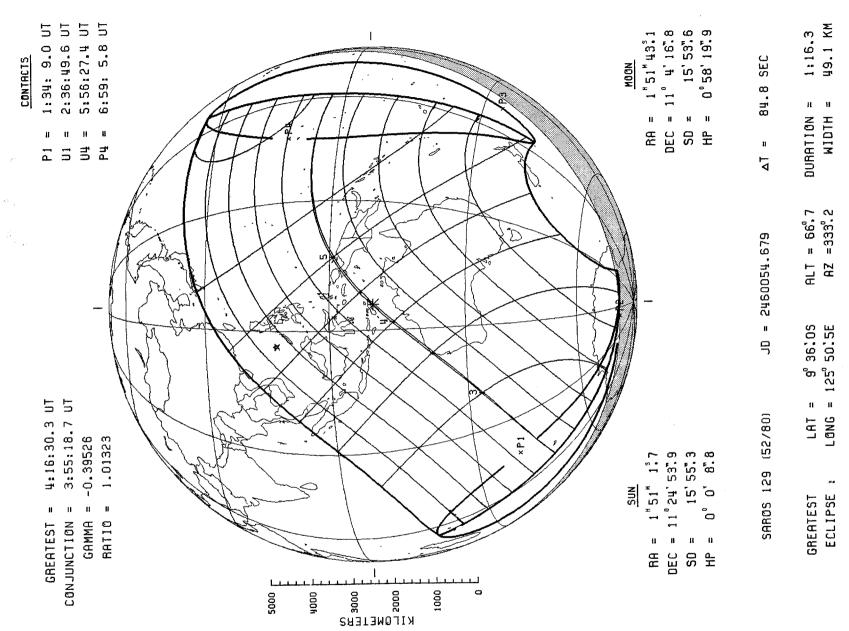


Figure 112

### 2023 OCT ゴニ ŧ ANNULAR SOLAR ECLIPSE

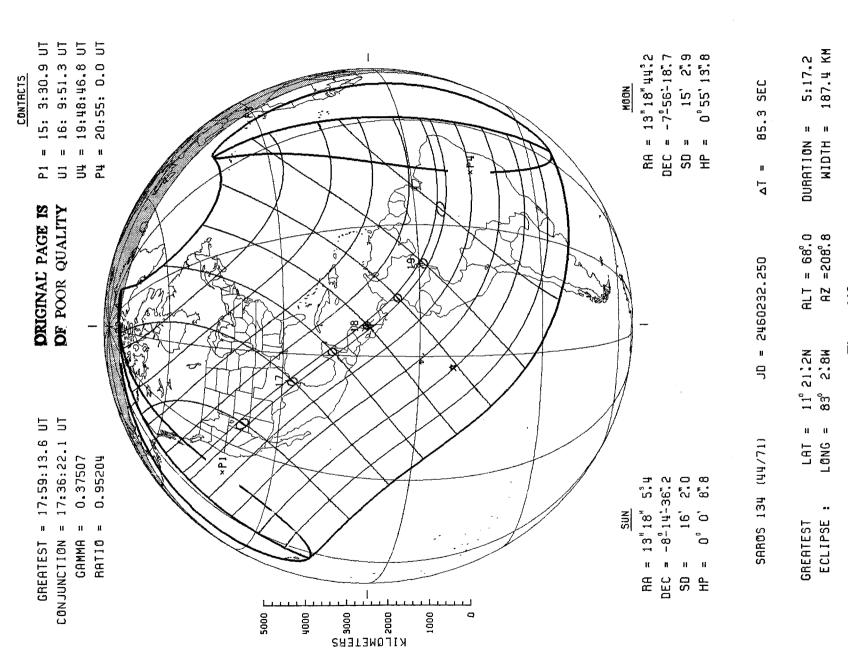


Figure 113 225

# TOTAL SOLAR ECLIPSE - 8 APR

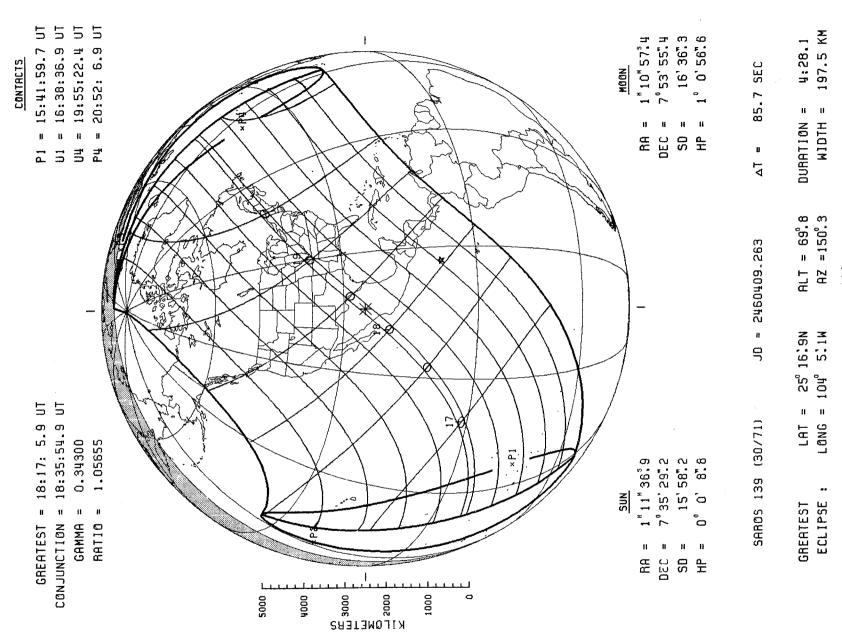


Figure 114 226

### 2024 2 0CT ı ANNULAR SOLAR ECLIPSE

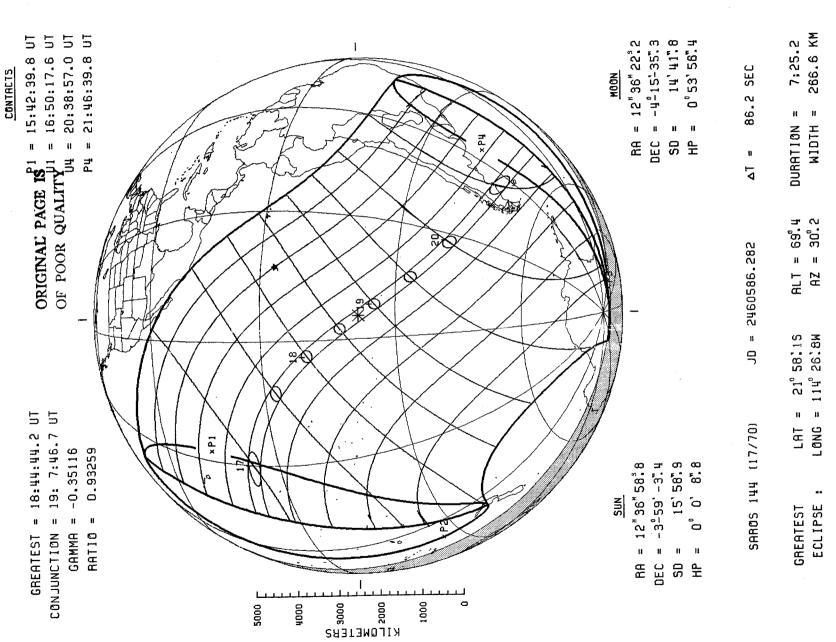
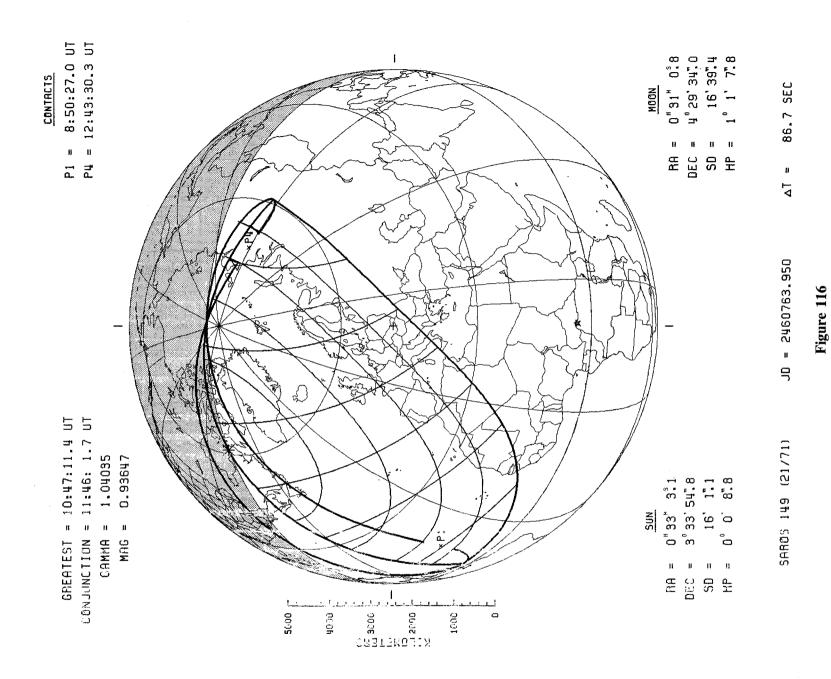


Figure 115

### 2025 MAR 29 1 SOLAR ECLIPSE PERTIAL



)

### 2025 SEP 21 t SOLAR ECLIPSE PARTIAL

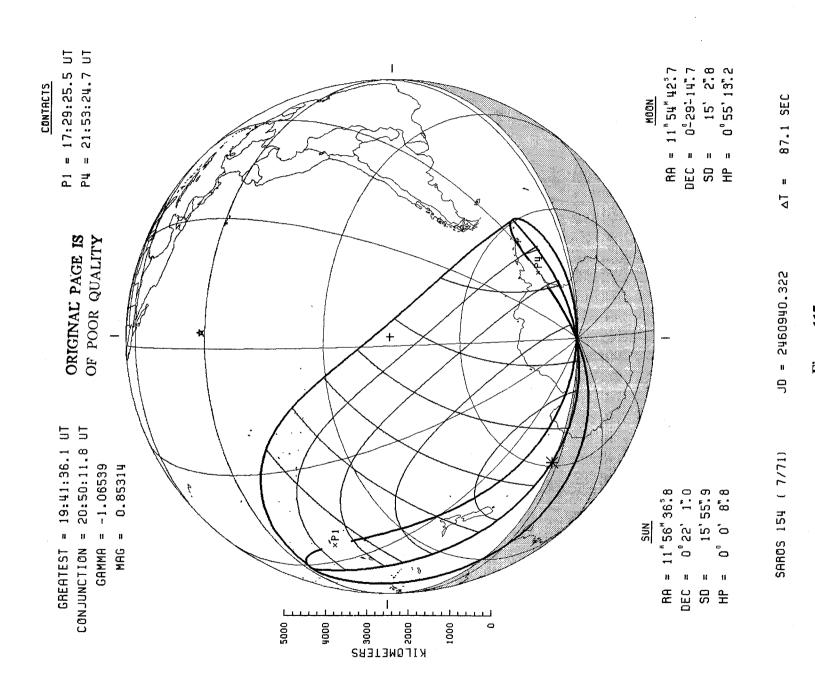


Figure 117

## 2026 FEB ANNULAR SOLAR ECLIPSE

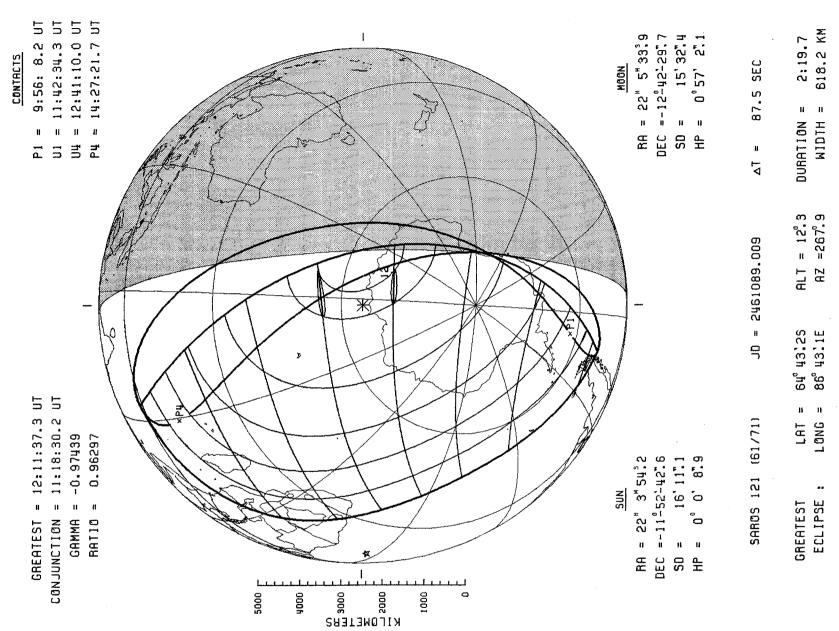


Figure 118 230

### 2026 AUG 2 SOLAR ECLIPSE TOTAL

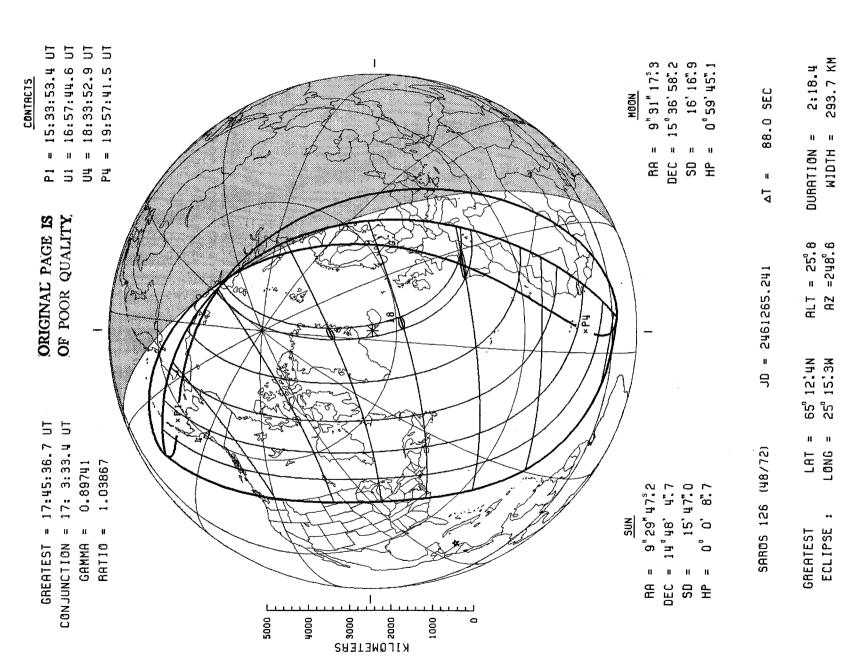


Figure 119

## ANNULAR SOLAR ECLIPSE -

2027

FEB

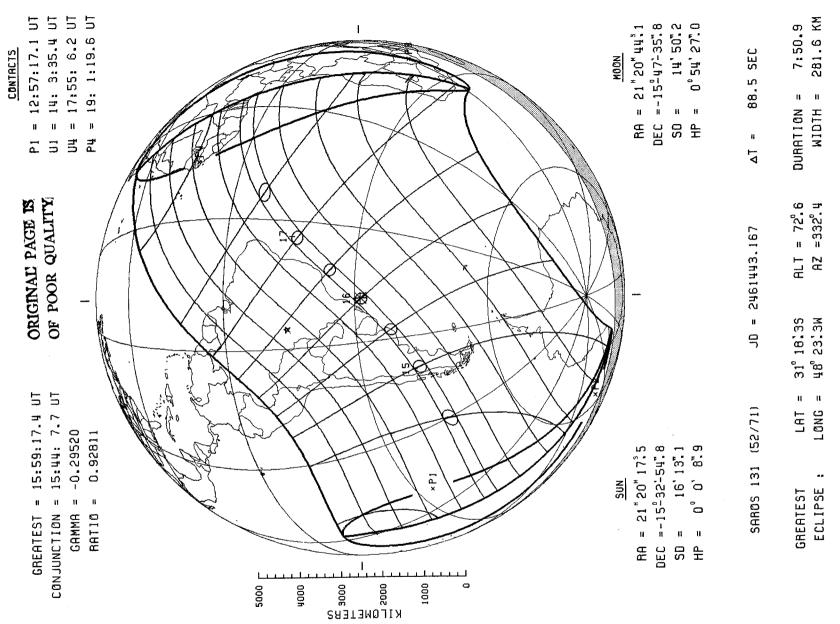


Figure 120 232

### 2 AUG ŧ SOLAR ECLIPSE TOTAL

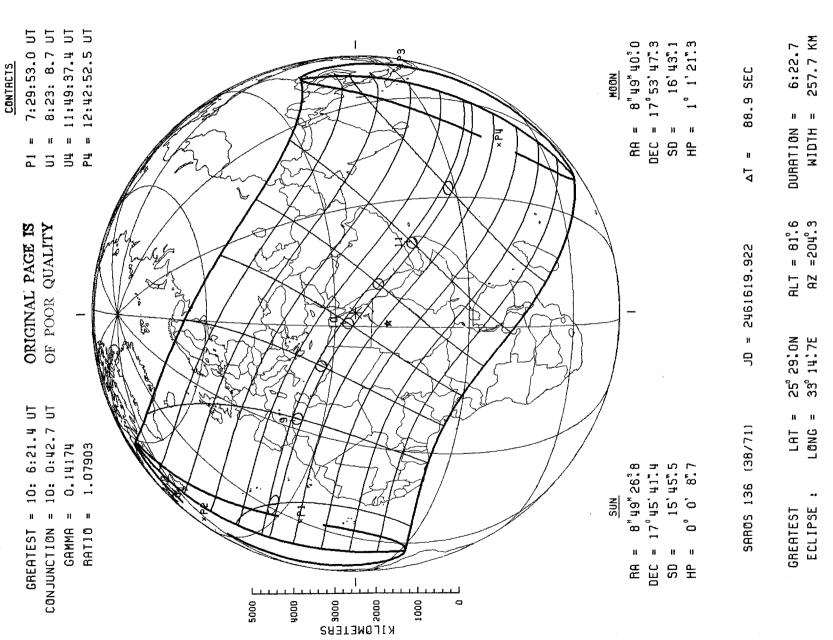


Figure 121 233

#### 2028 JAN 56 ı **ECLIPSE** SOLAR ANNULAR

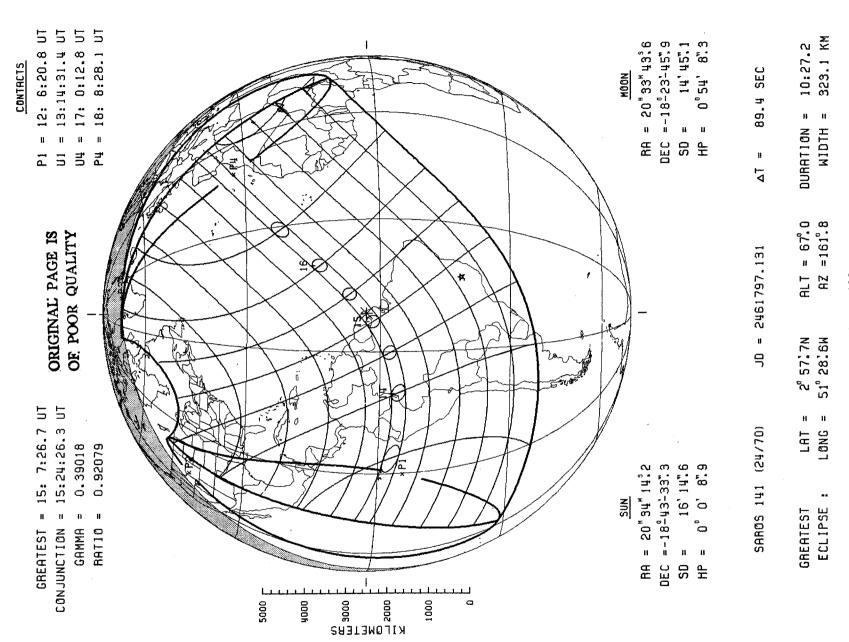


Figure 122 234

### 2028 22 SOLAR ECLIPSE TOTAL

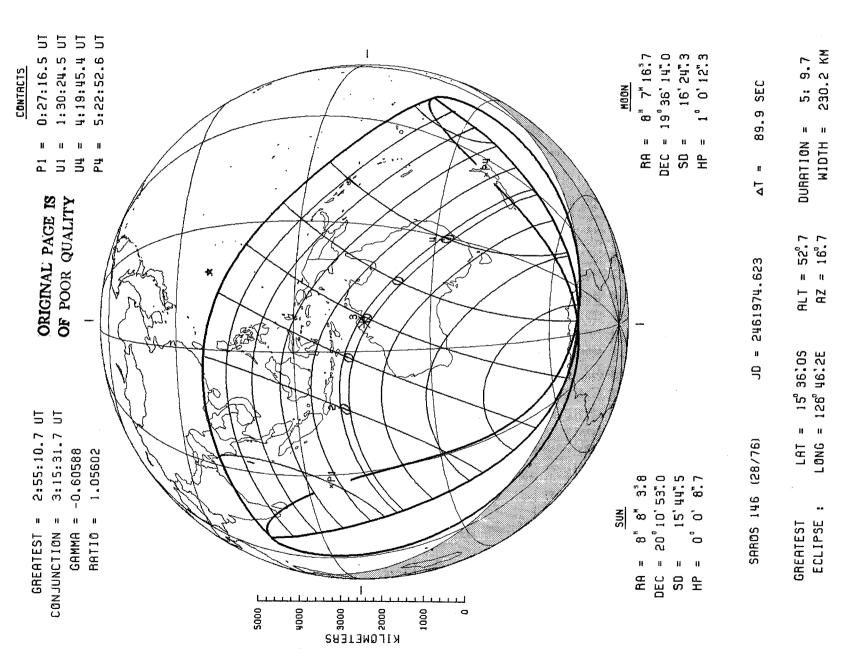
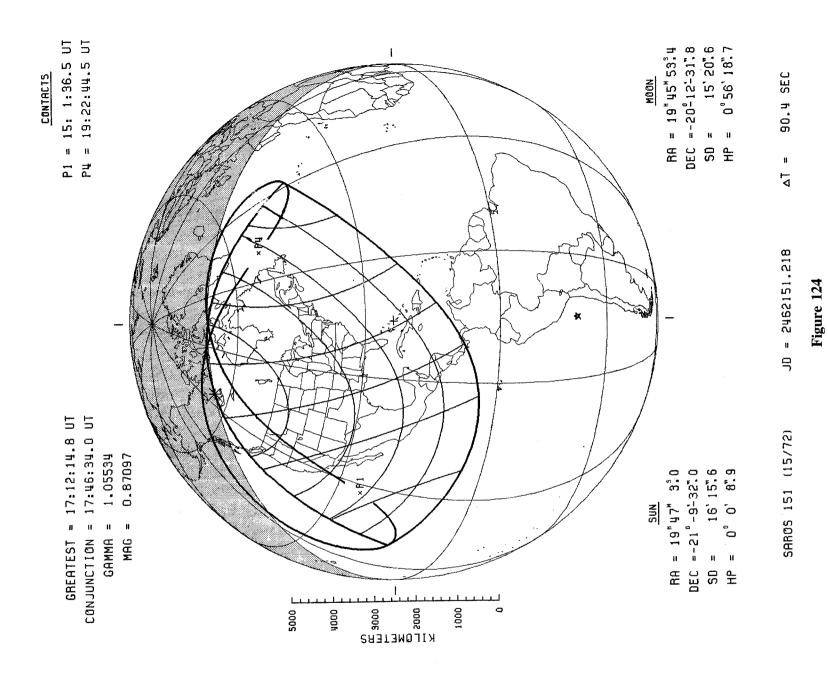
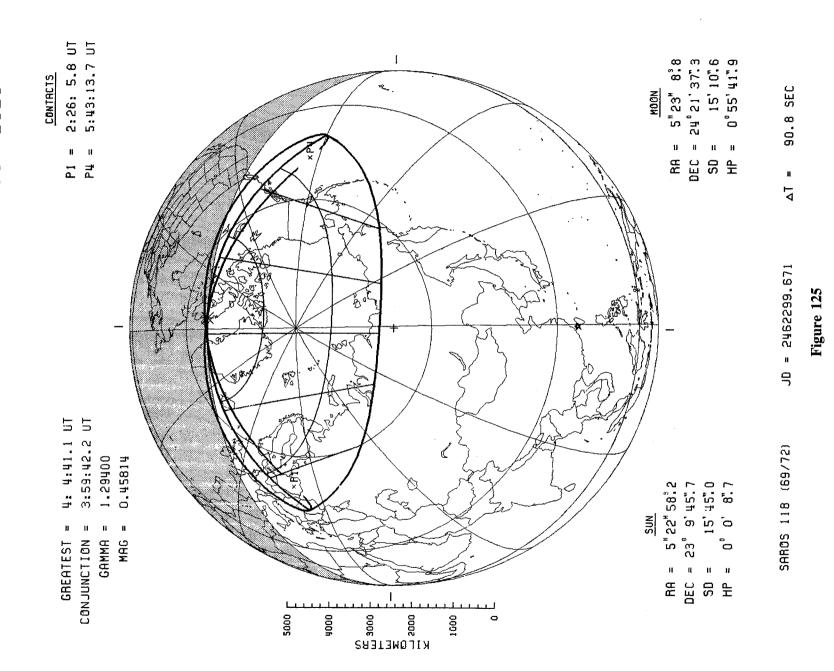


Figure 123

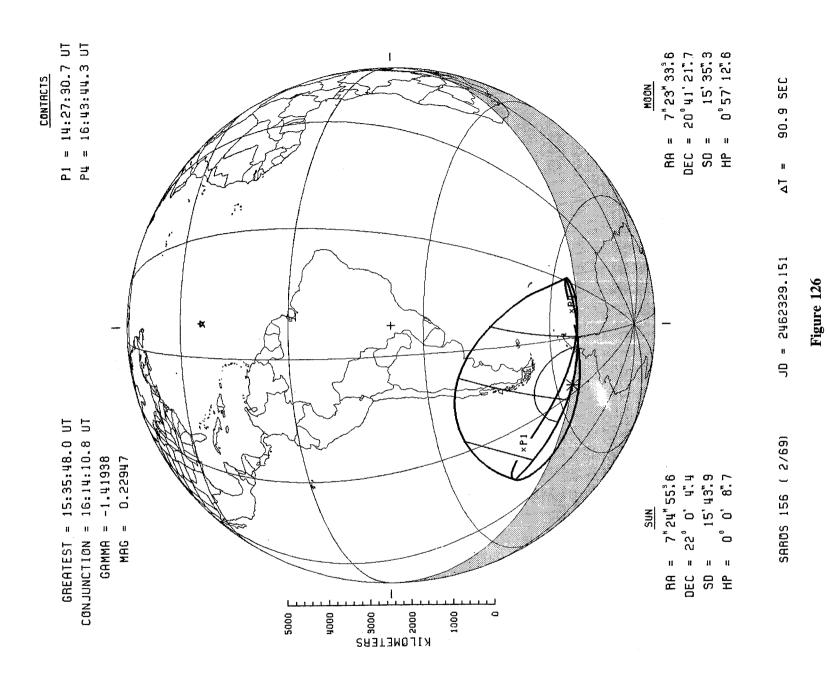
### 2029 JAN BN ゴニ ı SOLAR ECLIPSE PARTIAL



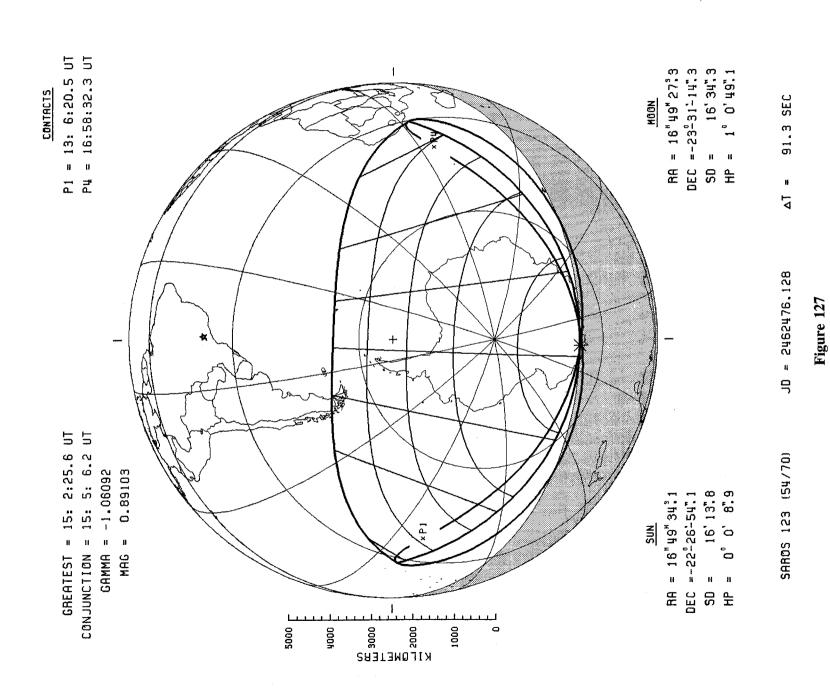
### 2029 N N N 12 SOLAR ECLIPSE PARTIAL



## 2029 SOLAR ECLIPSE PARTIAL



### 2029 DEC S ŀ SOLAR ECLIPSE PARTIAL



2030

S

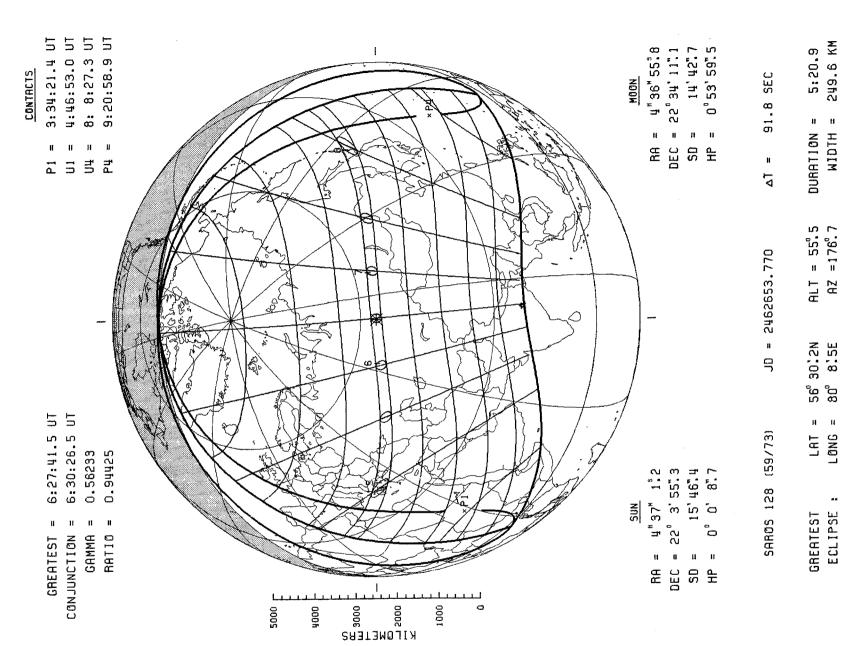


Figure 128 240

### 25 NØV 2030 ı TOTAL SOLAR ECLIPSE

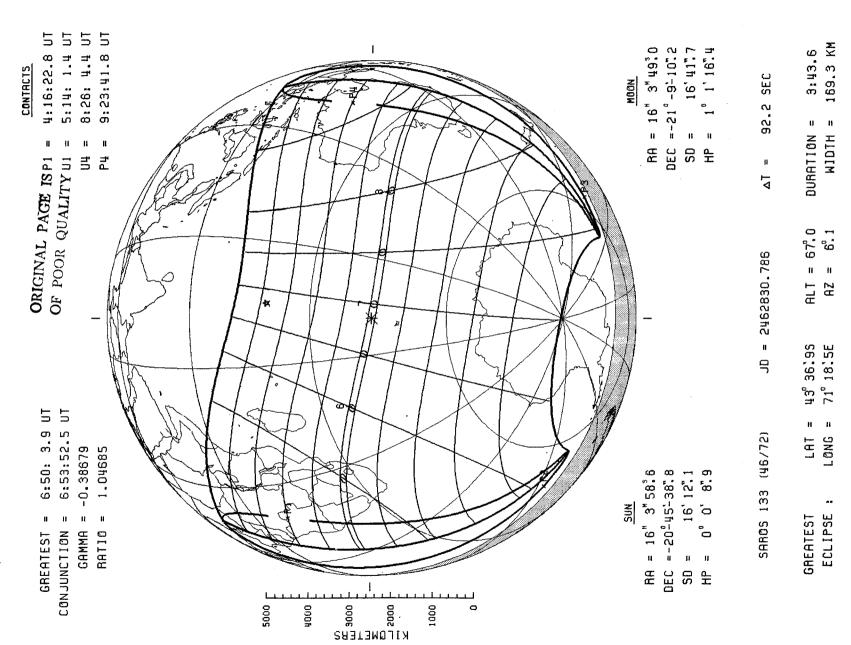


Figure 129 241

### 2031 MAY2 ANNULAR SOLAR ECLIPSE

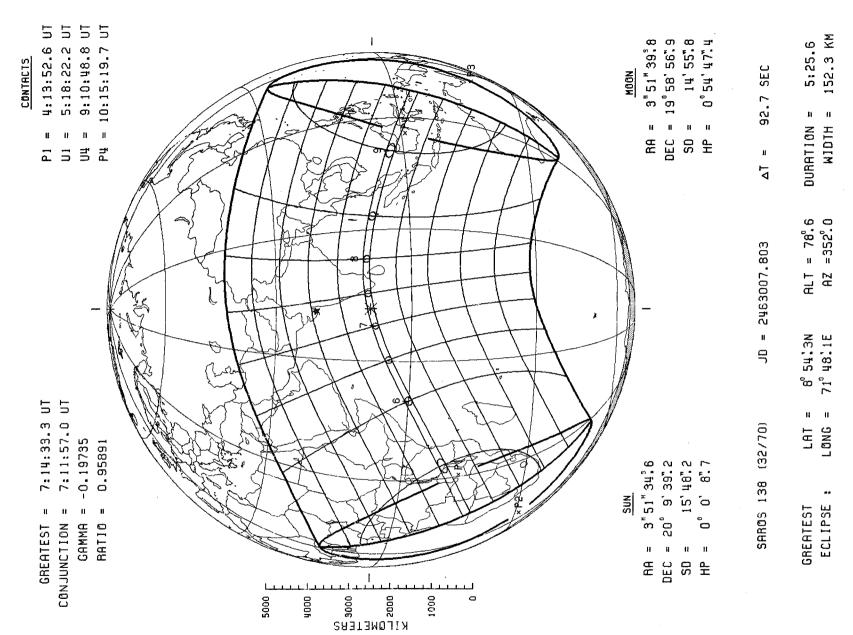


Figure 130 242

## 14 NOV 2031 ı ANN/TOT SOLAR ECLIPSE

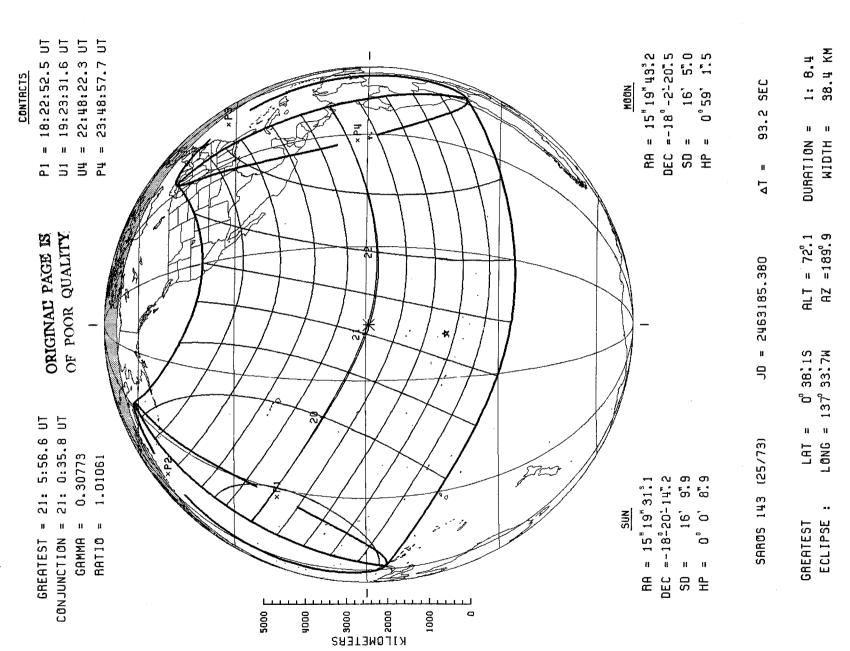


Figure 131 243

## ANNULAR SOLAR ECLIPSE -

2032

9 MAY

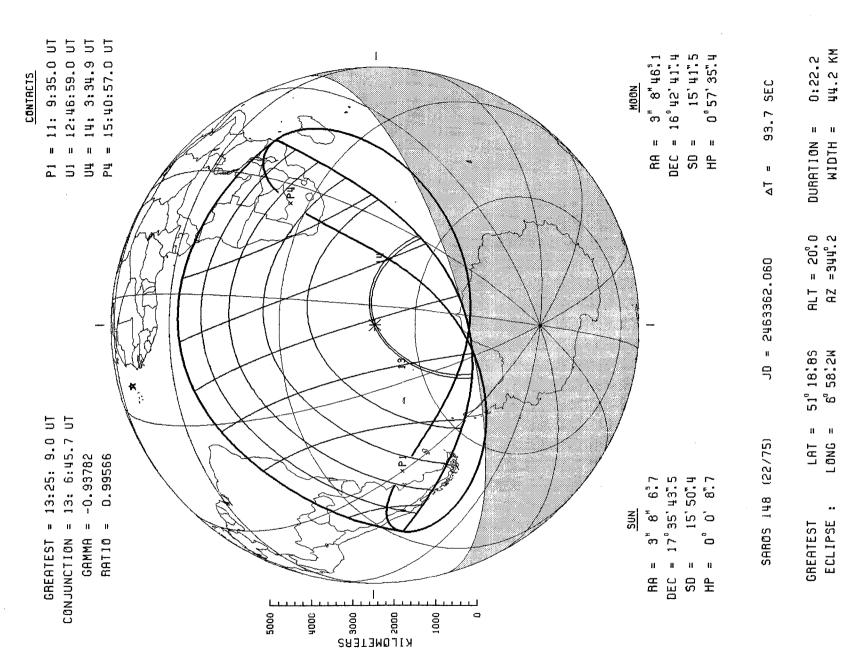
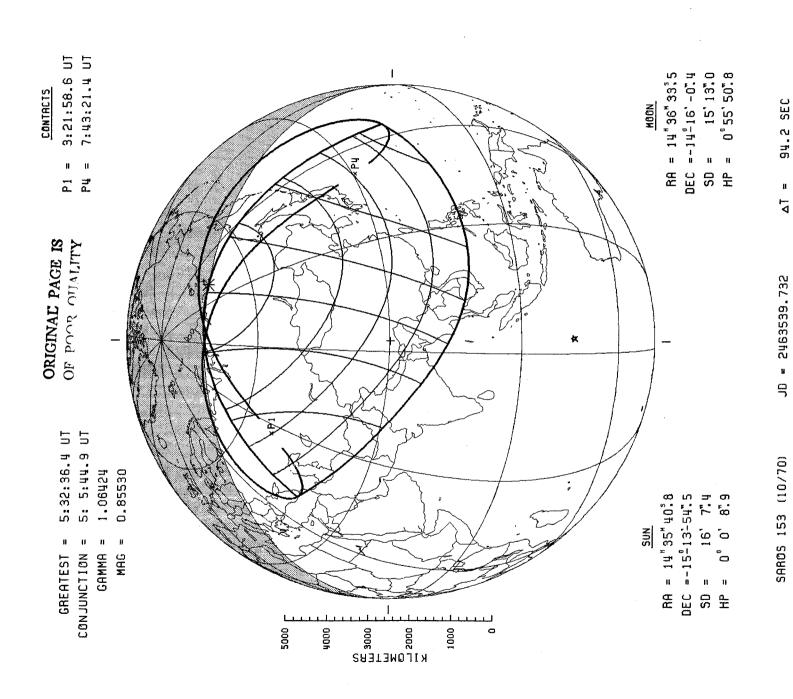


Figure 132 244

## PARTIAL SOLAR ECLIPSE -

2032

3 NOV



245

Figure 133

#### 2033 MAR 30 ı **ECLIPSE** SOLAR TOTAL

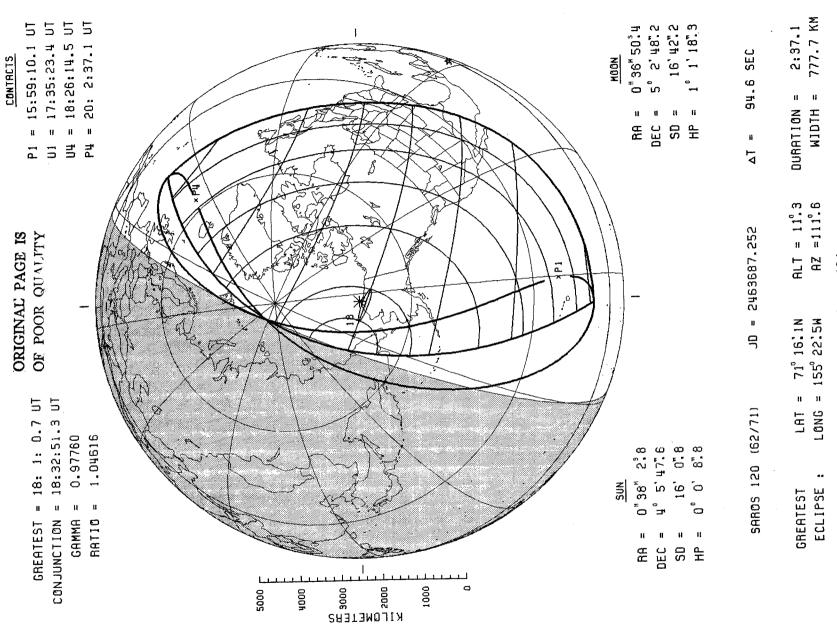


Figure 134 246

### 2033 23 SEP ı SOLAR ECLIPSE PARTIAL

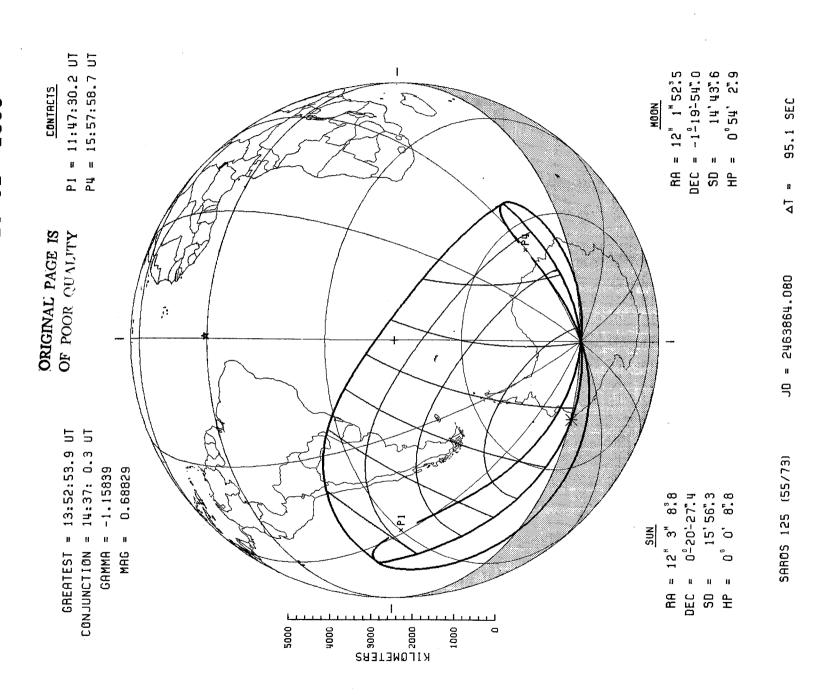


Figure 135

### 2034 **20 MAR** ı SOLAR ECLIPSE TOTAL

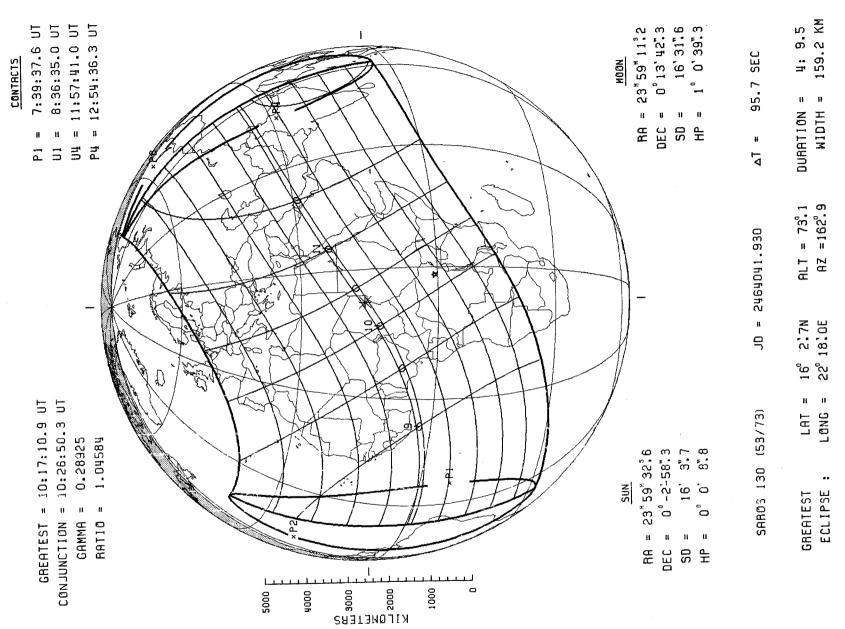


Figure 136 248

#### 2034 SEP 2 **ECLIPSE** ANNULAR SOLAR

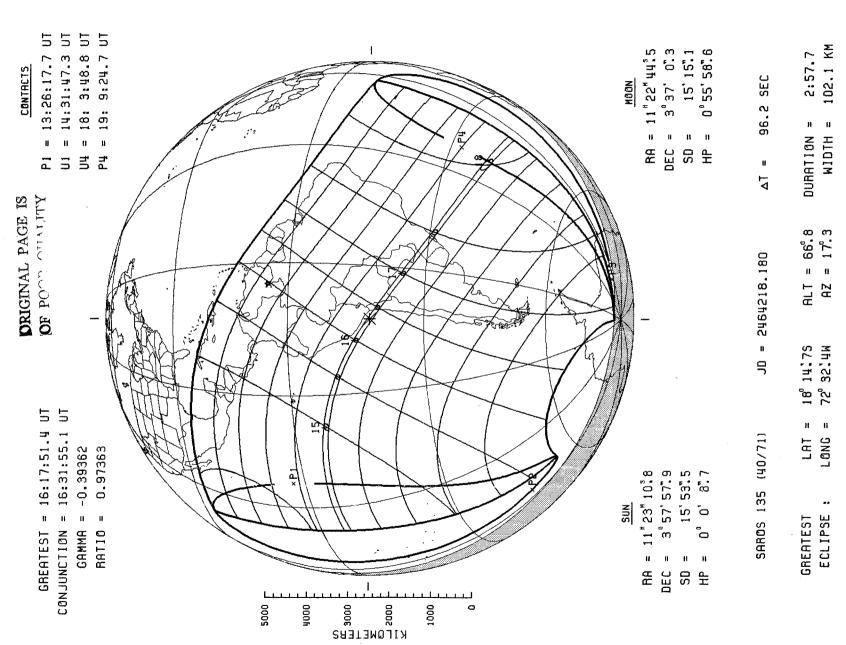


Figure 137

## ANNULAR SOLAR ECLIPSE

2035

MAR

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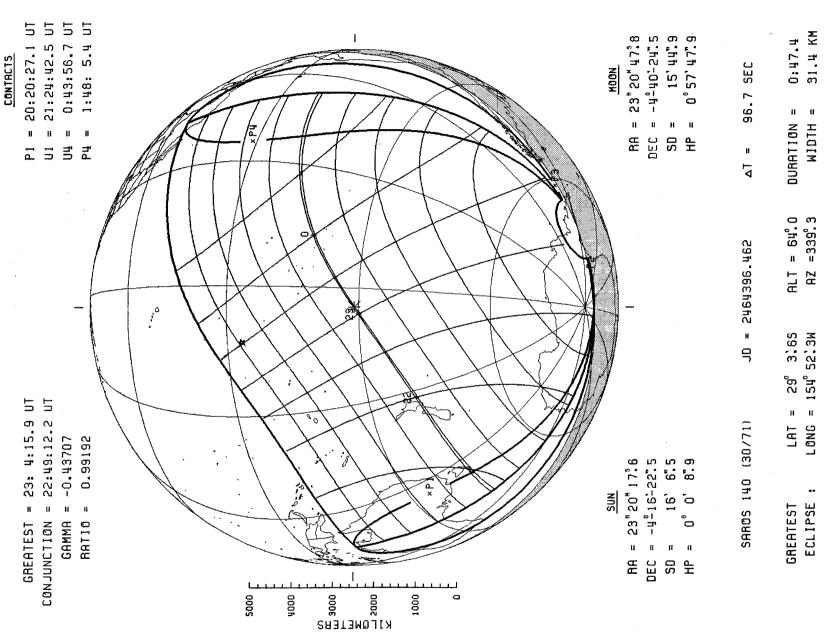


Figure 138

#### 2035 SEP N ı SOLAR ECLIPSE TOTAL

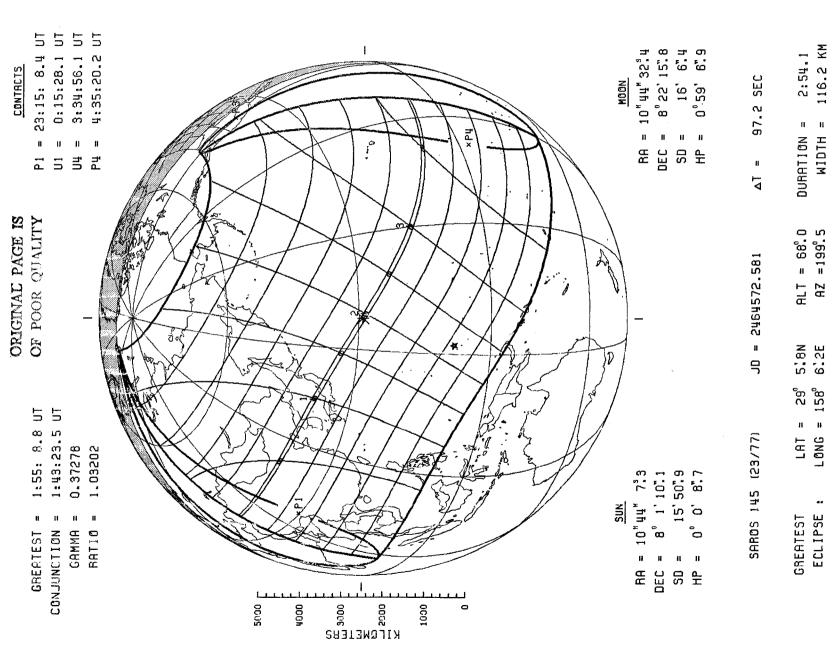


Figure 139

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# FIFTY YEAR CANON OF SOLAR ECLIPSES: 1986 - 2035

APPENDIX A - SOLAR ECLIPSES

### GEOMETRY OF SOLAR ECLIPSES

One of the most remarkable coincidences found in nature is the fact Earth, The Moon, a small, cold, dark body, is only 3500 km in diameter The coincidence arises from the fact that although the Sun is 400 times while the Sun, a self luminous, gaseous giant, is 1,400,000 km across. that the Moon and Sun both appear the same size as seen from the direct consequence of this fortuitous geometry is that during a total larger than the Moon, it's also 400 times farther from the Earth. A solar eclipse, the Moon occults the Sun with a nearly perfect fit.

a partial eclipse is seen. The path of the umbra is rarely more than 300 through the Moon's shadow. This shadow is composed of two parts: the dark, central umbra is the shadow of complete or total eclipse. During a eerie twilight. Outside the path of totality but still within the penumbra, total eclipse, the umbra sweeps across the Earth from west to east and as long as  $7\ 1/2$  minutes. At this time, the solar corona is visible as a within the penumbra, only part of the Sun is obscured. In contrast, the halo about the Moon and the landscape takes on the appearance of an within this zone will see the Sun completely obscured by the Moon for The fundamental basis of the solar eclipse is the alignment of the Sun, Moon and the Earth such that some region of the Earth passes Sometimes the umbral shadow misses the Earth entirely and only a the course it travels is called the path of totality. Anyone standing outer or penumbral shadow and the inner or umbral shadow. From km wide while that of the penumbra is about 7000 km wide. partial eclipse occurs.

diameter varies from 944 arc-seconds at aphelion to 976 arc-seconds at Eclipse geometry is complicated by the fact that the Earth's orbit around the Sun is elliptical. As a result, the Sun's apparent semiperihelion. This 3% range in apparent size is, of course, quite indistinguishable to the naked eye.

The Moon is 406,700 km from the Earth's center at apogee and 356,400 the Moon to appear almost 10% or 3 arc-minutes smaller than the Sun. semi-diameter to vary between 882 and 1006 arc-seconds. Thus, during km at perigee. This 12% range in distance causes the Moon's apparent total solar eclipse, the Moon's apparent diameter can exceed the Sun's by as much as 7% or 2 arc-minutes. Conversely, it's also possible for However, the orbit of the Moon about the Earth is also elliptical.

When the Moon is near apogee, it's umbral shadow falls short of the Such a geometry results in the case of an annular solar eclipse.

takes its name from the ring or annulus of sunlight which surrounds the photosphere hides the corona from view and precludes any measurements silhouetted against the Sun's bright photosphere. This type of eclipse stationed in the path of totality would see the Moon completely Earth and the Moon appears smaller than the Sun. An observer Moon at maximum eclipse. Unfortunately, the blindingly bright or photographs of the Sun's outer atmosphere.

the shadow falls 39,400 km short of the geocenter. These represent the extremes of the Moon's umbra (Figure 1). In the first case, the umbral The term "central eclipse" is reserved for any eclipse in which the cone can have a maximum diameter of 273 kilometers at the Earth. If However, when the Moon is at apogee and the Earth is at perihelion, annular in nature. When the Moon is at perigee and the Earth is at generates a negative or anti-umbra. As it strikes the Earth, the antiaxis of the Moon's shadow intersects the Earth. From the previous aphelion, the shadow extends 23,500 km beyond the Earth's center. discussion, it's obvious that a central eclipse can be either total or the surface of the shadow cone in the second case is extended, it umbra can have a maximum diameter of 313 km and an observer positioned there will see an annular eclipse.

between the annular and total eclipse. It occurs when the umbral shadow A third type of central eclipse is possible which forms the transition eclipses of 3 October 1986 and 30 March 1987 are two examples of the Earth's center. In this case, the eclipse will be annular at either end of is just long enough to reach part of the Earth's surface, but not the the eclipse path while it will be total along the middle section. The annular/total eclipse.

# ECLIPSE FREQUENCY AND RECURRANCE

new Moon? Since the Moon cycles through its phases every 29 1/2 days or one synodic month, one would expect an eclipse to occur during each conjunction with the Sun. If the Moon's orbit around the Earth were in month at a pair of points called the nodes (Figure 2). The rest of the time, the Moon is either above or below the plane of the Earth's orbit. would happen. However, the Moon's orbit is inclined 5° to the Earth's. question immediately arises. Why doesn't a solar eclipse occur at every Since an eclipse can only occur when the Sun, Moon and Earth lie in the same plane as the Earth's around the Sun, this is precisely what Our planet's natural satellite passes through the ecliptic only twice a Having established the preliminary geometry for solar eclipses, a

#### LUNAR SHADOW EXTREMES

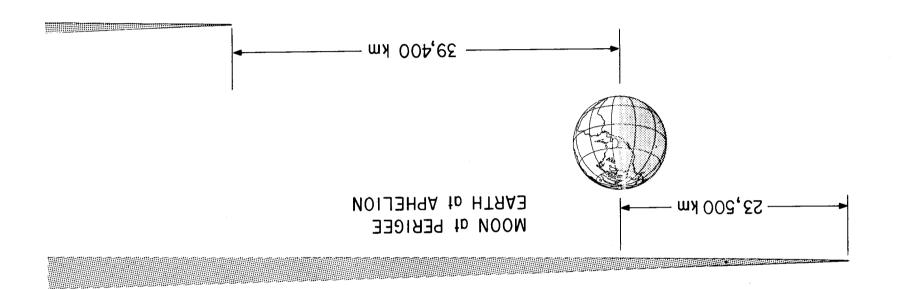
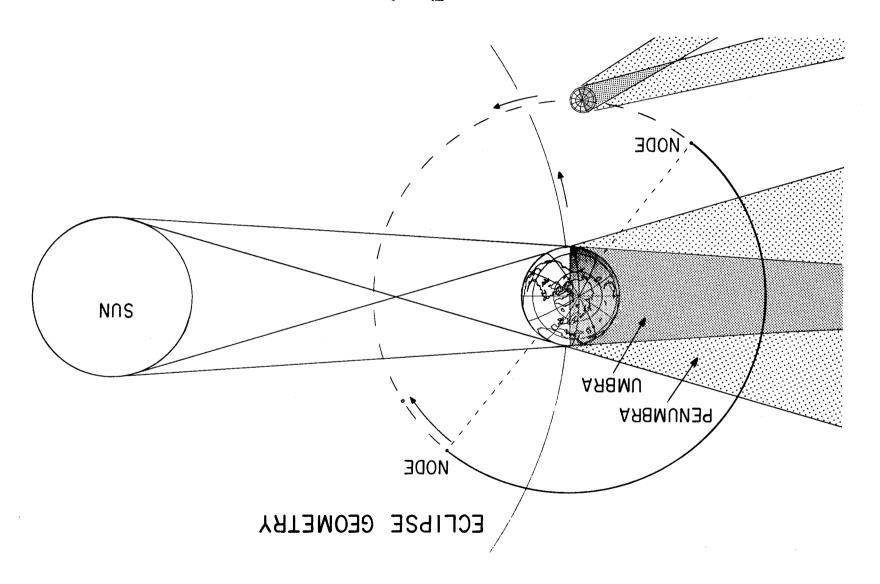


Figure 1

MOON at APOGEE

EARTH of PERIHELION





the same plane, these conditions are met when new Moon takes place at one of the nodes.

orbit inscribed by the exterior tangents. However, the sunward arc of the they're more common than lunar eclipses. An examination of the exterior Contrary to popular belief, solar eclipses are not at all rare. In fact, An eclipse is possible only when the Moon is within that section of its tangents which delineate the Earth's umbra will substantiate this claim. through the shadow. The number of solar and lunar eclipses that occur Moon's orbit is clearly longer than the anti-sunward arc which passes are proportional to the lengths of these two arcs. Thus, solar eclipses out number lunar eclipses by almost 5 to 3. In this argument, the Earth's penumbral shadow has been ignored since penumbral lunar eclipses are essentially unobservable.

seven eclipses. What made it even more remarkable was the fact that all three lunar eclipses were total. This will not happen again until the year five solar eclipses. On the other hand, there can be no more than three occur in the combinations of five solar and two lunar or four solar and point of interest, 1982 happened to be one of the rare years containing three lunar. In either case, the solar eclipses must all be partial. As a year to contain a maximum of seven eclipses. However, they can only In any one calendar year, there are at least two and as many as Combining both solar and lunar eclipses, it's possible for one calendar lunar eclipses per year and it's quite possible to have none at all. 2485 AD.

The previous discussion contradicts common experience because lunar eclipses are observed more frequently than solar eclipses. The conflict is resolved since solar eclipses are only visible from isolated regions of the Earth while lunar eclipses are visible from the entire night time hemisphere of our planet.

eclipse to occur. In addition, an observer's position on the surface of the An examination of the geometry of the nodes yields further clues on each node. New Moon occurs every  $29 \, 1/2$  days and thus guarantees at the subject of eclipse recurrence. Since the Sun and Moon both subtend of a node. The Sun travels along the ecliptic at about  $1^\circ$  per day and factors make a solar eclipse possible whenever the Sun is within  $18.5^\circ$ requires about 37 days to cross through the eclipse zone centered on significant angles, neither one has to be exactly at the nodes for an Earth introduces a sizable parallax of 2° in ecliptic latitude. These least one eclipse during each of the Sun's node crossings.

The period during which the Sun is near a node is called an eclipse season and there are two eclipse seasons each year. If the line of nodes

and at the same time each year. Actually, the line of nodes slowly drifts is equal to the time required by the Sun to cross the same node twice. were fixed in space, then eclipse seasons would occur six months apart eclipse year of 346.6 days. This is 18.6 days short of a solar year and seasons occur every 173.3 days. Two eclipse seasons constitute an westward at the rate of 19 degrees per year. As a result, eclipse

223 synodic months; they differ by only 11 hours. The coincidence is all anomalistic month. This is the time required for the Moon to pass from must search for a commensurability between the synodic month and the In order to find a periodicity in the mechanics of solar eclipses, we primary factor determining the annular or total nature of a solar eclipse. As unlikely as it may seem, 239 anomalistic months are also equal to eclipse year. Fortunately, 19 eclipse years are almost exactly equal to perigee to perigee and is approximately  $27 \, 1/2$  days. The anomalistic month is important because the Moon's geocentric distance is the the more remarkable when compared to a period known as the 223 synodic months to within 6 hours.

series returns to the same geographic region every 3 Saroses or 56 years displacement shifts the eclipse path 120° westward with each cycle, the the same node with the Moon at the same distance from Earth and at the same time of year. Because the Saros does not contain an integral Saros cycle share very similar mechanical characteristics. They occur at This is the origin of the famous Saros cycle of  $6585 \, 1/3$  days or number of days, its biggest drawback is that subsequent eclipses are 18 years, 11 days and 8 hours. Any two eclipses separated by one visible from different parts of the globe. Although the 1/3 day and 34 days.

A Saros series doesn't last indefinitely because the various periods eclipse years are 1/2 day longer than the Saros. As a result, the node are not perfectly commensurate with one another. In particular, 19 shifts eastward by about 0.5° with each cycle.

decending node, the Moon's umbral shadow will pass 3500 km below the On the following return, the umbra will pass about 300 km closer to the ten or eleven Saros cycles (about 200 years), the first central eclipse will occur near the south pole of the Earth. Over the course of the next 950 Earth and a partial eclipse of slightly larger magnitude will result. After Earth and a partial eclipse will be visible from the south polar region. years, a central eclipse will occur at each Saros but will be displaced A typical Saros series begins when new Moon occurs about 18 northward by an average of 300 km. Halfway through this period, degrees east of a node. If the first eclipse occurs at the Moon's

eclipse of the series will occur near the north pole. The next ten eclipses typical series may be comprised of 70 to 80 eclipses, about 50 of which series will end some 13 centuries after it began at the opposite pole. A are central. If a Saros series begins near the ascending node, the first will be partial with successively smaller magnitudes. Finally, the Saros eclipse will be partial from the northern polar region and the previous eclipses of long duration will occur near the equator. The last central sequence of events is reversed.

individual series and 26 of them are producing central eclipses. As old series terminate, new ones are always beginning and take their places. obviously many different Saros series in progress simultaneously. For instance, during the later half of the twentieth century, there are 41 Since at least two solar eclipses occur every year, there are

shadow cone passes closer to the limb of the Earth. The next eclipse in 2033 event is the last central eclipse of the series. Note that the paths the series will be a partial eclipse in 2051. Saros 120 will end with a series began with a partial eclipse at the south pole in 915 AD. The To illustrate, the total solar eclipses of 1925, 1943, 1961, 1979, 1997, 2015 and 2033 are all members of Saros 120 (Figure 3). The of the last four eclipses grow progressively broader as the umbral partial eclipse near the north pole in 2195.

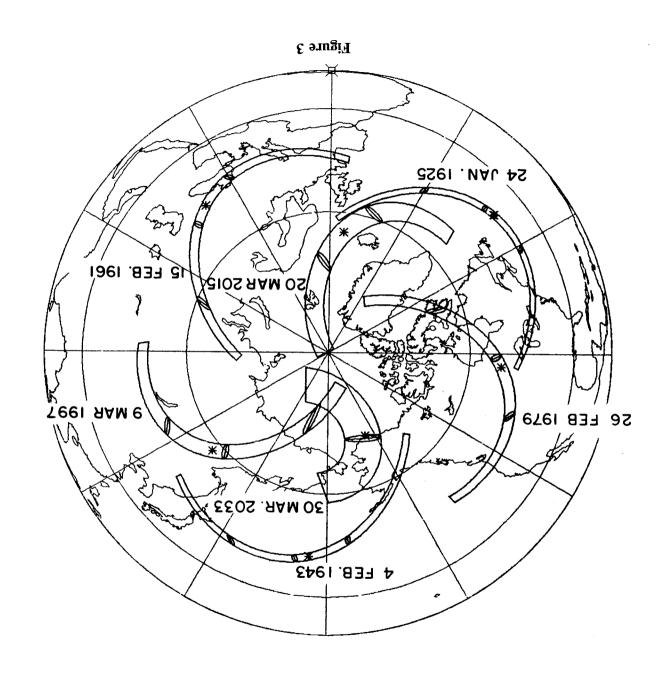
#### MODERN ECLIPSE PREDICTION

circumstances for a solar eclipse, high accuracy ephemerides for both the position, dimensions and velocity of the Moon's shadow on the Earth's Sun and the Moon are required. Conventional ephemerides tabulate the In order to predict the general characteristics as well as the local center. However, the eclipse calculator is primarily interested in the positions and distances of these bodies with respect to the Earth's

In 1824, the Prussian astronomer and mathematician Friedrich Bessel express the ephemerides of the Sun and Moon in terms of the Moon's successful that it remains today as the most powerful technique, even with the application of the digital computer. What Bessel did was to shadow. This change in the frame of reference greatly simplifies the introduced a new theory for the prediction of eclipses. It was so mathematics and geometry without any sacrifice in accuracy.

through the center of the Earth which is fixed perpendicular to axis of To define the Besselian elements of an eclipse, a plane is passed the lunar shadow. This is called the fundamental plane and on it is

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20LAR ECLIPSES OF SAROS 120

constructed an X-Y rectangular coordinate system with its origin at the perpendicular to the fundamental plane and parallel to the shadow axis. geocenter. The axes of this system are oriented with north in the positive Y direction and east in the positive X direction. The Z axis is

and umbral shadows on the fundamental plane are also tabulated as L<sub>1</sub> The X-Y coordinates of the shadow axis can now be expressed in units of the equatorial radius of the Earth. The radii of the penumbral and L<sub>2</sub>, respectively. The direction of the shadow axis on the celestial sphere is defined by its declination 'd' and ephemeris hour angle ' $\mu$ '.

Finally, the angles which the penumbral and umbral shadow cones These eight parameters, tabulated at hourly intervals serve as the only input needed to characterize an eclipse. The details of actual eclipse make with the shadow axis are expressed as  $f_1$  and  $f_2$ , respectively. calculations can be found in Chauvenet [1891] or the Explanatory Supplement [1974].

# GEOMETRY OF THE UMBRAL SHADOW

The length of the Moon's cone-shaped umbral shadow is a function of the Moon's distance from the Sun. For any given eclipse, it can be determined by first calculating the half-angle ' $f_2$ ' which the umbral cone makes with its axis:

$$\sin f_2 = (\sin s_0 - k \sin \pi_0) / D_{sm}$$

 $\pi_0$  = horizontal parallax of Sun at mean distance (= 8.794")  $D_{Sm}=$  distance between the Moon and Sun in Earth radii  $s_0 = \text{semi-diameter of Sun at mean distance} (= 959.63")$ = mean radius of Moon in Earth radii (= 0.272281) ¥

as the difference in distance between the Moon and Earth 'Dm' and the The distance between the Moon and the Sun  $^{1}D_{sm}$  is readily calculated distance between the Sun and the Earth 'Ds' as:

$$D_{Sm} = D_S - D_m$$
 
$$D_m = 1 \ / \ tan \ \pi_m$$
 and 
$$D_S = 1 \ / \ tan \ \pi_S$$

= distance of Moon from Earth in Earth radii = distance of Sun from Earth in Earth radii Dm

 $\pi_{\rm m}=$  horizontal parallax of Moon (from Section 4)  $\pi_{\rm S}=$  horizontal parallax of Sun (from Section 4)

The length of the umbral shadow  ${}^{\prime}D_{u}{}^{\prime}$  (in Earth radii) then follows as:

$$D_u = k / \tan f_2$$

An observer somewhere along the eclipse path can calculate their topocentric distance (in Earth radii) from the Moon  $^{\prime}D_{t}$  as (approximately):

$$D_t = k / tan (q s_s)$$

= ratio of apparent diameters of the Moon and Sun geocentric semi-diameter of Sun (from Section 4) as seen by the observer (from Section 3) ≅ S Б where:

Then, the radius of the umbral shadow  ${}^{\prime} {}_{\rm u}$ ' seen by an observer at topocentric distance 'Dt' is just:

$$r_u = k (D_u-D_t) / D_u$$

Ignoring the curvature of the Earth's surface, the shadow is elliptical with its major The local geometry of the umbral shadow at any one point along axis aligned along the azimuth of the Sun; the minor axis is equal to the actual diameter of the umbral cone at that point 'ru'. The eccentricity 'e' of the shadow is related to the Sun's altitude 'A' by: the eclipse path is rather complicated and changes rapidly.

$$e = 1 - \sin^2 A$$

('a' and 'b', respectively) can also be used to define the eccentricity as: The major and minor semi-axes (in kilometers) of the umbral shadow

$$3 = \left(\frac{a^2 - b^2}{a}\right)$$

here: 
$$b = r_e r_u$$
  
 $a = b / \sin A$ 

$$r_e = equatorial radius of Earth (= 6378.388 km)$$

As a result, the width of the path necessary to adopt a different frame of reference which will simplify this of totality (or annularity) can take on any value between the major and In order to determine the relationship between Unfortunately, the azimuth of the shadow's path is independent of the distance from the center line and the duration of totality, it is parameters describing its shape. minor axes' dimensions. geometry.

Figure 4 represents the appearance of the umbral shadow, seen from obtained from a large scale map on which the path of totality has been Such information is readily plotted. As the shadow passes over the observer, he will lie on chord observer at point 'P' is clearly located perpendicular distances 'd' from the Moon as it sweeps over the Earth's surface. Neglecting the tiny the shadow is moving from the left to the right, the center line runs irregularities in the Moon's limb profile, the shadow is quite circular. 'C'. The key question is: how long will totality last at point 'P'? A hypothetical along diameter 'D' and totality lasts 'T' seconds. the center line and 'h' from the path edge.

From plane geometry, the length of chord 'C' is related to a circle's diameter 'D' and perpendicular distance 'd' by:

$$=$$
  $D^2 - 4d^2$ 

totality at any point on the chord. Therefore, the duration of totality 't' But the length of chord 'C' is directly proportional to the duration of at point 'P' is just:

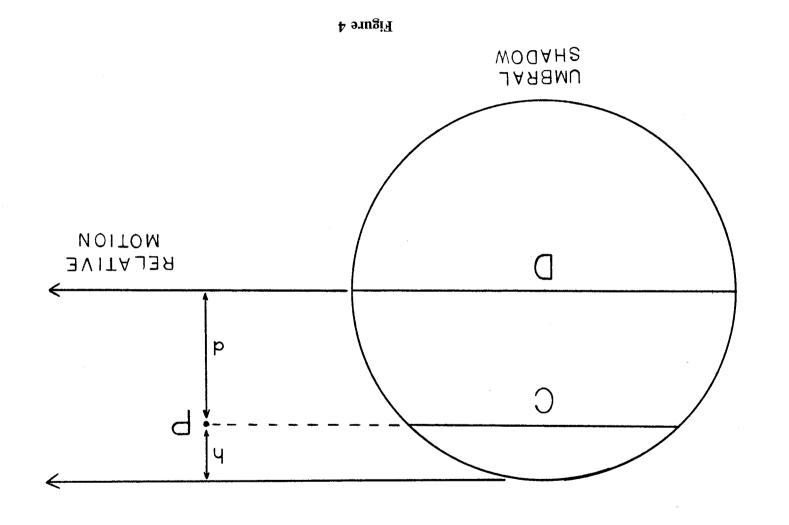
$$t = T \cdot C / D = T \cdot \sqrt{D^2 - 4d^2 / D}$$
 seconds

where 'D' is the width of the path, 'd' is the distance of the observer from the center line and 'T' is the duration on the center line.

Expressing the duration of totality as a function of distance from the path edge, the relation for chord 'C' becomes:

and the duration of totality 't' is:

$$t = T \cdot C / D = T \cdot \begin{cases} 4h(D-h) / D \text{ seconds} \end{cases}$$



It should be pointed out that observers within 5 to 10 kilometers of the path edge must consider the effects of the lunar limb profile in determining the duration of totality.

#### TIME DETERMINATION

solar day is not constant but varies with an annual cycle. What was not yardstick. It's been known for thousands of years that the length of the should come as no surprise then, that time reckoning remains intricately passage of time by observing the motions of the Sun and the Moon. It known before Kepler's time was that the Earth's elliptical orbit about branches of science, but to none more so than astronomy. In fact, entwined with astronomy even today. However, the Sun's apparent The measurement of time is of fundamental importance to all astronomy was born through man's first attempts to measure the motion no longer plays the pivotal role as the ultimate temporal the Sun, coupled with the inclination in the planet's axis were responsible for the periodic variations.

average rate of the true Sun. Greenwich Mean Time (GMT) or Universal Mean Solar Time can be conceptualized as time kept by a fictitious interaction with the Moon and, to a lesser extent, the Sun. This secular acceleration gradually transfers angular momentum from the Earth to the Moon. As the Earth loses energy and slows down, the Moon gains this energy and its distance from the Earth increases. In fact, the Moon's Earth does not turn on its axis at a uniform and constant rate. As the distance will eventually increase to the point where its angular diameter is always smaller than the Sun's and total solar eclipses will no longer ranging has shown that the Moon's average distance from the Earth is or mean Sun which moves eastward along the celestial equator at the increasing by about four centimeters per year. At this rate, total solar Time (UT) is simply Mean Solar Time as measured from Greenwich, Earth spins, a tidal friction is imposed on it through the gravitational be possible. Although still in its infancy, the technique of lunar laser years. Unfortunately, this too has fallen by the wayside because the England and was used in navigation and surveying for hundreds of eclipses will continue to occur for the next 750 million years.

derivation only go back as far as 100 years or so. Before then, spurious It should be pointed out that the secular acceleration of the Moon is very poorly known and may not be constant. Careful records for its and often incomplete eclipse observations from medieval and ancient manuscripts comprise the data base. In any case, the current value

century. Such a trivially small amount may seem insignificant, but it has implies an increase in the length of the day by about 0.001 seconds per seconds, while in one millennium, the planet is one and a quarter hours very measurable cummulative effects. In one century, the Earth loses 45 "behind schedule"

fluctuations for periods of up to several decades. It is believed that these significant role since they should alter the Earth's moment of inertia. fluctuations may be due to fluid motions in the Earth's core which The Earth's rotation on its axis is also subject to short term climatological changes and variations in sea-level may also play a Whatever the mechanism is, it is clear that its effects cannot be interact with and disturb the rotation of the mantle. However, predicted with the current state of knowledge.

A better standard than diurnal rotation for the absolute measurement of directly verifiable through observations. The resulting time is referred to planets and of the Moon are predictable to very high accuracy and are time is the use of solar system dynamics. The orbital motions of the as Ephemeris Time (ET).

slowing of the Earth's rotation on its axis had caused Universal Time to observed with respect to Universal Time. Between 1900 and 1980, the The Moon's position is predicted in terms of Ephemeris Time but it's Universal Time. The difference between Ephemeris Time and Universal 1/31,556,925,9747 of the tropical year 1900 at January 0 at 12 hours In 1957, the International Astronomical Union adopted Ephemeris Time (delta T or  $\Delta T$ ) is obtained through observations of the Moon. Time as the standard and defined the ephemeris second as ag 50.54 seconds (= delta T) behind Ephemeris Time.

9,192,631,770 periods of the chosen to agree as closely as possible to the ephemeris second. In 1984, 1984. With the technological development of the atomic clock, a method radiation corresponding to the transition between two hyperfine levels of the SI second was adopted as the newest time standard and Terrestrial the ground state of the Cesium 133 atom. The SI second was carefully Ephemeris Time remained the basis of all time measurements until stability unmatched by even celestial mechanics. The atomic or SI (for Dynamical Time (TDT) replaced Ephemeris Time. For consistency, the time scale for Terrestrial Dynamical Time was chosen to agree with of time measurement became available which has a permanence and Systeme International) second is defined as 1984 Ephemeris Time.

Solar eclipse predictions are now based on Terrestrial Dynamical Time but the position of the central eclipse path still depends on

be extrapolated but the resulting values of delta T will inevitably diverge (i.e.: TDT-UT) will vary in the future. At best, the current trends can corrections to the eclipse path longitudes can be calculated as follows: Universal Time. Unfortunately, it's impossible to predict how delta T from actual observations. As such observations become available,

Shift (in degrees) = 
$$0.00417807 * (\Delta T1 - \Delta T2)$$

where:  $\Delta T1 = \text{table value of delta T (in seconds)}$ .  $\Delta T2 = \text{true or observed delta T (in seconds)}$ .

correct longitudes of the central path. Changes in the value of delta T This shift is added to the tabulated path longitudes to calculate the have no effect on the tabulated latitudes. FIFTY YEAR CANON OF SOLAR ECLIPSES: 1986 - 2035

APPENDIX B - Program SUNECL

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#### APPENDIX B : Program SUNECL

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DISTANCE OF LUNAR SHADOW AXIS FROM EARTH'S CENTER (IN UNITS OF EARTH RADII).
MAGNITUDE OF ECLIPSE (FRACTION SUN OBSCURED).
(FOR TOTALS: DIAMETER RATIO OF SUN/MOON).
SEMI-DURATION OF PENUMBRAL AND UMBRAL PHASES.
                                                                                                                                                                                                                                                                                                                                                                                                                                                START OF SEARCH INTERVAL
                                                                                                                                                                                                                                                                                                                                                                                                                                                               END OF SEARCH INTERVAL.
                                                                                                                                                                                                                                                   ECLIPSE
                                                                                                                                                                                                                                                                                                                                                                                      C****PROGRAM SUNECL SEARCHES FOR ALL SOLAR ECLIPSES
C****OCCURRING WITHIN A GIVEN DATE INTERVAL.
C****THE GENERAL CHARACTERISTICS AND TIMES FOR EACH ECLIPSE ARE
                                                                                                                                                                          =1 - TOTAL SOLAR ECLIPSE.

=2 - ANNULAR SOLAR ECLIPSE.

=3 - PARTIAL SOLAR ECLIPSE.

=4 - ANNULAR/TOTAL SOLAR ECLIPSE.

=5 - PARTIAL ECLIPSE IS POSSIBLE.

- JULIAN DATE OF INSTANT OF GREATEST EC

- TIME (TDT) OF GREATEST ECLIPSE.
                                                                                            C****THEN CALCULATED.
C****THE PREDICTED ECLIPSE CHARACTERISTICS ARE STORED IN
                                                                                                                                     CALENDAR DATE OF ECLIPSE
                                                                                                                                                 TYPE OF ECLIPSE WHERE:
=0 - NO ECLIPSE OCCURS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 CALL JULDAT(DJ1, IW1, ID1, IM1, IY1, 0, 0, 0.0)
CALL JULDAT(DJ2, IW2, ID2, IM2, IY2, 0, 0, 0.0)

    OCTOBER 1983.

                                                                                                                                                                                                                                                                                                                                                                           IMPLICIT REAL*8(A-H,0-Z)
                                                                                                                                                                                                                                                                                                                                                              - NOV 1986.
                                                                                                                                                                                                                                                                                                                                   T1,T2 - S
ESPENAK
                                                                                                                                                                                                                                                                                                          ZMAG
                                                                                                                    C****COMMON/ZERO/ WHERE
C**** MONTH, IDAY, IYEAR
C****
                                                                                                                                                                                                                                                                FTIME
                                                                                                                                                                                                                                                                               GAMMA
                           ****PROGRAM : SUNECL
                                                                                                                                                                                                                                                                                                                                                   C****WRITTEN BY F.
                                                                                                                                                                                                                                                                                                                                                              C****LAST MODIFIED
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99 WRITE(6,220) K
220 FORMAT(/5X,'**** A TOTAL OF',14,' ECLIPSES WERE PREDICTED FOR
1 'THIS DATE INTERVAL.'/)
                                                                                                                                                 WRITE(6,210) MONTH, IDAY, IYEAR, FTIME, GAMMA, ZMAG, ITYPE, K
210 FORMAT(5X, ***** SOLAR ECLIPSE ON', I3, '/', I2, '/', I5,
1 4X, 'TIME =', F6.2, 'TDT', 4X, 'GAMMA =', F6.3,
2 4X, 'MAG =', F6.3, 4X, 'ITYPE =', I2, 4X, 'K =', I2)
GO TO 1
C****EXIT PROGRAM ECLIPSE.
                                                                                                                                              K=K+1
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1 +3.3D-04*DSIN(DTR*(166.56+132.87*Q-9.173D-03*Q*Q))
C****CALCULATE THE MEAN ANOMALIES OF THE SUN AND MOON.
ZM=359.2242D0+29.10535608D0*P-3.33D-05*Q*Q-3.47D-06*Q*Q*Q*Q
                                                                                                                                                                                            C**** "ASTRONOMICAL FORMULAE FOR CALCULATORS", MEEUS, PAGES 153-160
C**** "ASTRONOMICAL FORMULAE FOR CALCULATORS", MEEUS, PAGES 153-160
C**** "ASTRONOMICAL FORMULAE FOR CALCULATORS", MEEUS, PAGES 153-160
IMPLICIT REAL*8(A-H,0-Z)
COMMON/ZERO/MONTH, IDAY, IYEAR, ITYPE, FJD, FTIME, DELTA, GAMMA, ZMAG,
1 NSAR, NCN, LNS, IXX, T1, T2
DATA SYNOD/29.53058868DO/, PI/3.1415926535DO/
DATA DTR, RTD/0.017453292519943DO, 57.2957795131DO/
                                                                                                                                 METHER
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             XF=DMOD(XF,360.D0)
*CALCULATE DATE CORRECTION FOR ECLIPSE TEST.
EPC=+(0.1734-3.93D-04*Q)*DSIN(DTR*ZM)+0.0021*DSIN(DTR*(ZM+ZM))
1    -0.4068*DSIN(DTR*XM)+0.0161*DSIN(DTR*(XM+XM))
2    -0.0051*DSIN(DTR*(ZM+XM))-0.0074*DSIN(DTR*(ZM-XM))
3    -0.0104*DSIN(DTR*(XF+XF))
                                                                                               C****PASSES NEAREST TO THE EARTH'S CENTER.
C****SUBROUTINE PRESEC THEN TESTS THE ALIGNMENT TO DETERMINE WHETH!
C****A SOLAR ECLIPSE WILL OCCUR AND CALCULATES ITS CHARACTERISTICS
                                                                                                                                                                                                                                                                                                                                                                                                         SINCE FIRST NEW MOON
                                                                     C****THIS CORRESPONDS TO THE INSTANT WHEN THE MOON'S SHADOW AXIS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              =21.2964D0+390.67050646*P-1.6528D-03*Q*Q-2.39D-06*Q*Q
                               SYZYGY
                              OF NEW MOON
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  ZM=DMOD(ZM,360.DO)
XM=DMOD(XM,360.DO)
C****CALCULATE THE MOON'S ARGUEMENT OF LATITUDE
                                                                                                                                                                                                                                                                                                                                                                                              C****CALCULATE TIME ELLAPSED IN LUNAR MONTHS
C****DF 1900. (I.E. - 1/1/1900 13:34:05ET)
1 KNT=KNT+1
SUBROUTINE PRESEC(EJD)
C****SUBROUTINE PRESEC PREDICTS THE INSTANT
                                                  C****NEAREST TO THE INPUT JULIAN DATE 'EJD'
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             Q=SYNOD*P/36525.DO
C****CALCULATE JULIAN DATE OF MEAN PHASE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 KP=IDINT(Z+0.5)
IF(Z.LT.0.0) KP=IDINT(Z-0.5)
P=DFLOAT(KP)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                            Z=(EJD-2415021.065D0)/SYNOD
                                                                                                                                                                             C****BASED ON ALGORITHMS FROM
                                                                                                                                                                                                                                                                                                                                                                               KNT=0
                                                   003
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(SDS)
                                                                                                                                                                                                                                                                                                                                                                       IF(AGAM.LE.(1.5432+ZL2)) ITYPE=3
ZMAG=(1.5432+ZL2-AGAM)/(0.5460+2.*ZL2)
IF(AGAM.GT.(0.9972+DABS(ZL2))) G0 T0 5
IF(AGAM.GT.(1.5432+ZL2)) G0 T0 5
C****CALCULATE THE SOLAR RADIUS VECTOR (RAU) AND SEMI-DIAMETER
                                                                                                                                                                                                 OF SOLAR ECLIPSE AND ECLIPSE MAGNITUDE.

NO ECLIPSE OCCURS.

TOTAL SOLAR ECLIPSE.

ANNULAR SOLAR ECLIPSE.

PARTIAL SOLAR ECLIPSE.

ANNULAR/TOTAL SOLAR ECLIPSE.
                                                                                                                                                                                                                                                             ECLIPSE IS POSSIBLE
                                                                                                                                                                                                                                                                                                                                                    IF(AGAM.GT.(1.5432+ZL2+0.2)) GO TO 999
                   C****CALCULATE INSTANT OF MAXIMUM ECLIPSE
                                                                                                                                                                                                                                                              PARTIAL
                                                                                                                                                                                                                                                                                                      IF(GAMMA.GT.0.0) LNS=+1
                                        CO TO
                                                                                                                                                                                                   C****DETERMINE TYPE OF
                                                                                                                                                                                                                                                                                                                                             AGAM=DABS (GAMMA)
                                                                                                                                                                                           ZL1=ZL2+0.5460
                                        IF (KNT.LT.3)
                                                                                                                                                                                                             ITYPE=0
                                                                                                                                                                                                                                                             ITYPE=5
                                                                                                                                                                                                                                  ITYPE=2
                                                                                                                                                                                                                                            ITYPE=3
                                                                                                                                                                                                                                                    ITYPE=4
                                                                                                                                                                                                                        ITYPE=1
                                EJD=PJD+EPC
                                                                                                                                                                                                                                                                                                                                   ZMAG=0.0
                                                                                                                                                                                                                                                                                                                                                               ITYPE=5
                                                                                                                                                                                                                                                                         ITYPE=0
                                                   FJD=EJD
                                                                                                                                                                                                                                                                                                                1=0.0
                                                                                                                                                                                                                                                                                             LNS=-1
                                                                                                                                                                                                                                                                                  NCN=1
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T=(FJD-2415020.0D0)/36525.0D0
X=296.104608D0+477198.849109D0*T+9.1917D-03*T*T+1.439D-05*T*T*T
D=350.737486D0+445267.114217D0*T-1.4361D-03*T*T+1.889D-06*T*T*T
Z=358.47583D0+35999.04975D0*T-1.50D-04*T*T-3.3D-06*T*T*T
                                                                                                                                                                                                                                        PAGE 141)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         ZN=0.5458+0.0400*DCOS(DTR*XM)
IF(DABS(S1).GT.DABS(GAMMA)) T1=DSQRT(S1*S1-GAMMA*GAMMA)/ZN
IF(DABS(S2).GT.DABS(GAMMA)) T2=DSQRT(S2*S2-GAMMA*GAMMA)/ZN
C****EXIT SUBROUTINE PRESEC.
                                                                                                   X=DTR*DMOD(X,360.D0)

S=DTR*DMOD(D,360.D0)

Z=DTR*DMOD(Z,360.D0)

S=DTR*DMOD(Z,360.D0)

ENOM=DATAN2(DSIN(Z),(DCOS(Z)-E))

RAU=1.0000002*(1.0-E*DCOS(ENOM))

SDS=959.63/RAU

C****(FROM "ASTRONOMICAL FORMULAE FOR CALCULATORS", MEEUS, PAG
PIM=0.950724+0.051818*DCOS(X)

1 +0.009531*DCOS(D+D-X)+0.007843*DCOS(D+D+X)

2 +0.002824*DCOS(X+X)+0.000857*DCOS(D+D+X)
                                                                                                                                                                                                                                                                                                                         IF(DABS(GAMMA).LT.1.0) DZ=DSQRT(1.0-GAMMA**2)
PIM=2.*RTD*DATAN(1.0/((1.0/DTAN(0.5*DTR*PIM))-DZ))
SDM=0.272476D0*3600.0*PIM
C***CALCULATE MAGNITUDE FOR CENTRAL ECLIPSES.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       W=DSIGN(0.5*P1,GAMMA)
IF(DABS(GAMMA).LT.1.0) W=DASIN(GAMMA)
OMEGA=0.00464*DCOS(W)
IF(ZL2.GT.0.0.AND.ZL2.LT.0.0047.AND.OMEGA.GT.ZL2)
IF(AGAM.GT.0.9972) NCN=+1
IF(AGAM.LE.0.9972) LNS=0
C****CALCULATE THE SOLAR ECLIPSE SEMI-DURATIONS.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                           ZMAG=-ZMAG
                                                                                                                                                                                                                                                                                                                                                                                                                                        ITYPE=1
                                                                                                                                                                                                                                                                                                                                                                                                                                                        ITYPE=2
                                                                                                                                                                                                                                                                                                                                                                                                                                    IF(ZL2.LÉ.0.0)
IF(ZL2.GT.0.0)
IF(ZL2.GT.0.0)
                                                                                                                                                                                                                                                                                                                                                                                                                       ZMAG=SDM/SDS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       S2=1.00+ZL2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               RETURN
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IF(IY.LT.0) JD=IDINT(365.25D0*IYO-0.75)+IDINT(30.6001D0*(IMO+1))
+ID+1720994
                                                                                                                                                                                                          ۰
                                                                                                                                                                                                                                                                                                                            GYR=DFL0AT(IY)+0.01*DFL0AT(IM)+0.0001*DFL0AT(ID)+0.0001*FRAC
                                                  FROM
                                                                                                                                                                                                         MEEUS,
                                                  (Te
                                                                                    15
                                                                                                                                                                                                                                                          REAL*8 DJ,SEC,FRAC,GYR
C****CALCULATE DECIMAL DAY FRACTION.
FRAC=DFLOAT(IHOUR)/24.+DFLOAT(IMIN)/1440.+SEC/86400.
C****CONVERT DATE TO FORMAT YYYY.MMDDdd
                                                                                                                                                         L****REFERENCE : "ASTRONOMICAL FORMULAE FOR CALCULATORS", C****WRITTEN BY F. ESPENAK - APRIL 1982.

REAL*8 DI CEC - TOTAL 1982
                             SUBROUTINE JULDAT (DJ, IW, ID, IM, IY, IHOUR, IMIN, SEC)

C****SUBROUTINE JULDAT COMPUTES THE JULIAN DECIMAL DATE

C****THE GREGORIAN (OR JULIAN) CALENDAR DATE.

C****THE GREGORIAN CALENDAR REFORM OCCURRED ON 1582 OCT

C****THIS IS 1582 OCT 5 BY THE JULIAN CALENDAR.

C****INPUT: ID, IM, IY - DAY, MONTH, YEAR.

C****OUTPUT: DAY, MONTH, YEAR.

C****OUTPUT: DAY, MONTH, YEAR.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           IF(GYR.GE.1582.1015D0) JD=JD+IB
                                                                                                                                                                                                                                                                                                                                                                C****CALCULATE CONVERSION FACTORS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             DJ=DFLOAT(JD)+FRAC+0.5DO
C****CALCULATE DAY OF WEEK.
                                                                                                                                                                                                                                                                                                                                                                                                                                        IMO=IM+12
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         C****CALCULATE JULIAN DATE
                                                                                                                                                                                                                                                                                                                                                                                                                       IY0=IY-1
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  IW=JMOD((JD+1), 7)+1
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              JD=IDINT(DJ+0.5)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                      IB=2-IA+IA/4
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                                                                                                                                                                                                                                                                                                                                                   +1.0D-09
                                                                                                                                                                                                                                                                                                                                                                                                                                                        IA=IY0/100
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SUBROUTINE CALDAT (DJ, IW, ND, ID, IM, IY, IHR, IMIN, ISEC, AHR, AMIN, ASEC)

C****SUBROUTINE CALCAL CALCULATES THE DAY OF THE WEEK, THE DAY OF

C****THE YEAR, THE GREGORIAN (OR JULIAN) CALENDAR DATE AND

C****THE UNIVERSAL TIME FROM THE JULIAN DECIMAL DATE.

C****THE GREGORIAN CALENDAR REFORM OCCURRED ON 1582 OCT 15.

C****THIS IS 1582 OCT 5 BY THE JULIAN CALENDAR.

C****INPUT:

DJ - JULIAN DECIMAL DATE
                                                                                                                                                                        (= O FOR B.C. 4713 JAN 1, 12 GMT).

IW - DAY OF THE WEEK (1=SUNDAY).

ND - DAY OF THE YEAR (1 JAN = 1).

IM, IY - CALENDAR DAY, MONTH, YEAR.

ISEC - INTEGER HOUR, MINUTE, SECOND.

ASEC - DECIMAL HOUR, MINUTE, SECOND.

MICAL FORMULAE FOR CALCULATORS", MEEUS, P.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     IF(KE.GT.13) IM=KE-13
IF(IM.EQ.2.AND.ID.GT.28) ID=29
IY=KC-4715
IF(IM.GT.2) IY=KC-4716
IF(IM.EQ.2.AND.ID.EQ.29.AND.KE.EQ.3) IY=KC-4716
C****CALCULATE THE UNIVERSAL TIME FROM THE FRACTIONAL DAY.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  MONTH AND YEAR
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          IF(JD.LT.2299161) G0 T0 10
IALP=IDINT((JD-1867216.25D0)/36524.25D0)
KA=JD+1+IALP-IALP/4
                                                                                                                                                                                                                                                                                                             C****WRITTEN BY F. ESPENAK - APRIL 1982
C****LAST MODIFIED - 22 JULY 1986.
REAL*8 DJ,FRAC,AHR,AMIN,ASEC
C***CALCULATE INTERGER JULIAN DATE.
                                                                                                                                                                                                                                                                                                                                                                                                                                  FRAC=DJ+0.5-DFL0AT(JD)+1.0D-10
C****CALCULATE CONVERSION FACTORS.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    KC=IDINT((KB-122.1)/365.25D0)
KD=IDINT(365.25D0*KC)
KE=IDINT((KB-KD)/30.6001D0)
C****CALCULATE THE CALENDAR DAY, MO
ID=KB-KD-IDINT(30.6001D0*KE)
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AHR, AMIN, ASEC -
: "ASTRONOMICAL B
                                                                                                                                                                                                                                                                                                                                                                                             JD=IDINT(DJ+0.5)
C****CALCULATE DAY FRACTION.
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IHR=AHR

AMIN=(AHR-IHR)\*60.

IMIN=AMIN

ASEC=(AMIN-IMIN)\*60.

ISEC=ASEC

C\*\*\*\*CALCULATE THE DAY OF THE WEEK.

IW=JMOD((JD+1),7)+1

C\*\*\*\*CALCULATE THE DAY OF THE YEAR.

LYR=4\*(IY/4)

ND=(275\*IM)/9-2\*((IM+9)/12)+ID-30

IF(IY:Eq.LYR) ND=(275\*IM)/9-((IM+9)/12)+ID-30

IF(IX:YRA-E=-',5IB)/9-((IM+9)/12)+ID-30 042 043 044 045 046 047 048 050 053 054 055 055

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#### 16. Abstract

A complete catalog is presented. listing the general characteristics of every solar eclipse from 1901 through 2100. To compliment this catalog, a detailed set of cylindrical projection world maps show the umbral paths of every solar eclipse over the 200 year interval. Focusing in on the next 50 years, accurate geodetic path coordinates and local circumstances for the 71 central eclipses from 1987 through 2035 are tabulated. Finally, the geodetic paths of the umbral and penumbral shadows of a all 109 solar eclipses in this period are plotted on orthographic projection maps of

Appendices are included which discuss eclipse geometry, eclipse frequency and occurrence, modern eclipse prediction and time determination. Finally, code for a simple Fortran program is given to predict the occurrence and characteristics of solar eclipses.

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